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GROUND GEOPHYSICAL SURVEY WORK REPORT ON A 3D DCIP SURVEY

AT THE REED-ROBINSON CLAIMS (EBY-OTTO PROPERTY)

EBY & OTTO TOWNSHIPS

LARDER LAKE MINING DIVISION, ONTARIO

NTS Sheet 042A01

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Summary

A ground surface 3D IP geophysical survey was undertaken at the Reed-Robinson claims between October 24 and November 16, 2022 (24 days). Dias Geophysical of Saskatoon, SK, was contracted to perform the 3D IP survey at the request of Canada Silver Cobalt Works (CSCW, "the Company"). Additionally, Jordan Barrette was hired as a contractor to assist the Company and Dias Geophysical personnel with line cutting from October 25th to November 16th, 2022 (23 days).

42.35 kms of grid lines surveyed over a total of 24 days of work. The 3D IP and resistivity data was collected as full waveforms and quality controlled by Dias Geophysical during collection. All data was collected in UTM WGS84 Zone 17 coordinates and then converted to UTM NAD83 Zone 17 during the data processing phase. The 3D DCIP data was processed, and quality controlled, with in-house proprietary algorithms and then transformed with inversion models by Dias Geophysical. Deliverables were provided to the Company on December 9, 2022.

The purpose of this program was to characterize the electrical properties of the sub-surface, up to a depth of ~400m, and identify new geophysical targets for drilling that have the potential for Cadillac-Larder Lake Break associated vein-hosted gold mineralization as well as base and/or battery metal mineralization.

To complete this work Dias Geophysical employees: cut survey lines, installed then removed survey equipment along the survey lines, injected the wires and nodes with current, and collected/reviewed the data in field. These physical activities were undertaken at the field site daily. The non-invasive nature of the surveys did not require the need for rehabilitation. Dias Geophysical personnel processed and modeled the data remotely.

The 3D conductivity, resistivity, and chargeability models provided by Dias Geophysical on Dec 9th, 2022, gave an excellent characterization of the subsurface electrical properties for the entirety of the greater Reed-Robinson claim package to a maximum depth of 400m below surface. The 3D models reveal that the gabbroic intrusion that underlies most of the ground survey surface area is generally resistive with low chargeability. There are several features that contrast the weak electrical background of the gabbroic intrusion with discrete, overlapping highly conductive, and chargeable values that are spatially consistent.

Based on the geophysical ground survey it is concluded that there are geologically unexplained discrete conductive bodies and chargeable areas within 400m of the sub-surface within the greater Reed-Robinson claim package. Some of these conductive and chargeable features are possibly areas of increased sulphide mineralization. Areas of increased sulphide mineralization within the gabbroic intrusion that are hosted in brecciated veins, as seen in the Vigrass Lake occurrence, may host economic quantities of gold.

It is the recommendation of the company that, based on the electrical properties of the subsurface as modeled by Dias Geophysics, drilling targets shallower than 400m below surface could be selected and drilled in future drill programs within the greater Reed-Robinson claim package.

Property Location, Description, and Access

The Reed-Robinson claim group is part of the larger Eby-Otto property consolidated by Canada Silver Cobalt Works (CSCW, "the Company") through several option agreements, as reported in a news release announced on February 14, 2022 (https://www.canadasilvercobaltworks.com/news/gold-property-consolidated-near-agnico-eagles-macassa-mine/).

The Reed-Robinson claim group is comprised of 11 single and boundary cell claims and 3 leases optioned from four separate claim holders. The claims and leases are currently held by Canada Silver Cobalt Works under an option agreement with prospectors James Reed, Emmy Reed, Douglas Raymond Robinson, and Betty (Elizabeth) Robinson executed on July 28, 2021. The location of the Property is shown in Figures 1 and 2, and the details of the claims are listed in Table 1. The agreement allows for Canada Silver Cobalt Works to acquire a 100% interest over a five-year period through a combination of share issuances, cash payments, and work expenditures. The work described in this report fulfills a portion of the first year of work expenditure requirements.

The Reed-Robinson claims lie between 1 and 5 km southeast of the community of Kenogami Lake and approximately 9 km southwest of the Town of Kirkland Lake in northeastern Eby Township (and partly in northwestern Otto Township) in Northeastern Ontario. The property is bounded to the west by a natural gas pipeline and crossed by a hydroelectric powerline in the east. There are two non-contiguous land areas in this claim package. Lease 108929 and 108931 are located approximately 1km south of all other contiguous claims. These two leases had no geophysical ground surveys conducted on them and will be accordingly excluded from the remainder of this report.

The reported ground geophysical survey program covered an extent of the Eby and Otto Townships that is shown in Figure 3.

Access to the property is via Highway 11 to Highway 66 East, and then turning south onto Metering Road and entering the property through a privately owned driveway. The Company has cut a new trail into the property to access the drill site with heavy equipment. The property is bounded to the west by a natural gas pipeline and a hydroelectric powerline crosses the east side of the property.

Access to the planned drill site was difficult as the terrain here is a mosaic of densely forested, roughly parallel east-west trending outcrop ridges with wet and swampy troughs between them that are often very wet.

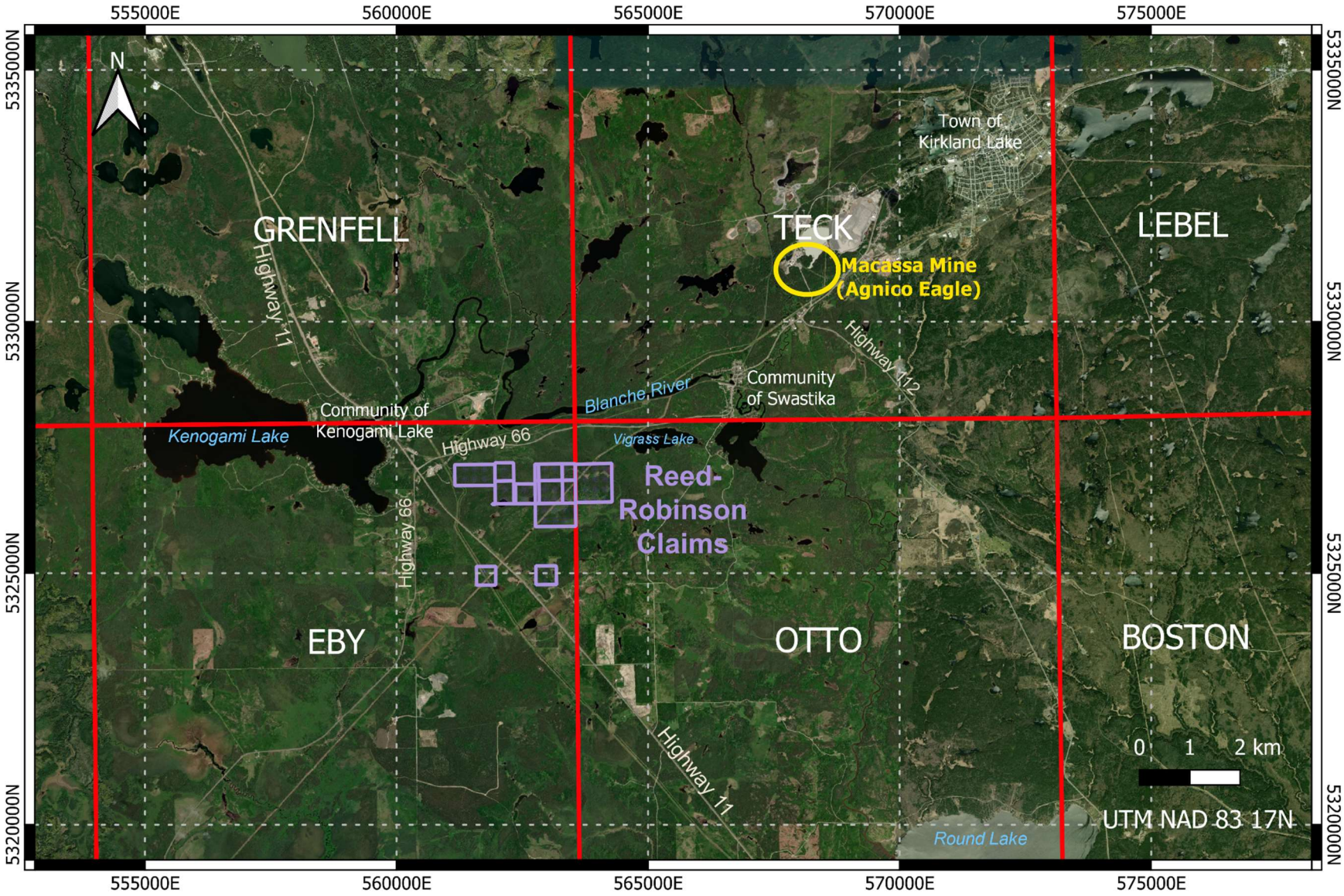


Figure 1. Regional property location map. Purple outline bounds the Reed-Robinson claims. Township boundaries in red.

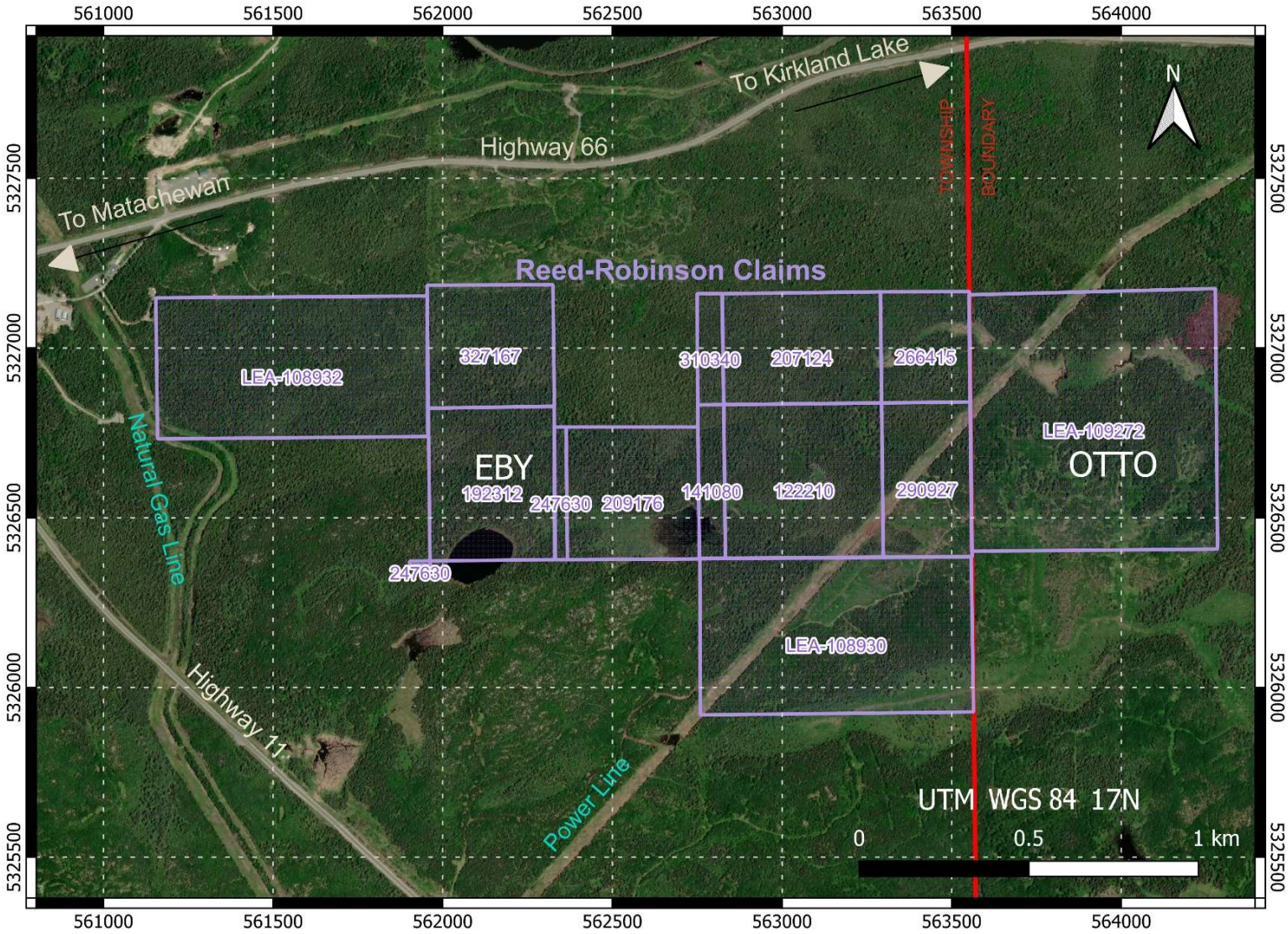


Figure 2. Reed-Robinson property claim areas in which work was performed. Boundary cell claims are clipped to extents of legacy claim boundaries.

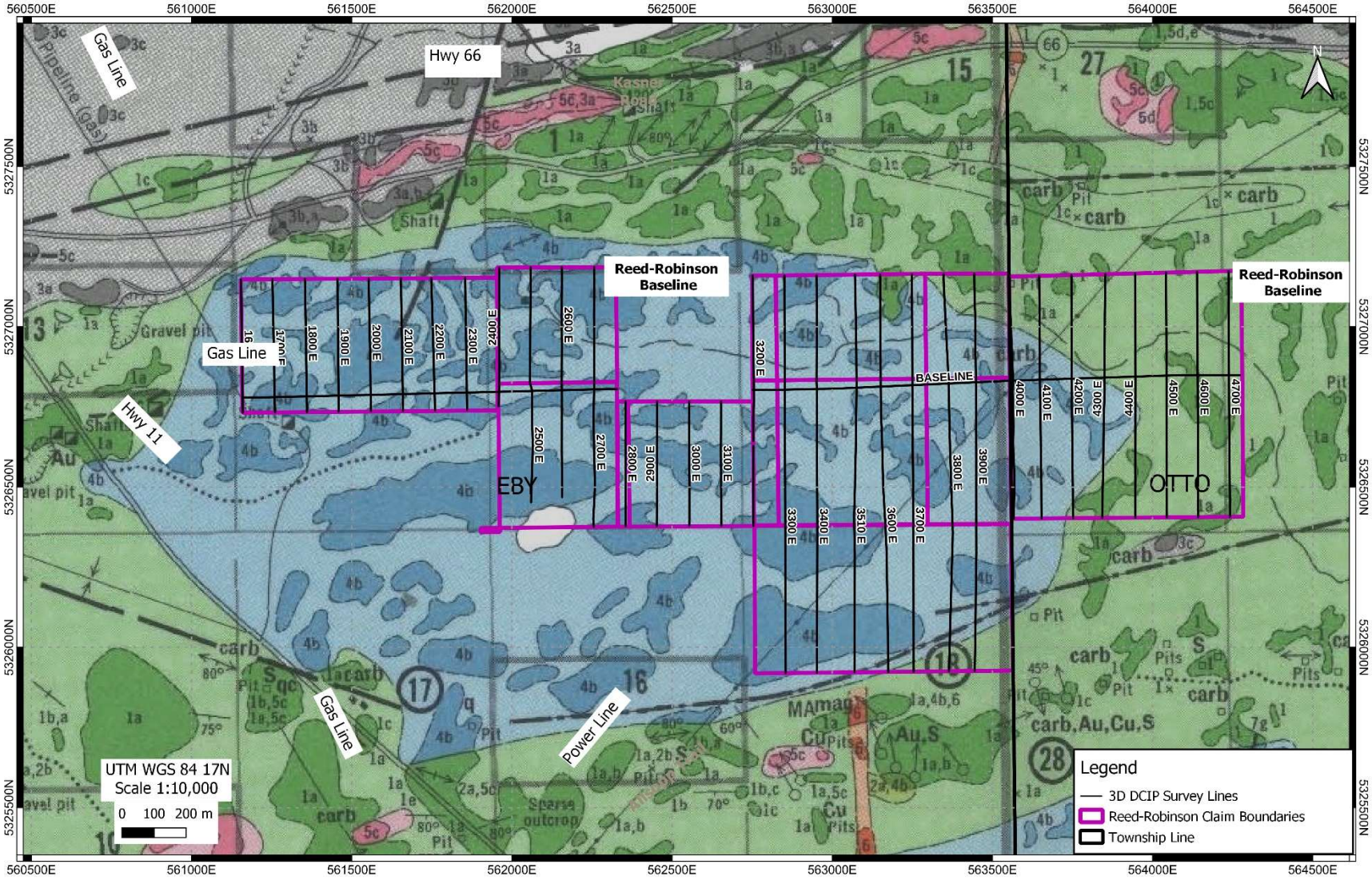


Figure 3. Ground geophysics survey lines in the greater Reed-Robinson claim package with geologic map from Lovell (1972)

Table 1. Details of claims included in Option Agreement where Ground Geophysical Surveys were completed.

Claim Number	Township	Claim Title Type	Anniversary Date	Claim Holder, the Optionor (percentage held)
122210	EBY	Single Cell Mining Claim	12-01-2027	EMMY L REED (100%)
141080	EBY	Boundary Cell Mining Claim	12-01-2027	EMMY L REED (100%)
192312	EBY	Boundary Cell Mining Claim	06-01-2027	DOUGLAS RAYMOND ROBINSON (100%)
207124	EBY	Boundary Cell Mining Claim	12-01-2027	EMMY L REED (100%)
209176	EBY	Boundary Cell Mining Claim	08-02-2028	BETTY (ELIZABETH) ROBINSON (100%)
247630	EBY	Boundary Cell Mining Claim	08-02-2028	BETTY (ELIZABETH) ROBINSON (100%)
247630	EBY	Boundary Cell Mining Claim	08-02-2028	BETTY (ELIZABETH) ROBINSON (100%)
266415	EBY-OTTO	Boundary Cell Mining Claim	12-01-2027	EMMY L REED (100%)
290927	EBY-OTTO	Single Cell Mining Claim	12-01-2027	EMMY L REED (100%)
310340	EBY	Boundary Cell Mining Claim	12-01-2027	EMMY L REED (100%)
327167	EBY	Single Cell Mining Claim	06-01-2027	DOUGLAS RAYMOND ROBINSON (100%)
108930	EBY	Lease	30-11-2032	JAMES AND EMMY L. REED (100%)
108932	EBY	Lease	30-11-2032	JAMES AND EMMY L. REED (100%)
109272	OTTO	Lease	30-05-2033	JAMES AND EMMY L. REED (100%)

Permits

No permits were required for this work. Plans were required because of line cutting less than 1.5m wide and because the survey utilize a generator in the field during survey day. Plans PL-22-000068, PL-22-000069, PL-22-000070, PL-22-000071, PL-22-000074, and PL-22-000075 were approved on Oct 22nd 2022.

Previous Work

Much of the previous work completed on the greater Reed-Robinson claim group has been described by Halliday et al (2021) and Marion (2016). This report will focus on work completed only across the claims listed in Table 1.

Various Ontario government geological agencies have performed geological mapping and geophysical surveying of the Reed-Robinson claim group area since the first mapping survey of Eby Township in 1914. Generally, these surveys of the Reed-Robinson claim group area are included as an extension of the Kirkland Lake, Matachewan, or Kenogami Lake areas, and have only occasionally focused on Eby and Otto townships (Lovell, 1972). A summary of maps and reports produced by government agencies is presented in Table 2.

Various prospecting individuals and exploration groups have completed historic assessment reports, and associated field work, in the greater Reed-Robinson claim package from 1977 to present. A summary of historic assessment work is presented in Table 3.

The first work filed in the vicinity of the claim package was Essex Minerals Co in 1977 who surveyed the area with electromagnetic and magnetics ground surveys as well as preliminary geologic mapping. Three years later in 1980, two instances of diamond drilling were reported. These programs were for Noranda Exploration Company LTD, and James D Reed who respectively drilled three ~125m holes, and one 93m hole. Noranda Exploration's drill logs mostly logged andesite, tuff, mafic intrusives, syenite dikes and graphitic sediments that this author interprets as graphitic fault zones. Assays reported in the log did not have any Au values above 0.005 oz/t.

Throughout the 1980s, James D Reed continued work and assessment reports on the eastern half of the greater Reed-Robinson claim package, specifically claims 310340, 207124, 266415, 141080, 122210, 290927 and lease 109272. Radiometric and VLF electromagnetic geophysical ground surveys in addition to overburden stripping were completed in 1982. In 1984 James D Reed drilled 6 shallow holes into the subsurface under a bog, in hopes of finding commercial gold values near surface. These holes reached maximum depths of 35m, and no significant gold values were found. Also in 1984, James D Reed completed geologic surveying and mapping program to compliment and follow up on the drill program.

The next work reported in the claim package is in 1995 when Reed, Reed, Reed, and Reed conducted a comprehensive field season. The work is summarized as line cutting, detailed mapping and hand stripping with emphasis on alteration and structural lineaments, max-min EM surveys and

a total field-magnetic gradient survey. Several geophysical anomalies were located, and it was recommended at the end of the program that more lines be cut and that higher resolution ground surveys be conducted.

In 1995, over the same lease and claims, James D Reed completed a portion of the 1994 recommendations. Similar recommendations were made at the end of that year as they were made in 1994, indicating that additional line cuts and ground surveys should continue to be added to the property. Also, in 1995 Doug Robinson completed detailed geologic mapping with an emphasis on alteration and structural lineations, line cutting, overburden stripping, and various geophysical ground surveys over the western claims of the greater Reed-Robinson claim group, specifically claims 327167, 192312, 247630, and 209176.

From 1997 to 1998, J E Tisley & Associates, in conjunction with Nastek Exploration Ltd optioned the claims from Reed and Robinson. During this time, they completed a similar suite of work over the claim package in furtherance of the recommendations from 1994 and 1995.

Assessment worthy work over the claim package ceased for over a decade until 2011 when Robinson, Robinson, and Reed returned for several field seasons to recut lines, perform magnetic surveys, and collect samples for assay. In 2018 aboriginal consultation and a mobile metal ion survey was completed on claims 327167, 192312, 247630, and 209176 that produced mixed results. In 2020 Eric Marion completed physical work over the northeast portion of lease 109272. This work included the manual stripping, outcrop clearing and mapping of one outcrop that contained a heavily altered deformation zone with up to 10% pyrite in some areas.

To date there has not been any reported IP surveys of any kind on this claim package. The ground survey program outlined in this report will be the first to characterize the resistivity and chargeability of the subsurface to depths of up to 400m below surface.

Excluding line cutting and the installation of the hydro line and gas pipeline infrastructure, there has never been any historical development of these claims, nor has there ever been any production aside from assays of outcrop cuttings and diamond drilling samples.

Table 2. Summary of government agency maps and reports across the Reed-Robinson claim group.

Title	Map Number	Authors	Year	Map Scale	Government Agency
Townships of Maisonville, Grenfell and Eby, District of Timiskaming	ARM 23B	R.M. Smith, R.W. Young, P.E. Hopkins & A.G. Burrows	1914	1:47,520	Ontario Department of Lands, Forests, and Mines
Matachewan-Kenogami area, District of Timiskaming, Ontario	ARM 44B	W.S. Dyer and G.H. Charlewood	1935	1:63,360	Province of Ontario Department of Mines
Eby Township, District of Timiskaming	P0448	H.L. Lovell	1968	1:15,840	Province of Ontario Department of Mines
Eby-Otto area, Timiskaming District	M2239	H.L. Lovell	1972	1:31,680	Province of Ontario Department of Mines and Northern Affairs
Geology of the Eby and Otto Area, District of Timiskaming	GR 99	H.L. Lovell	1972	NA	Province of Ontario Department of Mines and Northern Affairs
Ontario Airborne Geophysical Surveys, Magnetic and Electromagnetic Data, Grid and Profile Data, ASCII and Geosoft Formats, Kirkland Lake Area	GDS1022	Ontario Geological Survey	2003	NA	Ontario Geological Survey
Precambrian Geology of Otto and Eby Townships	P3534	L. Pigeon and B.R. Berger	2004	1:20,000	Ontario Geological Survey
Precambrian Geology, Highway 66 Area, Swastika to Matachewan	2677	B.R. Berger, L. Pigeon, & G. Leblanc	2006	1:50,000	Ontario Geological Survey
Geological Synthesis Along Highway 66 from Matachewan to Swastika	OFR 6177	B.R. Berger	2006		Ontario Geological Survey

Table 3. List of reported previous work on the relevant Reed-Robinson Claims

YEAR	AUTHOR	DESCRIPTION OF WORK	ASSESSMENT FILE NUMBER
1977	ESSEX MINERALS CO	Electromagnetic, Geologic Survey/Mapping, Magnetic and Magnetometer Survey	41P14NE0080
1980	JAMES D REED	Diamond Drilling	42A01SE0152
1980	NORANDA EXPLORATION CO	Diamond Drilling	42A01SE0146
1982	JAMES D REED	Miscellaneous, Radiometric, Very Low Frequency Electromagnetics	42A01SE0139
1982	JAMES D REED	Miscellaneous Compilation and Interpretation, Radiometric Survey	42A01SE0134
1983	JAMES D REED	Overburden Stripping	42A01SE0122
1984	JAMES D REED	Assaying and Analyses, Overburden Stripping	42A01SE0196
1984	JAMES D REED	Geologic Survey/Mapping	42A01SE0128
1990	BATTLE MOUNTAIN CANADA LTD	Airborne Very Low Frequency Electromagnetics, Airborne Gradiometer, Airborne Magnetometer	42A01SE0002
1995	C E REED, E L REED, JAMES D REED, AND N E REED	Assaying and Analyses, Electromagnetic, Geologic Survey/Mapping, Gradiometric, Magnetic and Magnetometer Survey, Manual Labour Mechanical, Open Cutting	42A01SE0088
1995	JAMES D REED	Electromagnetic Ground Survey, Line Cutting, open Cutting	42A01SE0028
1995	DOUG ROBINSON	Compilation and Interpretation - Geology, Electromagnetic Survey, Geochemical, Geologic Survey/Mapping, Magnetic/Magnetometer Survey, Open Cutting, Overburden Stripping	42A01SE0085
1997	J E TISLEY & ASSOCIATED LTD, NASTEK EXPL LTD	Compilation and Interpretation – Max-Min Electromagnetics and Radiometric Ground Survey, Digging Pits, Geologic Survey/Mapping	42A01SE2010
1998	NASTEK EXPL LTD	Compilation and Interpretation - Geology, Electromagnetic, Magnetic/Magnetometer Survey, Open Cutting	42A01SE2006
1998	NASTEK EXPL LTD	Compilation and Interpretation – Magnetic and Electromagnetic Survey, Geologic Survey/Mapping, Open Cutting	42A01SE2007
2011	BETTY ROBINSON, DOUGLAS RAYMOND ROBINSON, JAMES D	Line cutting, Magnetic/Magnetometer Survey	20000006072

YEAR	AUTHOR	DESCRIPTION OF WORK	ASSESSMENT FILE NUMBER
	REED		
2013	BETTY ROBINSON, DOUGLAS RAYMOND ROBINSON, JAMES D REED	Geochemical, Line Cutting	20000008656
2018	BETTY ROBINSON, DOUGLAS RAYMOND ROBINSON, JAMES D REED	Aboriginal Consultation, Mobile Metal Ion Survey	20000015637
2020	ERIC MARION	Bedrock Trenching, Digging Pits, Overburden Stripping	20000018161

Regional Geology

The Neoarchean Abitibi Greenstone Belt is composed of a series of stacked assemblages (or sub-terranes) comprised predominantly of supracrustal volcanic, associated intrusive, and related interflow sedimentary rocks in the south-central region of the Superior Province, spanning across Ontario and Quebec. The assemblages are stitched together by major structural deformation zones, such as the Cadillac-Larder Lake Deformation Zone (CLLDZ) and the Porcupine Deformation Zone (PDZ), which parallel each other west to east across the belt, and record a history of orogenesis. Granitoid plutons associated with orogenesis intrude every lithology (Monecke et al., 2017).

The trend stretching from Matachewan, ON, to Val-d'Or, QC, known as the Kirkland Lake-Larder Lake Gold Belt, is marked by its association with the Cadillac-Larder Lake Deformation Zone (CLLDZ, or "Cadillac-Larder Lake Break"), a steeply dipping zone of deformation marked by intense and multiply-reactivated structures and hydrothermal carbonate alteration which hints at a long and complex structural history. Several major gold deposits occur along or proximal to the CLLDZ (or second order splays of the CLLDZ), including the Young-Davidson deposit (Matachewan, ON; currently operated by Alamos Gold), the Kirkland Lake deposit (Kirkland Lake, ON; the Macassa Mine is the only remaining operating mine of the Kirkland Lake Deposit, and is currently operated by Agnico Eagle Mines), the Kerr-Addison deposit (Virginiatown, ON; not currently operating), and the Canadian Malartic deposit (Val-d'Or, QC; operated by Agnico Eagle Mines and Yamana Gold Mines).

In the Kirkland Lake area, the Kirkland Lake-Larder Lake Gold Belt can be divided into three east-west bands of rocks, or assemblages: northern, central, and southern (Ispolatov et al., 2008). The northern assemblage is predominantly composed of Archean submarine volcanic, mafic intrusive, and related interflow sedimentary rocks of the Blake River Assemblage (2704-2696 Ma). The northern assemblage is separated from the central assemblage by a conformable contact. The central assemblage is comprised of sub-marine to sub-aerial volcanic rocks such as trachytes and tuffs, related syenitic intrusions, and associated orogenic and fluvial greywackes and conglomerates of the Temiskaming Assemblage (2676-2670 Ma). The central assemblage is separated from the southern assemblage by the CLLDZ, and is footwall to the southern assemblage. The southern assemblage is comprised of sub-marine mafic to ultramafic volcanic and related intrusive rocks and interflow sedimentary rocks of the Tisdale Assemblage (A.K.A. Larder Lake Group; 2710-2707 Ma) (Ispolatov et al., 2008). Several east-west to northeast-southwest faults occur within the southern assemblage and are possibly hanging wall splays of the CLLDZ. The most significant of these faults to the Tinney claims (and Eby-Otto property in general) is the Eby-Otto fault, which strikes approximately 070 and dips south (Lovell, 1972).

The Round Lake Batholith and smaller Otto stock are large Archean-aged granitic to dioritic intrusive bodies, occurring to the east and south-east of the property. Several major north-northwest striking late faults related to the Temiskaming Rift Valley cut across and offset these assemblages and well as the CLLDZ, the Main Break, the '04 Break, and the Amalgamated Break. The most significant of these faults is the Amikougami Creek Fault to the west of the Macassa Mine

in the community of Swastika, which offsets the breaks several hundred meters in the sinistral direction (west side south).

The Kirkland Lake deposit and related South Mine Complex (in operation at the Macassa Mine in Kirkland Lake) are entirely hosted within rocks of the Temiskaming assemblage. The Kirkland Lake deposit itself is hosted along the near-vertical south-dipping Kirkland Lake Main Break and the '04 Break (and related structures and splays) to the north, while the South Mine Complex is bound between the Main and '04 Breaks and the near-vertical north-dipping Amalgamated Break to the south (Ispolatov et al., 2008).

The Vigrass Lake gold occurrence (property held by Agnico Eagle), located approximately 6.5 km to the northeast of the claims surveyed in this report, is the closest known gold occurrence in the Eby-Otto township area, structurally and stratigraphically. The Vigrass Lake occurrence is hosted within mafic to ultramafic volcanic rocks with interbedded graphitic and pyritic interflow sedimentary rocks intruded by syenite porphyry and lamprophyre dykes of the Tisdale Assemblage (Benham, 1994). Mineralization occurs as finely disseminated sulphides and stockworks of quartz veins within a series of subparallel faults and strongly altered (carbonated and silicified) shear zones. These structures mark the contacts between the predominantly komatiitic and basaltic assemblages. A complex zone of shearing and alteration located south of and along the south shore of Vigrass Lake is known as the Vigrass Lake Fault (Benham, 1994).

The mineral deposit style CSCW is targeting in this 3D DCIP ground survey is the vein-hosted and breccia-hosted gold mineralization associated with second order structures similar to the mineralized zones observed at the Vigrass Lake occurrence. Breccia-hosted gold mineralization within 450m of the surface would appear as low resistivity, high chargeability zone in what is demonstrated to be a highly resistive gabbroic intrusion. The survey may also identify features consistent with base metal sulphide or battery metal deposits, which would also be targets for future drilling. Geophysical signatures as described will be priority drilling targets.

Table 4: Table of lithologic units (taken from Lovell's Geology of Eby and Otto Townships).

CENOZOIC

PLEISTOCENE AND RECENT

Silt, clay, sand, gravel

Unconformity

PRECAMBRIAN

PROTEROZOIC

LATE MAFIC INTRUSIVE ROCKS (NIPISSING OR KEWEENAWAN)

Diabase

Intrusive Contact

HURONIAN

COBALT GROUP

GOWGANDA FORMATION

Conglomerate, arkose, greywacke, argillite

Unconformity

ALKALIC INTRUSIVE ROCKS

Syenite, quartz syenite, porphyritic syenite, nepheline syenite, granite, aplite dikes, lamprophyre, diorite

Intrusive Contact

ARCHEAN

MAFIC INTRUSIVE ROCKS (MATACHEWAN OR NIPISSING)

Diabase

Intrusive Contact

FELSIC INTRUSIVE ROCKS (ALGOMAN)

Granite, porphyritic granite, granodiorite, granodioritic gneiss, syenite and trachyte

Intrusive Contact

EARLY MAFIC AND ULTRAMAFIC INTRUSIVE ROCKS (HAILEYBURIAN, EARLY ALGOMAN, AND KEEWATIN)

Serpentinite, peridotite, gabbro, diorite

Intrusive Contact

METASEDIMENTS (TIMISKAMING AND KEEWATIN)

Conglomerate, quartzite, greywacke, tuff, agglomerate, breccia

Unconformity and Interbedding

FELSIC METAVOLCANICS (KEEWATIN)

Rhyolite, dacite, dacite porphyry, iron formation, silicic tuff, agglomerate

MAFIC METAVOLCANICS AND METASEDIMENTS

Basalt, andesite, andesite porphyry, dacite, chloritic mafic tuff, agglomerate, amphibolite, garnet-epidote amphibolite, amphibolite gneiss, biotite-garnet-pyroxene amphibolite

Property Geology

According to OGS Map 2239 of Eby and Otto townships (Lovell, 1972), there are three lithologies mapped at surface across the claim group. The Reed-Robinson claims are almost entirely underlain by a large egg-shaped multi-phase mafic intrusion (gabbro to diorite in composition) known colloquially as the “Blue Blob” intrusion (Figure 3). The unit is contemporaneous with mafic volcanic rocks (pillowed basalts, variolitic basalts, volcanic breccias and tuffs) of the Tisdale Assemblage (A.K.A. Larder Lake Group)(Berger and Pigeon, 2004; Lovell, 1972). At surface the gabbroic body is ~2.5km long from east to west and ~1.5km wide from north to south.

Surrounding the intrusion are low-grade metamorphosed (greenschist facies) mafic volcanics and sediments of the Tisdale Assemblage (A.K.A. Larder Lake Group), specifically basalt. These lithologies are only exposed at surface at the east end of the property (claim 266415, LEA-109272, and LEA-108930). A small North-South striking diabase is mapped near the south-eastern corner of the gabbroic intrusion and may be present along the border of the southern-most extents of the lease LEA-108930.

A few syenite porphyry and feldspar porphyry dykes occur north and south of the Reed-Robinson claims (Lovell, 1972), though none have been mapped within the property boundaries.

The southern lithological contact of the gabbroic intrusion and the mafic volcanics is interpreted to be cut by an extension of the Eby-Otto fault that may also intersect the southeastern corners of leases LEA-109272 and LEA-108930.

Additionally, there is a NE-SW striking accommodation fault originating from the CLLDZ and terminating in the gabbroic intrusion. The accommodating fault will run under the northern extent of lease LEA-108932 and terminate within the same lease. Previous geologic mapping by claim holder Doug Robinson identified 4 lineaments interpreted as possible fault structures in lease LEA-1089322 as well.

In the area of the claims surveyed in this program, outcrop exposure is fairly good (~10% outcrop exposure). The property terrain here is a mosaic of densely forested, roughly parallel east-west trending outcrop ridges with wet and swampy troughs between them that are often very wet and swampy.

Methods

All survey specifications, parameters, in-field methodology, and data processing summarized below are taken, at times directly, from Appendix B: Dias Geophysical Logistics Report, that was written by Dias Geophysical Limited and delivered to the Company on Dec 9th 2022 as per our agreement.

The total distance of lines traversed by Dias Geophysical personnel between Oct 25, 2022 to Nov 16, 2022 (23 days) for the 3D DC-Resistivity and IP ground geophysics survey was 42.375 km. The 3D DC-Resistivity and IP ground geophysics survey ('the survey') was the only one performed on this property in this report and produced all results discussed within. All data was collected in UTM WGS84 Zone 17 coordinates and then converted to UTM NAD83 Zone 17 during the data processing phase.

The survey was performed using the DIAS32 acquisition system in conjunction with one GS5000 transmitter. The 3D program, covering an area of approximately 3.75 km^2, was completed using a rolling distributed partial 3D DCIP array with a pole-dipole configuration. For acquisition the DIAS32 Receiver, a single channel mesh network time series receiver, was used in conjunction with a control computer that acquired electrical information from a series of 45cm flat steel electrodes connected by insulated 16 American-wire-gauge wire. For transmission a 12.5 kW generator was used to power a DIA GS5000 transmitter that interfaced with an additional control computer and sent electrical signals through 1 meter steel rod electrodes through insulated 16 American-wire-gauge wire. Survey specifications that indicate a scale constant, sensitivity, or equivalent are listed below in Table 5.

Table 5. General specifications of survey equipment as replicated from Appendix A: Dias Geophysical Reed-Robinson Logistics Report

General Specifications	
Survey Mode	Rolling Distributed 3D survey with common voltage reference
Array Type	Pole-Dipole
Receiver Specifications	
Electrode 'a'/line spacing	75m/150m
Electrodes per injection	21 to 65
Receiver sampling interval	150 sampled per second
Transmitter Specifications	
Current injection/line spacing	150/150m
Current Remote Location	566115E/5327548N/320m (NAD83Z17U)
Transmitter waveform	50% duty cycle, square wave
Transmitter base frequency	0.125 Hz (8 second cycle)

Transmitter Injection Location	Coincident with every second receiver station

Survey methods, the instruments used, the operational technique, and the parameters measured, are described below.

Dias Geophysical completed the Reed-Robinson grid using a 3D rolling distributed array in common voltage reference (CVR). Characteristics of the survey layouts are as follows:

- The grid included 21 lines spaced 150m apart and of length varying between 0.45 to 1.275 km. All lines were oriented south-north with an azimuth of 0 °.
- All survey lines, labelled 3200E through 6400E, were used as both receiver and transmitter lines.
- Along the lines, receiver stations were spaced 75 m apart.
- Transmission stations were spaced 150 meters apart along each line, coincident with every second receiver station. Two extensions were done, when possible, to the north and south end of each line to improve depth resolution along the edges of the grid.
- The current remote station was located approximately 1.75 km east of the eastern-most survey line
- All stations were established by the field crew using handheld Garmin 64s GPS devices. The coordinates of the actual stations were recorded and stored for data processing.

The survey procedures are as follows:

- The project was completed using a Pole-Dipole configuration.
- For each injection on the grid, a minimum of three receiver lines were active.
- When injecting current at a given station, the receiver located at this station was deactivated to avoid damages.
- Following the completion of an injection line, the receiver line configuration was incremented in preparation for the next line of injections by picking up the completed injection line and infilling the new injection line with receivers.

Electrodes are used to receive and transmit electrical current from the ground to the installed nodes and potential wire. Electrodes are installed by driving the steel electrodes vertically into the ground to a minimum of 30 cm. The local current electrode is comprised of two separate steel cylindrical 1-meter rods driven vertically into the ground. The remote site was comprised of 6 steel cylindrical 1.2-meter rods. The rods were placed in damp ground. Both the local current and current remote were deployed using 16 AWG transmission wire to the transmitter site.

Dias employs a common voltage reference (CVR). Each receiver station has a dedicated DIAS32 receiver node connected to the CVR and a single receiver electrode. This allows each receiver node to record the voltage difference between the grounded electrode and the CVR wire.

CVR wire is deployed along all receiver lines to provide a CVR to receivers. Current injection wire is run from the transmitter site to the current remote location, where it terminates at the current remote stakes. A second current injection wire acts as the current feed and is run from the transmitter site to the active injection site. Two electrodes are driven into the ground at the active current injection site and are connected to the current feed wire. The procedure for power transmission is then initiated. Once the reading is complete and the procedure for ceasing power transmission is concluded, the current injection electrodes are removed and the crew advances to the next injection point. DIAS32 nodes and electrodes are installed before any injections take place and stay out for all injections.

A Dias GS5000 transmitter was used for the project to provide output up to 10.0 kW and 4000 V. The transmitted current ranged from ~100 mA to ~4.2 A for the grid. The current transmission was maintained for a recording time of 4 minutes per station, with the injection time being a function of current injected at each site. Since the injection site is coincident with the receiver locations, before injections, the receiver at that site was disconnected.

The following information was recorded with each reading:

- current electrode location
- potential electrode locations
- primary voltage
- integrated normalized secondary voltages (i.e. chargeabilities) in milliseconds (ms)
- the transmitter current amplitude
- number of stacks
- standard deviation of the stacks
- time of the reading
- the amount and width of the secondary voltages

Ground conditions at site were a mix of heavily forested east-west trending gabbroic ridges with overburden filled troughs that were often very wet and with poor drainage. Over the course of this project, the air temperature varied between -3 ° and 15 °C, with precipitation in the form of rain and snow later in the season, contributing to wet conditions. Terrain in the Reed-Robinson property was a mosaic of wet moss-covered rock outcroppings, deep loamy overburden, wet swampy ground, and wet moss-covered forest. All terrain effects/ ground conditions were quality controlled in field and during the data processing phase.

Dias deployed flat, stainless-steel electrodes driven into the ground at receiver stations. This type of electrode provides low noise characteristics for the band width of the survey. The contact resistance of each electrode was tested, where the resistance exceeded 10,000 Ω the electrode was moved, or a second electrode was installed to reduce the contact resistance. Where the ground contact was quite high salt water was added at the injection site.

In presence of high noise levels (as can be caused by power line utilities) and/or low signal, longer readings were collected to help support the rejection of compromised segments of signal. In

some areas of higher ground resistance, receivers located near the current injection tended to overvoltage, thus compromising data reliability. In these circumstances double injections were carried out: a 4 to 6 min injection at maximized current intensity with nearby receivers disconnected to provide good signal quality at medium and far offset, and a second, 2 min injection at a current amplitude low enough to prevent over-voltaging of the nearby receiver.

Where the current varied by more than 10% during this recording time, the transmission was terminated, the injection electrode contact was improved, and the transmission re-started to provide a stable current for the duration of the recording.

Buried gas line utilities often have repeating electrical cathode injections that prevent corrosion of the pipeline. These signatures were not significant enough to be observed in the raw field data and were later easily filtered out as minimal background noise during the Dias data processing procedure.

The DIAS32 receivers automatically recorded time series data stamped with GPS time and location information. In addition, time series recording of the current waveform was conducted at the current injection point. These two sets of time series data were processed using proprietary algorithms. A wide range of processing techniques were available (statistical rejection, ensembles, deep stacking, etc.). The most suitable processing technique was determined based on the type of interference affecting the signal.

For the Reed-Robinson project the signal was processed using two different processing techniques. For most injections Overlapping Ensembles were used: the time series recorded by each receiver during each reading was split into 11 overlapping segments – or ensembles. Each ensemble was then analyzed for spikes and other statistical inconsistencies. The ensembles showing inconsistencies were then discarded and the remaining “clean” ensembles were stacked.

A few injections showed some isolated spikes that lead to noisy stacked signal. As a result, Statistical Rejection was used to process the signal as it is more stringent than Overlapping Ensembles when most of the recorded stacks are relatively clean. During the Statistical Rejection process, the dipole waveform was analyzed by half-period increments and all segment of the signal showing statistically abnormal noise levels were discarded. The remaining portion of the waveform was then stacked. This technique was particularly effective for injections where a low count of stacks showing high noise levels was observed.

The total integrated chargeability was computed as the sum of each normalized secondary voltage multiplied by the length of its sample interval, divided by the total sample interval (i.e., 1.9 s for the 2 seconds time-base data). In the case of the Reed-Robinson data the apparent chargeabilities were calculated using a reduced integration window (220-1940ms). All georeferenced results for this survey were provided in UTM Z17N WGS84.

Following is a general description of the workflow for the daily processing, verification, and imaging of the survey data.

- The time series data that were stored on the individual receivers were downloaded to the processing computer at the end of each production day. Each file was a self-sufficient fully described file which contains all meta-data, including location, time, and recording units.

- Once downloaded, these individual signal files were loaded into the Dias Processing Software environment for dipole creation and stacking:

    - Dipoles were generated based on a range of lengths input by the user (i.e. all receivers within that range of lengths were paired up to form dipoles). The choice of lengths depended on the receiver station spacing, both along and across lines. It is customary to generate dipoles that extend over 2x the station spacing both along and across lines. Two approaches were available:
        - Blanket dipole generation: all possible dipoles between the minimum and maximum dipole lengths are generated using all available receivers for each injection. This option generates the maximum number of dipoles and is well suited for medium to high resistivity environments. It is also the most computer-intensive and lengthy option.
        - Smart dipole generation: the user enters a minimum and maximum dipole length for the close-offset dipoles. This range will be adjusted automatically to increase with the distance to the current injection. This option allows to maximize the signal/noise ratio and is best suited for more conductive environments. It also minimizes computing time, focusing on generating dipoles that will yield the strongest possible signal.
    - Where no data irregularities were encountered, the data were processed using proprietary processing algorithms that stacked the data, applied noise reduction strategies, and computed apparent resistivity and chargeability.
    - The error on the Vp was also calculated during this step. It was based on the mean difference between the sampled values over the window used for the Vp calculation and was designed to represent the stability of the signal. The same was done for the current and the combination of the two errors (Vp error/I error) was assigned as the error on apparent resistivity as used by certain inversion algorithms (UBC GIF for example).
- The resulting data were then concatenated in a single database where they could easily be displayed for verification, processing, and visualization.
- The processed data were organized by their respective survey grid and displayed in a point-cloud format along with all other data from that grid.
- Data quality control included an assessment of the following outputs and factors:
    - Locations: all receiver/transmitter locations, including elevations, were compared to corresponding hand-held GPS locations to ensure consistency. Grid coordinates were assigned to each survey station. Occasionally, the GPS elevations were replaced by elevations extracted from a NTS digital elevation model1.

  - Transmitter current stability: the amplitude of the injected current needed to remain stable over the course of the reading. If the injection were to vary or become abnormal the signal could be trimmed to only retain the sound portion of the injection
  - Waveform stacks: gave a quick snapshot of the signal/noise ratio
  - Spectral analysis: represented the signal in frequency domain to identify the frequency associated with potential cultural noise (power lines in particular) so proper signal procedure could be devised
  - Final decay: during the QC process the data set was run through a Cole-Cole rejection algorithm and the decays that were deemed untrustworthy were automatically rejected. During this process the Mx error was calculated based on the standard deviation of the measured decay relative to its Cole-Cole fit. Note that once the Cole-Cole rejection was complete the rejected decays were inspected one-by-one. Most rejected decays received further signal processing such as statistical rejection or ensemble stacking to try and eliminate the potentially bad cycles responsible for the noise in the decay. This technique reduced manual quality control time while maximizing data recovery.
  - Resistivity statistics: the rho values were plotted versus their corresponding mx values to obtain an estimate of the general data distribution. Any tailing values (i.e. very high/low rho/mx) were then automatically rejected.
  - Measurement point clouds: a final visual check was carried out on the data to ensure that the data looked consistent and detected potential inconsistencies in the data distribution. Individual data points in the point clouds could be analyzed interactively to determine the source of any irregularities.
  - Geometry testing: the coupling angle was calculated between the receiver and transmitter dipoles and was compared to the Vp values for each dipole. The poorly/null coupled zone was based on the value of the coupling angle beyond which the Vp value was deemed untrustworthy.
- Final processed data were exported as Dias and Geosoft formats as well as xyz point cloud in UTM Z17N/NAD83 coordinates.

After a thorough quality control, all the “accepted” data were used to produce a set of unconstrained 3D DC and IP models using the SimPEG inversion code (version 1.4 - https://www.simpeg.xyz/).

Following is the general procedure for producing the 3D models:

1. Carry out preliminary unconstrained inversion using a coarse mesh to establish the inversion parameters and identify any remaining data quality issues. The coarse mesh cell size of 1/2 of the closest nominal spacing between receiver electrodes in the horizontal direction. Vertical cell size increases progressively at depth to mimic the loss of sensitivity with a minimum size of ½ of the horizontal cell sizes.

2. Re-process or remove any data points that came up with high residual in the coarse mesh inversion and modify inversion parameters as required based on the results of step 1.
3. Carry out final unconstrained inversion using a fine mesh to yield the final 3D models. The fine mesh size is normally 1/4 of the closest nominal spacing between receiver electrodes in the horizontal and vertical directions
4. Modify the inversion parameters as needed to improve the model results until the fine models are considered acceptable.

A flat standard deviation error combined with a floor were assigned as uncertainties for both DC (error = 15% and floor = 10th percentile) and IP (error = 15% and floor = 1e-5mV/V) inversions. The DC inversion was carried out first followed by the IP inversion and both inversions used uniform backgrounds. The final DC model was used for the IP inversion. IP inversions were carried out with trimmed (220-1940ms) integration windows.

The inversions were carried out in UTM coordinates, and the current remote was included in the inversion calculation. Both coarse and fine inversions were carried out using topography incorporated into the inversion using the same NTS DEM used to update the survey elevations.

Once an inversion was completed, all iterations were examined independently, and the most suitable models were chosen. The model whose 'achieved misfit' was closest to the amount of data points used in the inversion were delivered as final model.

The resulting models were gridded and trimmed using Geosoft Oasis software and then converted into the UBC-GIF Tensor Mesh, XYZ-cell centered and Geosoft Voxel Format. The DC model is expressed in Ohm-m (resistivity model) and Siemens (conductivity model) and the Chargeability model in mV/V.

Results

The methods outlined in the previous section highlight empirical processes used to better define these geometrical and physical parameters of these anomalous zones and it is the opinion of the author and Dias Geophysical that the anomalous zones within the 3D models are reliable representations of the real and true electrical properties of the subsurface. Conductivity will be used exclusively in the interpretation of the results for clarity since conductivity and resistivity are the inverse of one another.

Analysis of the 3D conductivity and chargeability models reveal five zones with conductivity and chargeability features that may be indicative of mineralized veins or structures. Each potential zone is described in detail below starting in the west and moving east through the greater Reed-Robinson claim package. There is confirmed presence of graphite layers throughout the property which makes interpretation of conductive layers challenging because both graphite and sulphide mineralization are good conductors and can be chargeable.

The western most portion of the survey, Lease 108932, has relatively contiguous distributions of conductivity and chargeability values. The high chargeability values are concentrated near surface in the southern portion of the lease, creating a feature that strikes mostly east to west and then at the southeast corner of the lease begins striking north south through claim 192312. There is a large contiguous distribution of moderately high conductivity values firmly beneath the chargeability feature with almost no significant overlap. The conductivity values are stronger with depth and are strongest on either side of the 108932-192312 inside corner. The appearance of this conductive feature suggests that the conductive body is located off the greater Reed-Robinson claim group south of lease 108932 and west of claim 192312. The lack of overlap between the conductivity and chargeability features here is discouraging, however in the center of Lease 108932 there is a small discrete conductivity anomaly that overlaps precisely with a similar sized chargeability signature. The 108932 chargeability-conductivity feature (Figures 4 and 5) indicates that there may be a concentrated pocket of mineralization or graphite accumulation there. This potential drill target is located at 561543.28E 5326966.41N 35m below surface.

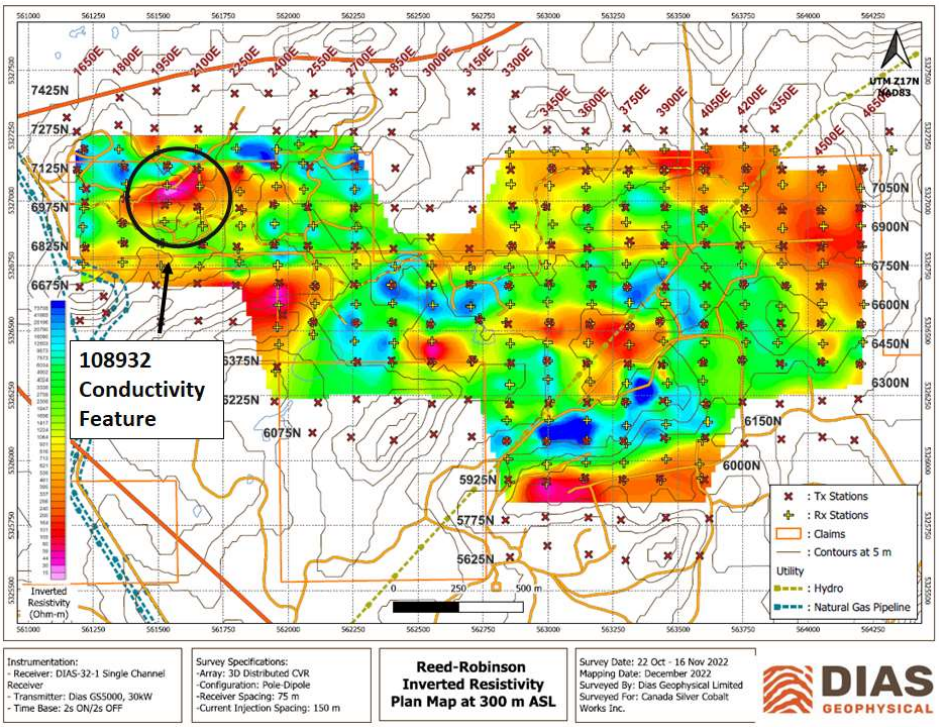


Figure 4.Resistivity plan map of 3D model at 325m asl, highlighting the 108932-conductivity feature

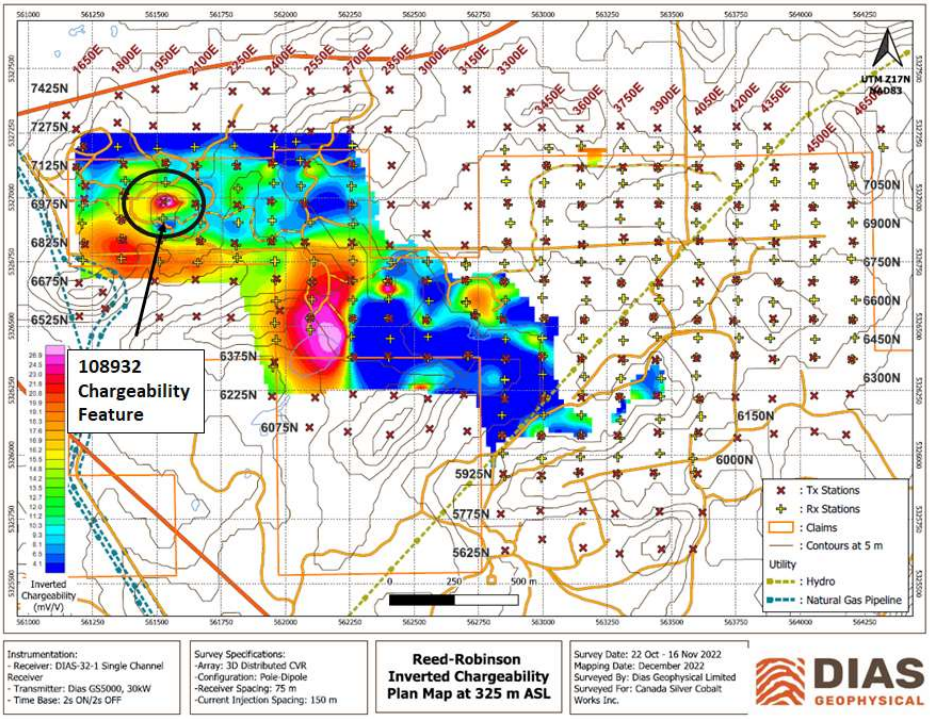


Figure 5. Chargeability plan map of 3D model at 325m asl, highlighting the 108932-chargeability feature

Moving east there is a large north to south striking feature of high chargeability values under claim 192312. This large linear chargeable feature occurs in an area of the gabbroic intrusion that is more conductive than it is to the East, although, the specific space occupied by the clear and distinct chargeability feature does not correspond to any anomalous conductivity values or features. The 192312 chargeable signal has two main 'cores' to it, a larger core with higher chargeability values to the south and a smaller core with lower chargeability values to the north (Figure 6). The relative magnitude and continuous nature of the signature could be indicative of sulphide mineralization along a vein, however the lack of overlapping dynamic conductivity values (Figure 7) indicates that it is instead an alteration or deformation zone that is contiguous for over 1km. This author interprets moderate background conductivity with strong and discrete spatially consistent chargeability to be caused by graphite accumulation in faults/deformation zones.

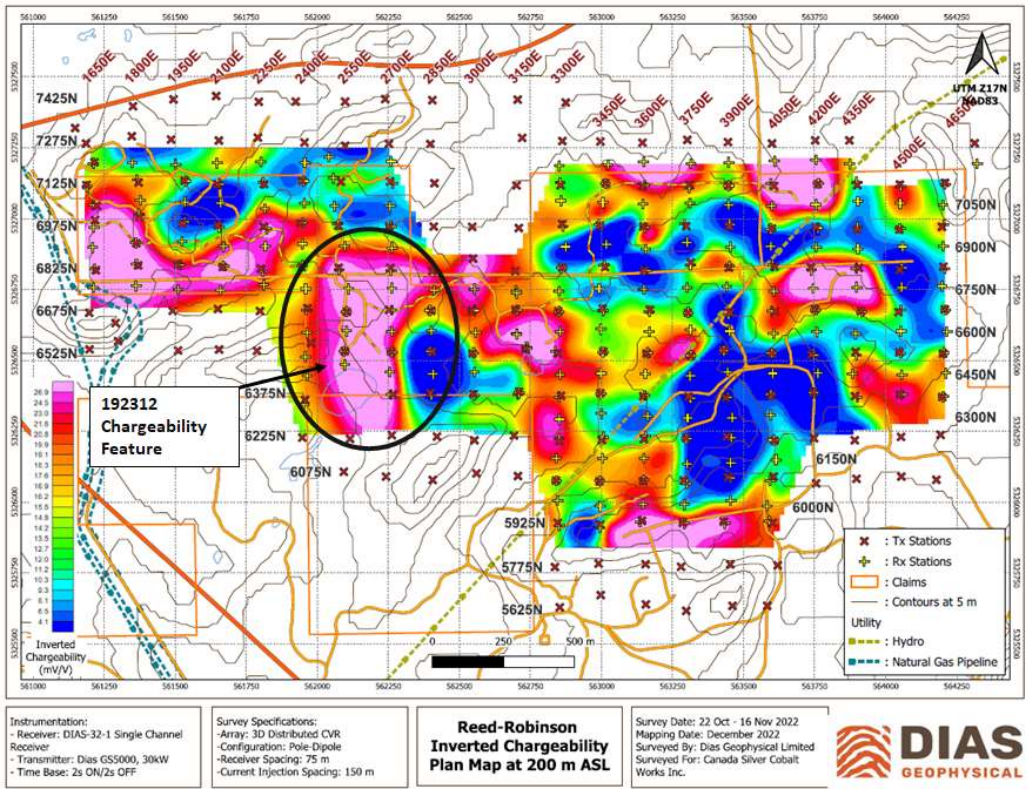


Figure 6. Chargeability plan map of 3D model at 200m asl, highlighting the 192312-chargeability feature

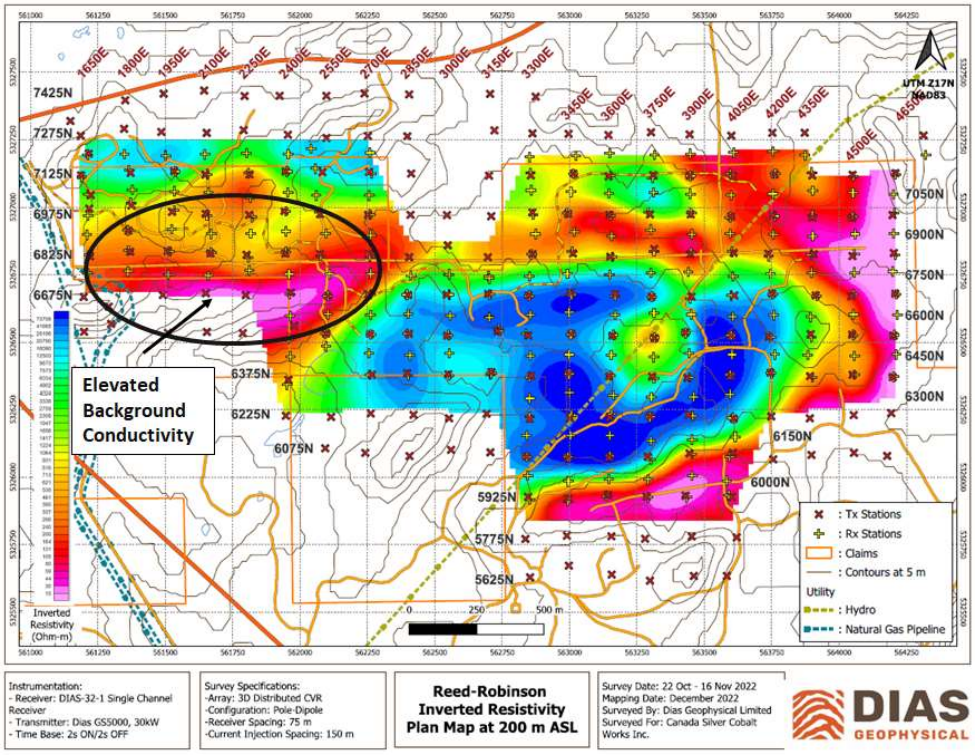


Figure 7. Resistivity plan map of 3D model at 200m asl, highlighting the regional elevated background conductivity

In the eastern portion of the greater Reed-Robinson claim package, under claim 122210 there is a discrete conductive anomaly near surface that trends East-West surrounded by a very low conductivity gabbro. There is a second, non-contiguous, smaller, slightly elongate conductive anomaly also trending East-West that is ~450m apart from the larger zone, center to center. The 122210-conductivity feature is the first, and larger anomaly (Figure 8) is more consistent with depth through the model, dipping north by northeast sharply towards a larger more conductive region at depth. A small chimney of moderate conductivity values extends between this near surface anomaly and what is likely the mafic metavolcanics at depth. The bridge occupies the same space as the Eastern edge of a large East-west trending chargeability signature that is very strong and consistent. The 122210-chargeability feature (Figure 9) runs through the highly resistive, bowl-shaped section of the gabbroic intrusion. It is the interpretation of this author that the east-west 122210 chargeability feature is likely a structure housing alteration and not mineralization. The Eastern most extent of the chargeability feature being directly under a strong conductive feature with overlap of both conductive and chargeable values is more promising. Drilling this target could reveal mineralization directly adjacent to deformation, allowing for the ground truthing of multiple electrical anomalies and optimistically finding economic quartz-breccia-hosted gold. Both feature's centers are located at 563249.32E, 5326504.18N, 50 m below surface for the conductivity anomaly and 188m below surface for the chargeability feature.

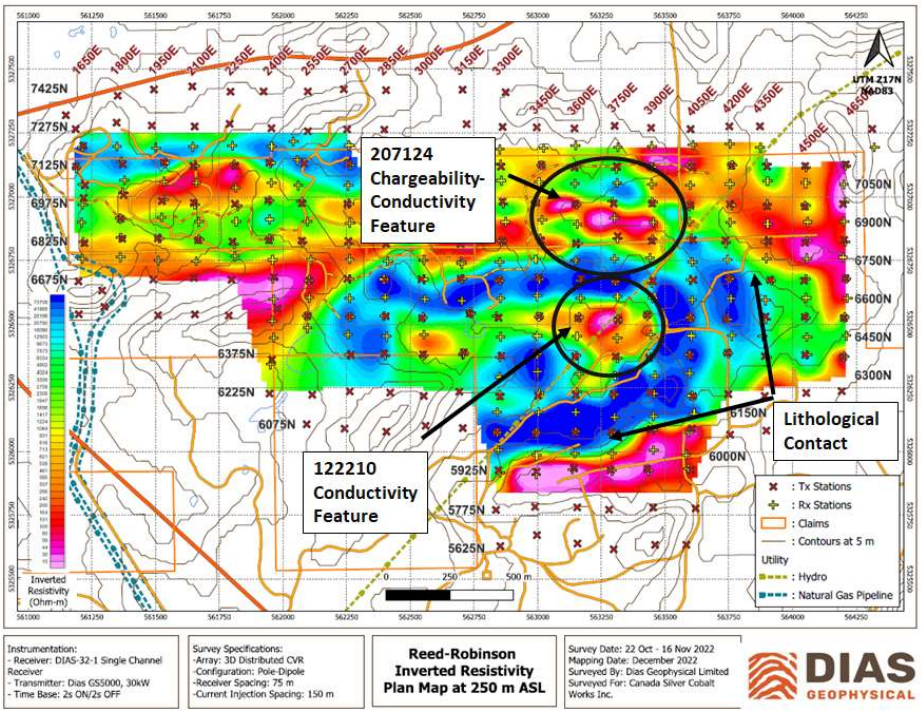


Figure 8. Inverted resistivity plan map of 3D model at 250m asl, highlighting the 122210-conductivity feature, the 207124-chargeability-conductivity feature, and the gabbroic intrusion, mafic metavolcanic lithological contact at depth.

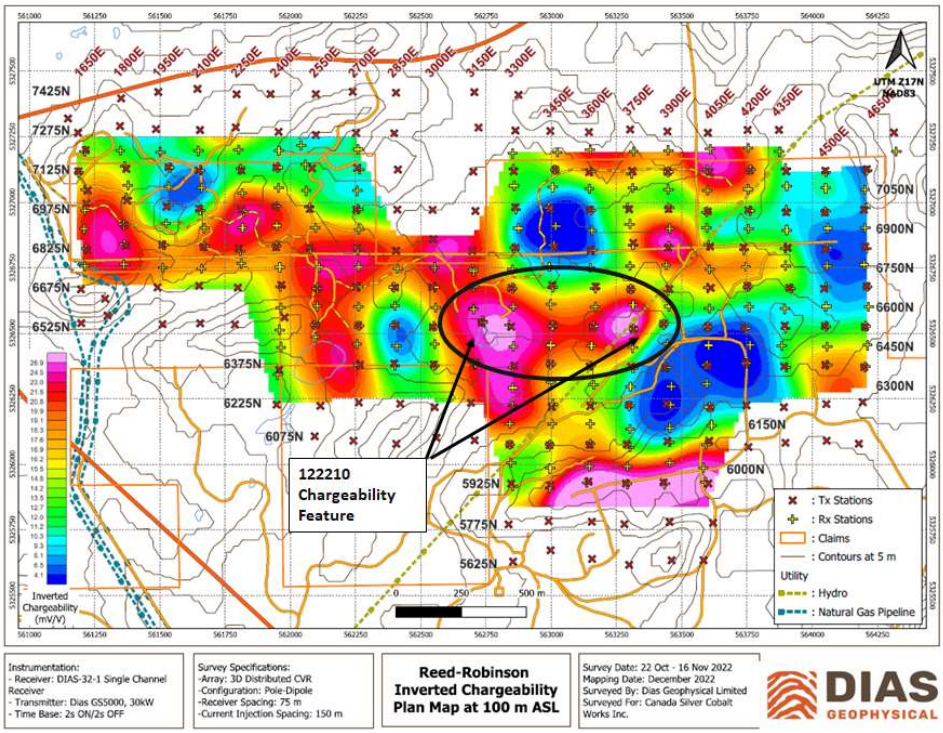


Figure 9. Inverted chargeability plan map of 3D model at 100m asl, highlighting the 122210-chargeability feature.

Under claims 310340, 207124, and 266415 there is a similar southeast-northwest trending series of conductive and chargeable anomalies. Here, neither the chargeability nor conductivity anomalies are contiguous by themselves, but together they create a consistent mosaic of strong electrical signatures that in some areas overlap (Figures 8 and 10). This collection of anomalies runs parallel to the northeastern contact between the gabbro and metavolcanics, 170m to the southwest. This 207124 conductivity-chargeability feature is interpreted by the author to be either a heterogeneously mineralized vein or graphitic structure. The feature trends in a straight line from 563007.31E 5327004.71N at 61m below surface to 563736.57E 5326707.21N at 88m below surface.

Moving to the southern edge of lease 108930, there is a series of discrete chargeability

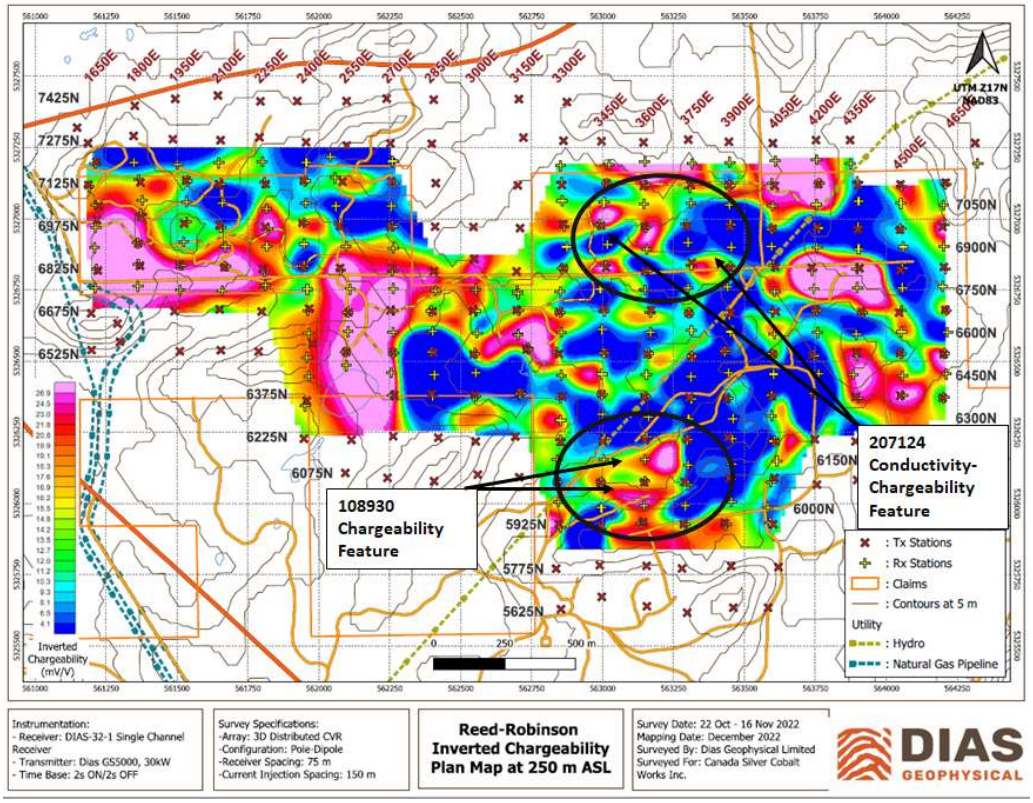


Figure 10. Inverted chargeability plan map of 3D model at 250m asl, highlighting the 207124-conductivity-chargeability feature, and the 108930-chargeability feature.

anomalies (Figure 10) adjacent and parallel to a clear distribution of conductivity that corresponds with the gabbro-mafic metavolcanic contact. The conductivity signature along the southern edge of the lease goes from very low in the gabbro to high in the mafic metavolcanics (Figure 8). The difference in these measurements is a few orders of magnitude, and as such, the contact appears very sharp in the conductivity model and can also be seen all around the western extent of the claim package. The southern extent of lease 108930 is where the Eby-Otto fault extension is interpreted to be. From conductivity alone there is no indication of any mineralized structure here. The non-contiguous series of chargeability anomalies can be traced along the southern contact as

little blips separated by more than 100m at a time. The 108930 non-contiguous chargeability feature may be indicative of sporadic alteration or graphite accumulation along a contact fault if one does exist here. The lack of corresponding dynamic conductivity values that one would expect to see with graphite or mineralization may be in part due to proximity to the contact and its many orders of magnitude transition.

Recommendations

The data collected and the models produced by Dias Geophysical on behalf of the Company has tremendous value for characterizing the subsurface electrical properties of the entire greater Reed-Robinson claim package to depths of up to 400m below surface. Having access to this 3DIP and resistivity data in has been demonstrated to be very valuable information for the interpretation of the claims and for the determination of future drill targets. After thorough review of the data collection, processing, and 3D model production, and then comparing that information to geological data and interpretation, it is concluded that the Dias Geophysical 2022 Reed-Robinson 3D DCIP ground geophysical survey program met its original objectives of identifying future drill targets.

It is the recommendation of this author that, based on the interpretation of the 3D DCIP models, targets identified as the 122210 chargeability-conductivity overlap, and the 207124 conductivity-chargeability feature in the Eastern portion of the greater Reed-Robinson claim package be considered as drill targets for future drill programs. Drilling these targets would be done with the aim of investigating possible mineralized and altered veins/structures that have potential to host economic amounts of gold. Furthermore, it is recommended that the Dias geophysical 3D DCIP ground survey be extended to neighbouring claim packages that the Company is currently optioning from other claim holders. Extending the surveys will allow for greater context on the Reed-Robinson claim package and may increase the level of interpretation possible around the gabbro – mafic metavolcanic boundary.

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Certificate Of Qualification

I, Gerhard Kiessling of Wasaga Beach, ON, hereby certify that:

1. I am employed by Canada Silver Cobalt Works as Vice President Exploration.
2. I am the Qualified Person for this report entitled “Ground Geophysical Survey Work Report On A 3D DCIP Survey”
3. AT THE REED-ROBINSON CLAIMS (EBY-OTTO PROPERTY)
4. I hold the following academic qualifications: BSc. (Hons.) Earth Sciences, Geology Specialization, University of Waterloo (Waterloo, ON)
5. I am a registered member of the Association of Professional Geoscientists of Ontario (Registration # 3670) and received my PGeo designation in July 2022.
6. I have practiced as an exploration geologist (GIT or PGeo.) in Ontario, Alberta, and Nunavut since 2013.
7. I have worked on mineral exploration projects in the Abitibi Greenstone Belt since 2017, and am familiar with the host rock lithologies, alteration and mineralization styles, and deposit models typical of the Abitibi Greenstone Belt.
8. I supervised the drilling and logging work reported in this assessment report.
9. I co-authored this report.
10. As of the date of this certificate, to the best of my knowledge, information, and belief, this report contains all scientific and technical information that is required to be disclosed to make this report not misleading.

Dated:

December 13 2022



Gerhard Kiessling, BSc., PGeo (Registration #3670)

Vice President Exploration, Canada Silver Cobalt Works



Expenses Incurred

Table 6: Cost breakdown for work completed

Item	Date From	Date To	Subitem	Rate / Unit	# Units	Cost
Geophysical Survey	22-Oct-22	16-Nov-22	Dias Geophysical - Invoice 1			$ 60,200.00
Geophysical Survey	22-Oct-22	16-Nov-22	Dias Geophysical - Invoice 2			$ 70,512.00
Geophysical Survey	22-Oct-22	16-Nov-22	Dias Geophysical - Invoice 3 (credit subtracted)			$ 116,075.00
Geophysical Survey	16-Nov-22	12-Dec-22	Dias Geophysical - Inversion			$ 16,000.00
Geophysical crew mobilization	22-Oct-22	16-Nov-22	Dias Geophysical - Mod/Demob			$ 25,000.00
Sheldon Ward	01-Oct-22	31-Oct-22	Line Brushing/Cutting (partial invoice)			$ 3,850.00
Sheldon Ward	01-Nov-22	27-Nov-22	Line Brushing/Cutting (partial invoice)			$ 2,240.00
Jordan Barrette	25-Oct-22	10-Nov-22	Line Brushing/Cutting (full invoice)			$ 4,175.00
Exploration Geologist	09-Dec-22	12-Dec-22	Report Writing	$ 50.00 / hour	40	$ 2,000.00
Senior Geologist	09-Dec-22	12-Dec-22	Report Writing & Review	$ 57.50 / hour	10	$ 575.00
Senior Geologist	24-Oct-22	08-Nov-22	Contractor Supervision	$ 57.50 / hour	70	$ 4,025.00
Pickup Trucks	24-Oct-22	08-Nov-22	Travelling to site to supervise contractors	$ 100.00 / day	70	$ 7,000.00
Vehicle Mileage - travel to site	24-Oct-22	08-Nov-22	Charge for gas and vehicle wear and tear	$ 0.50 / km	1414	$ 707.00
				TOTAL EXPENDITURES		**$ 312,359.00**

Appendices

Appendix A: Dias Geophysical Plan Maps and Sections

All 14 plan maps and 42 sections extracted from both the inverted 3D resistivity and chargeability models.

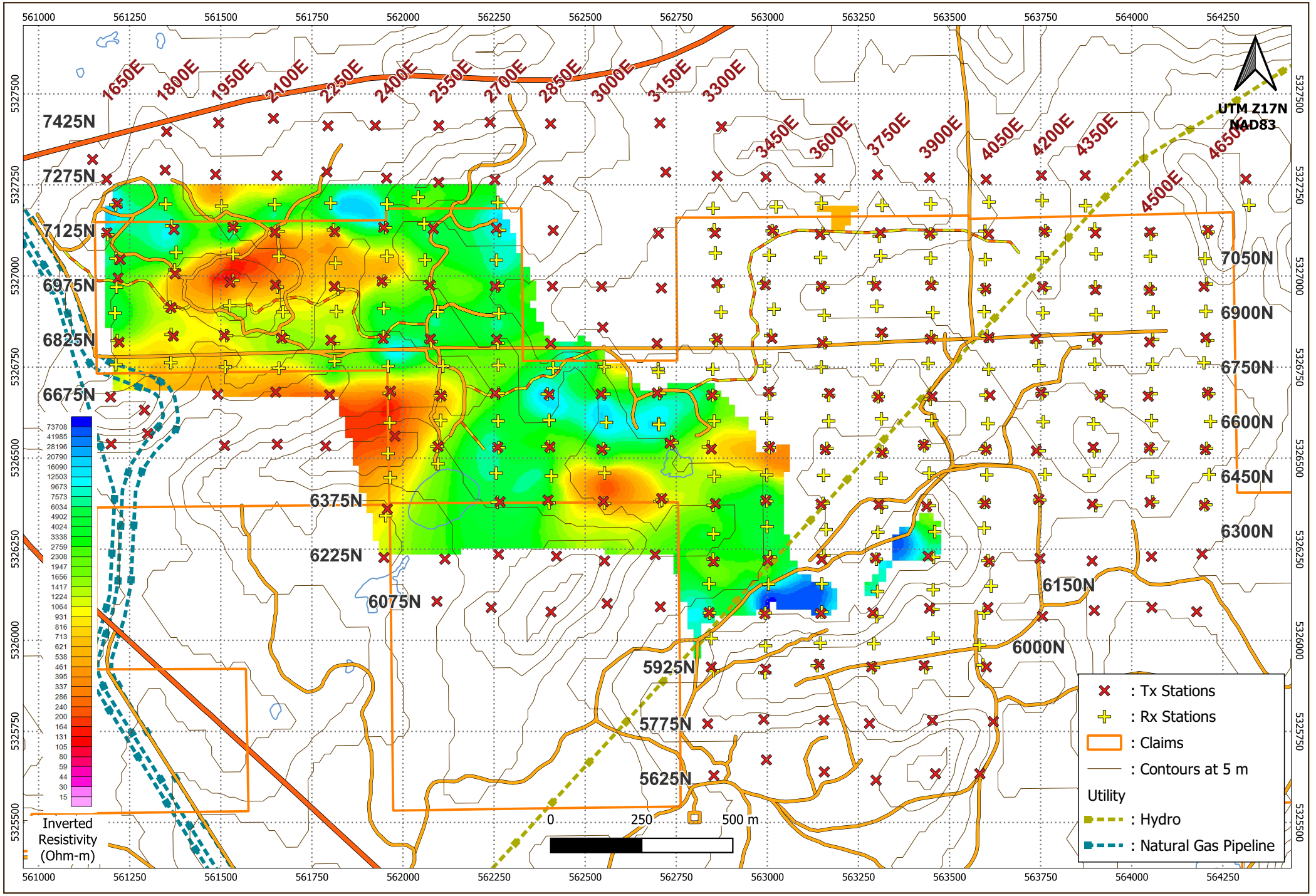
Appendix B: Dias Geophysical Logistics Report

A 26-page document reporting all field activity, survey methods/parameters, illustrative diagrams, and the data processing workflow.

Appendix C: Invoices

Appendix A

Dias Geophysical Plan Maps and Sections



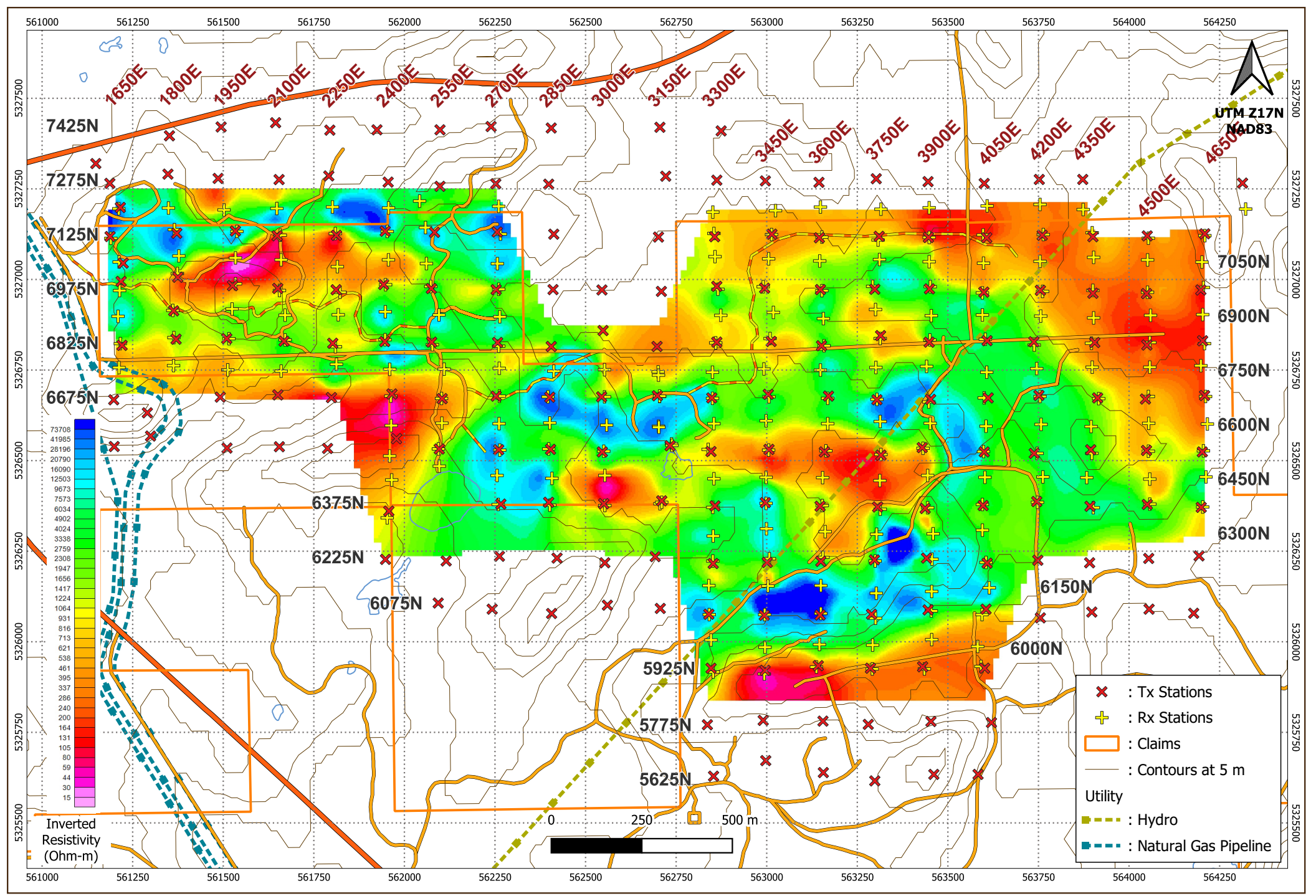
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at 325 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



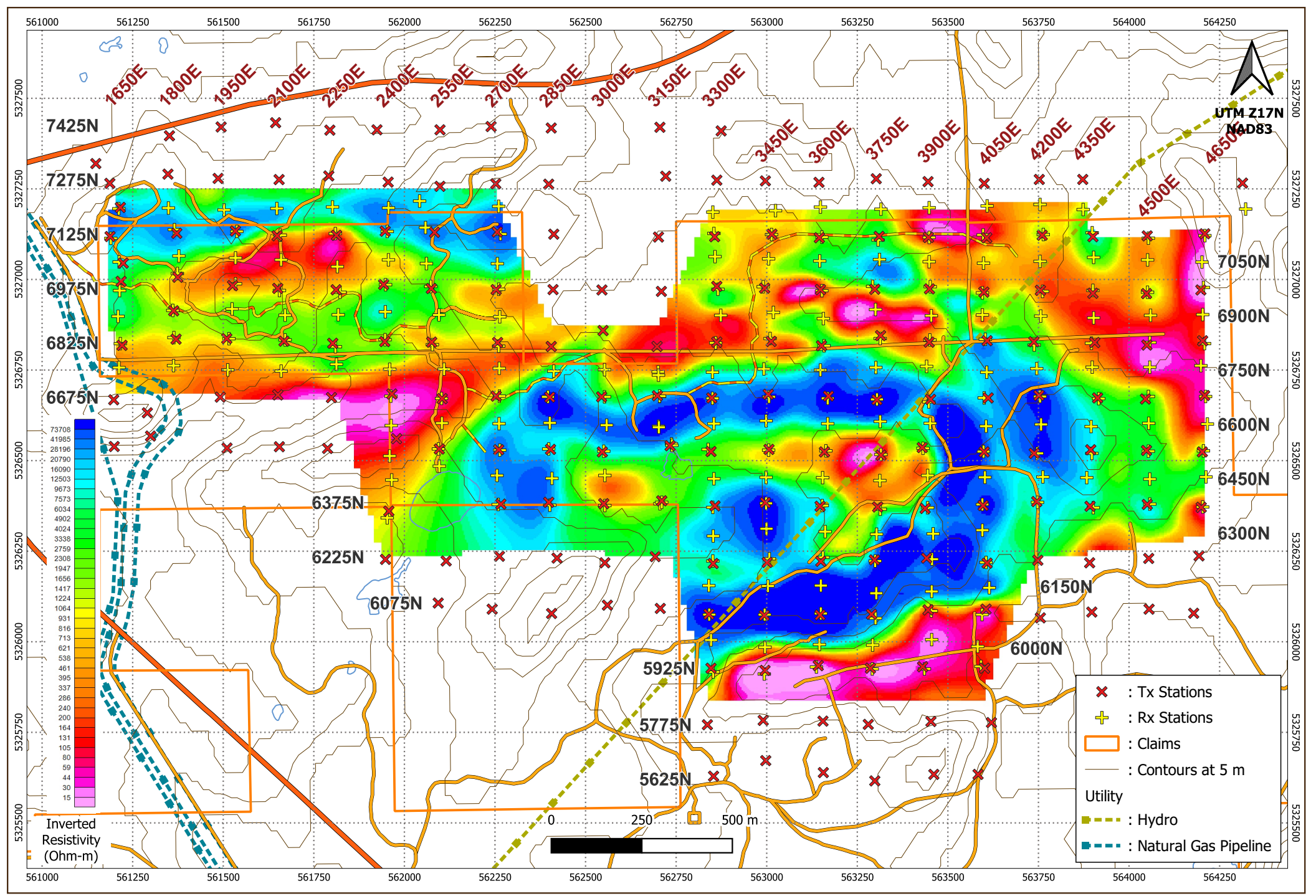
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at 300 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



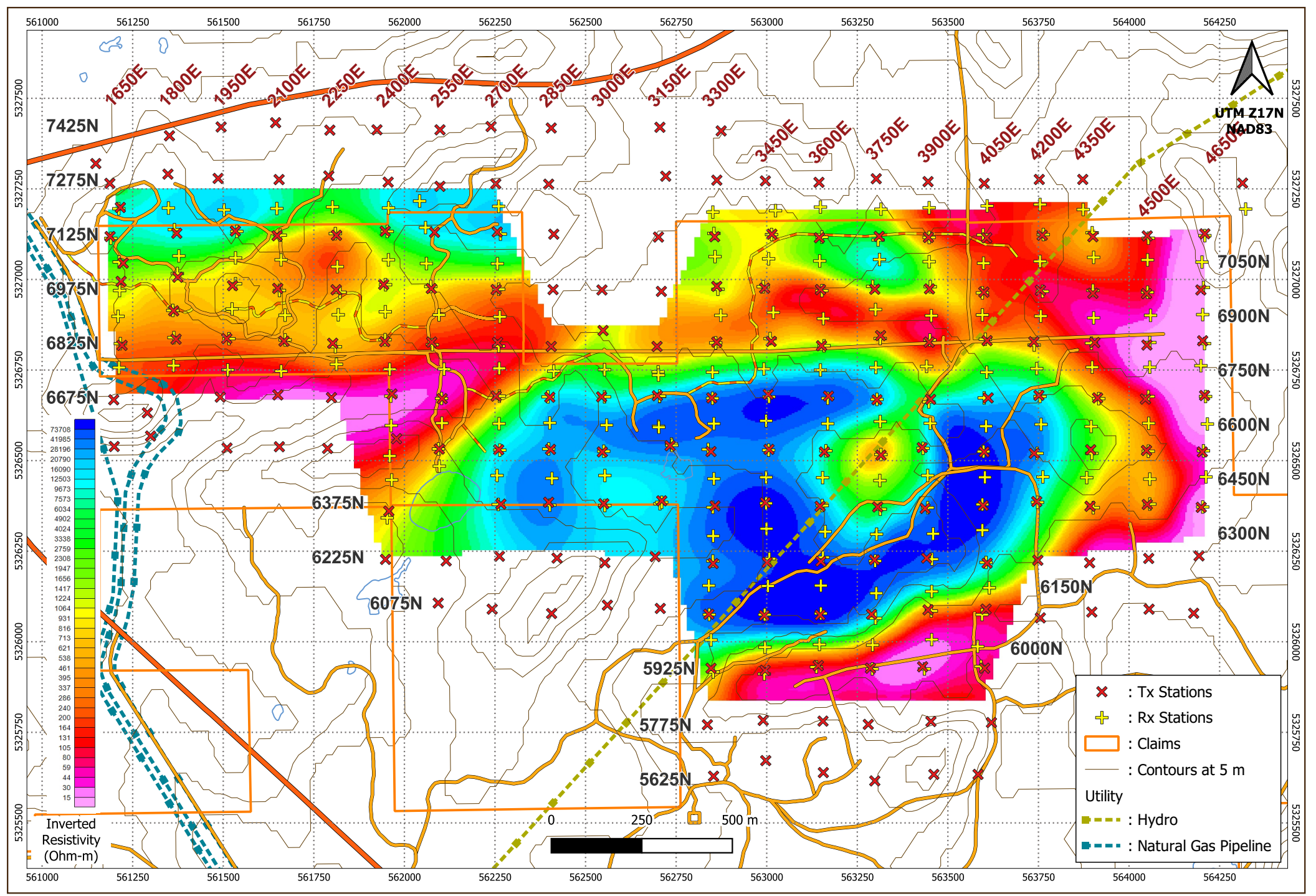
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at 250 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



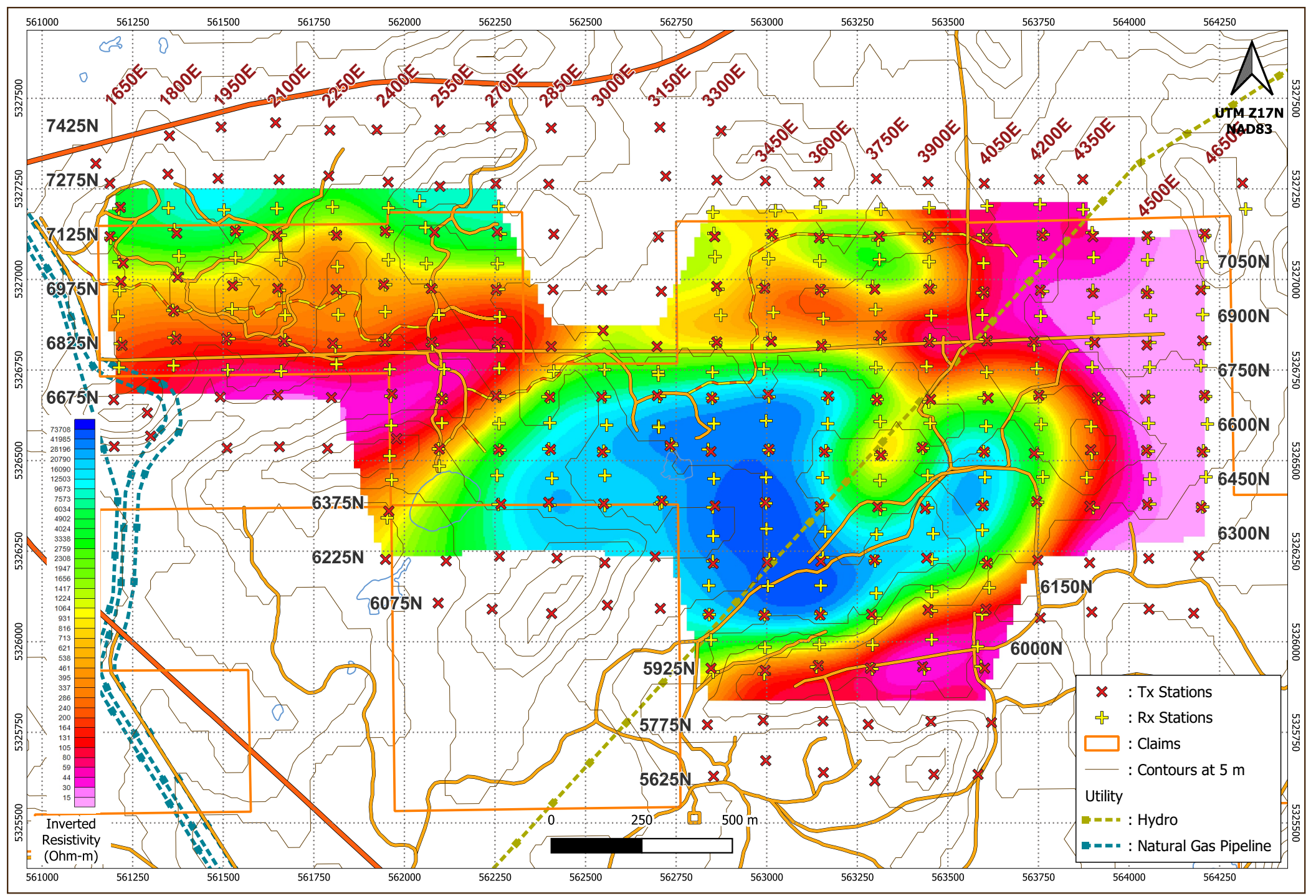
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at 200 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



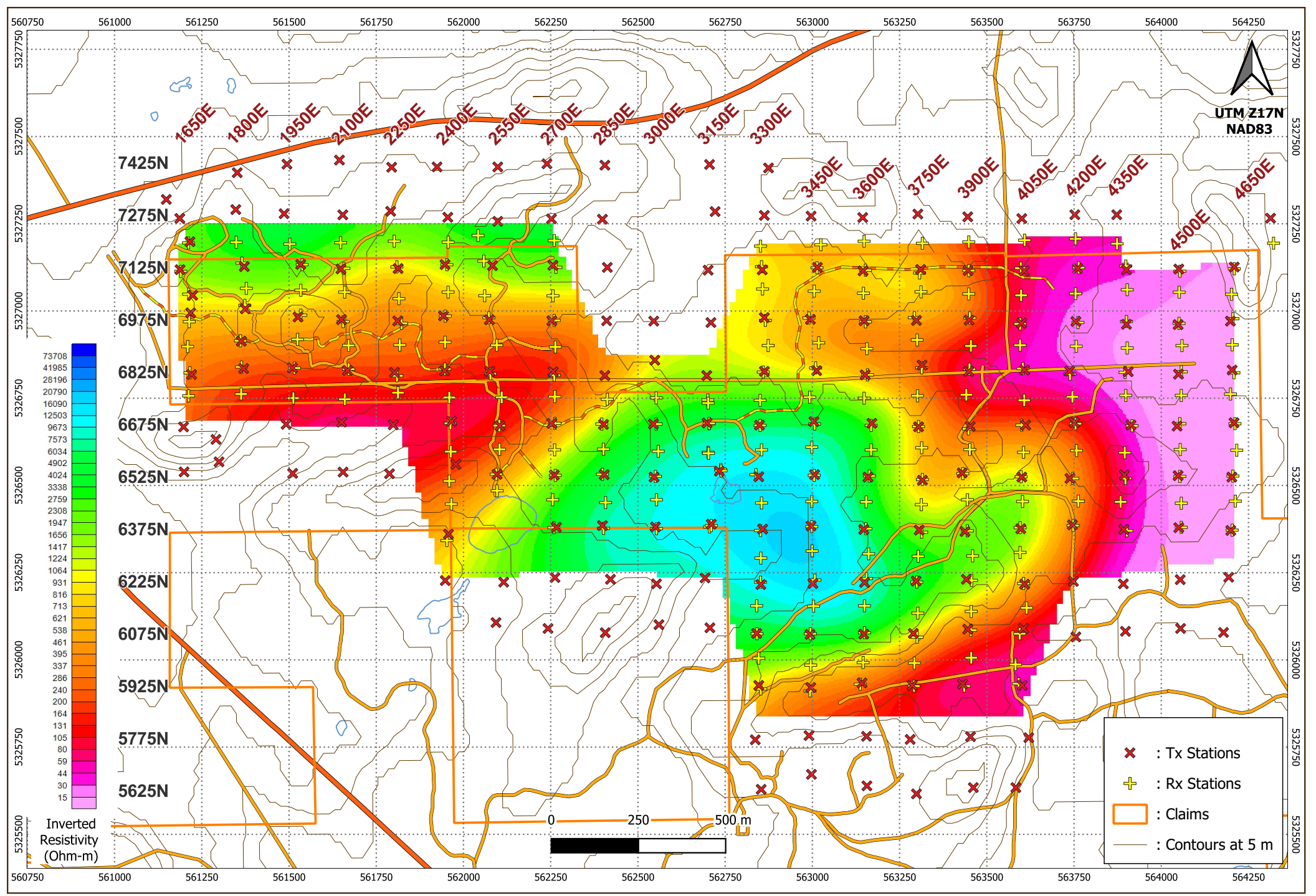
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at 100 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



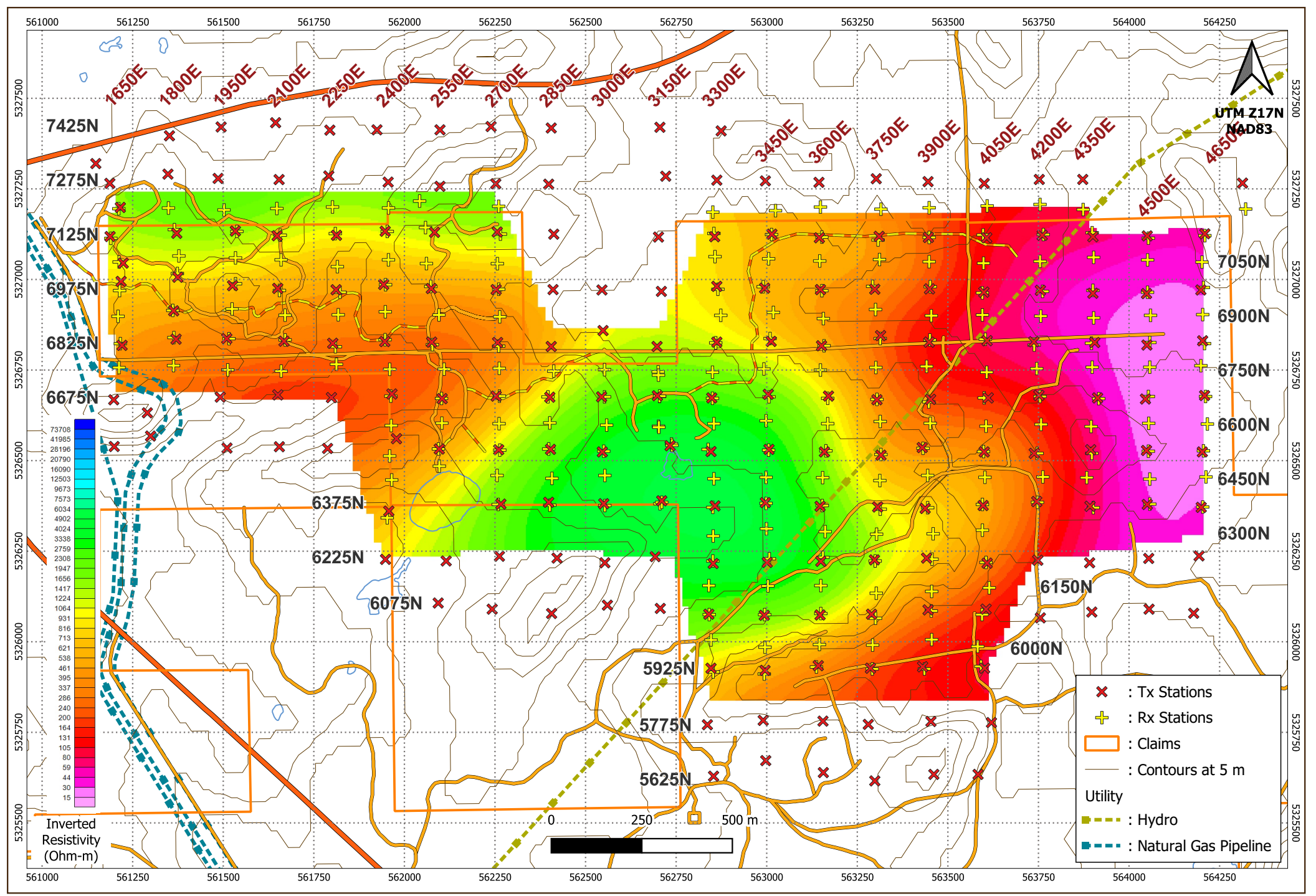
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at 0 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



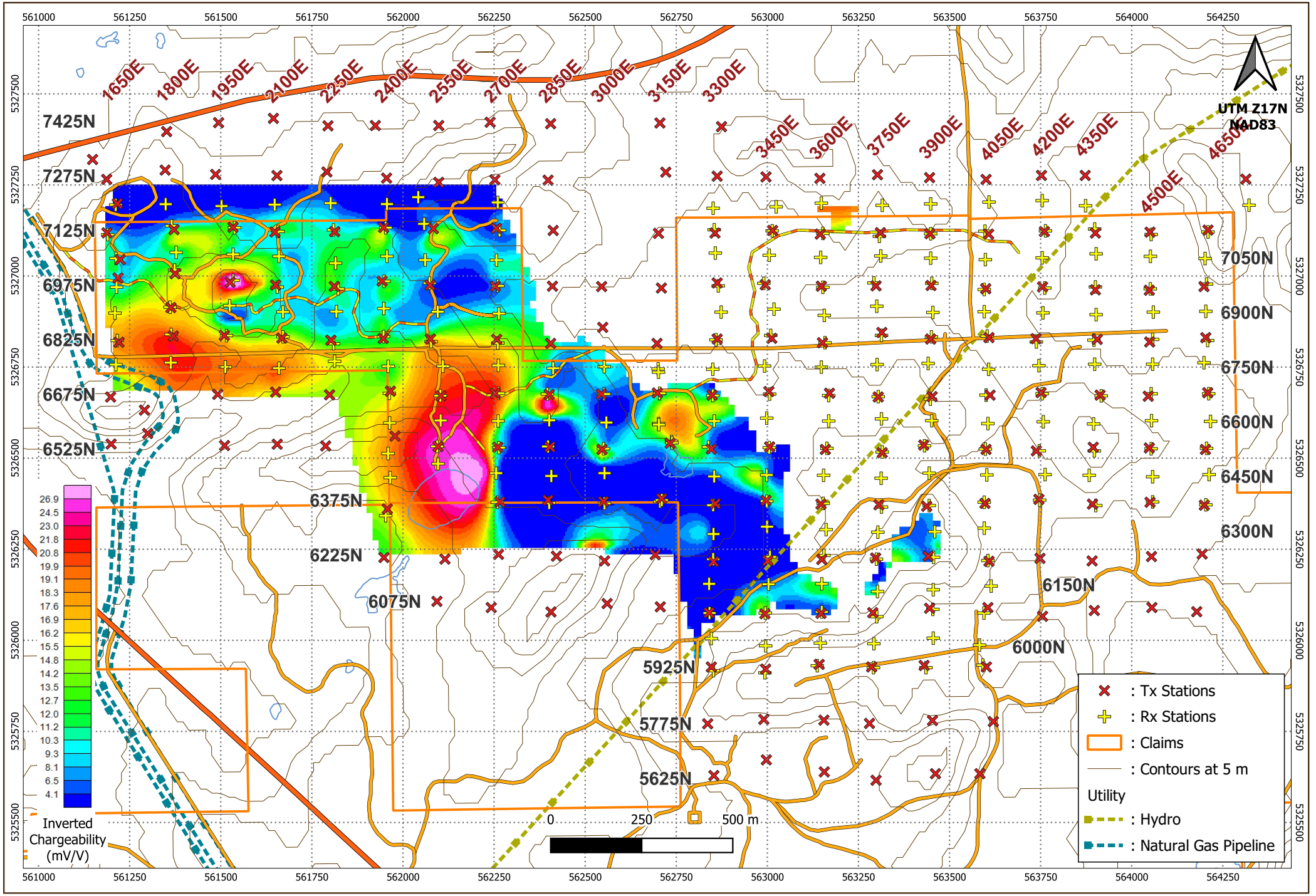
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Resistivity Plan Map at -100 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



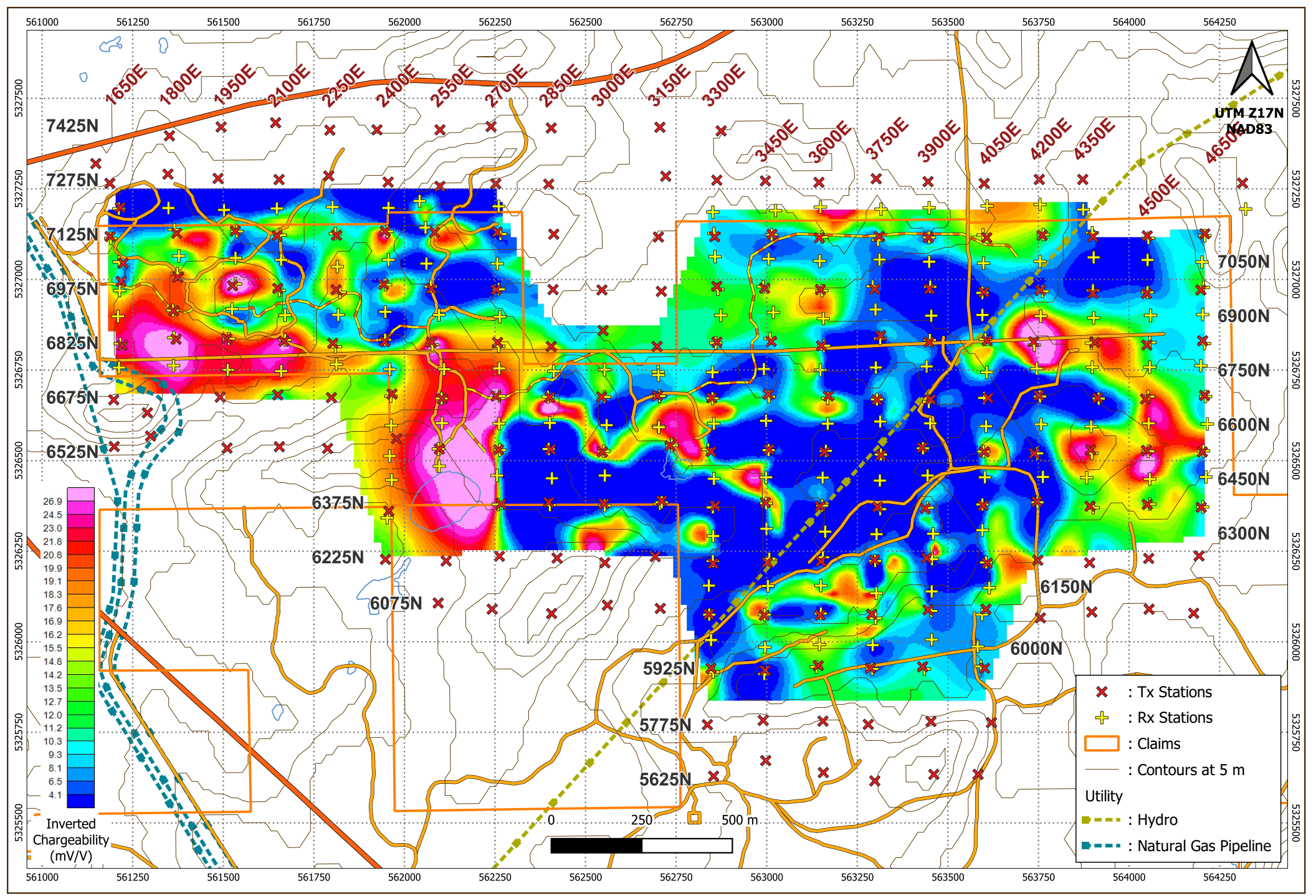
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Chargeability Plan Map at 325 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



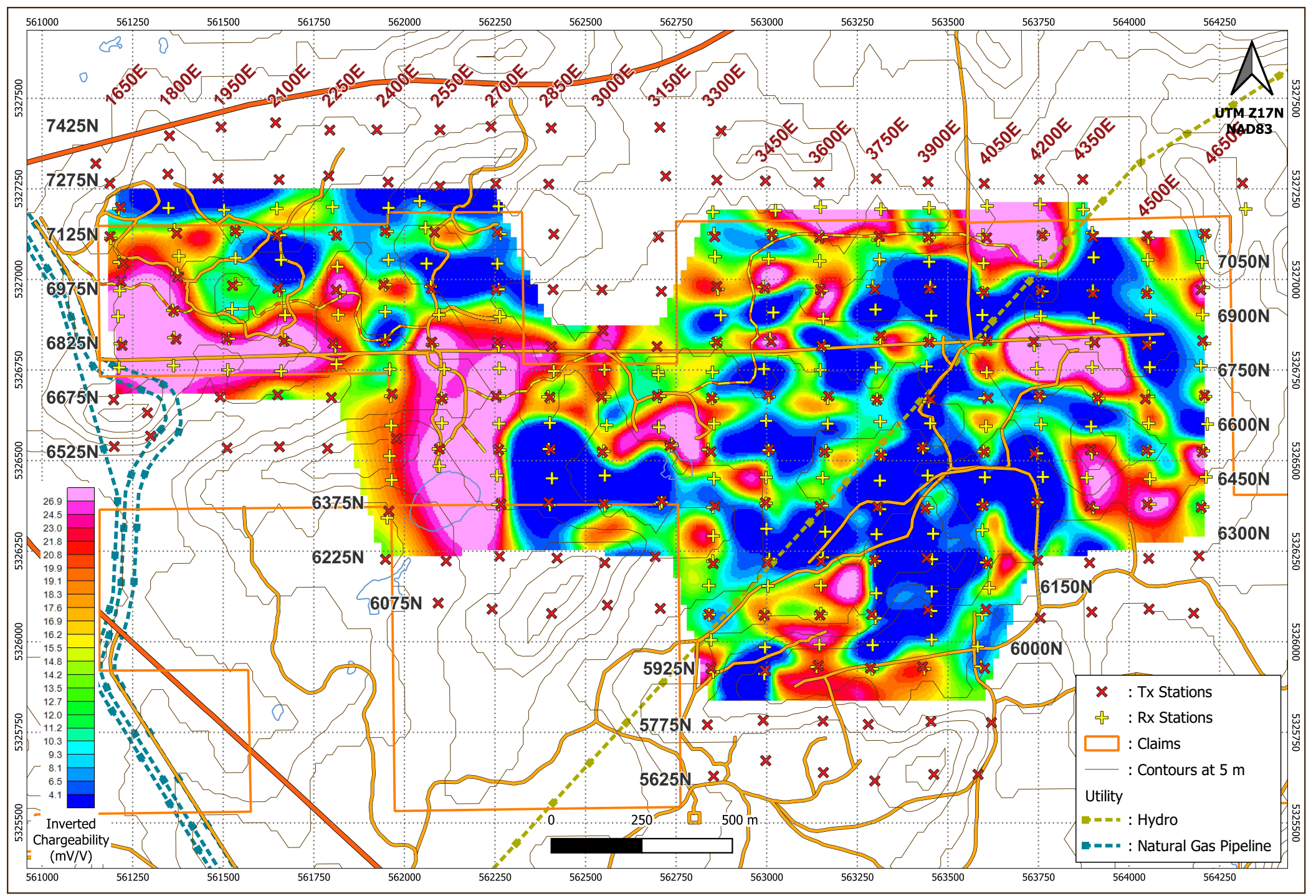
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Chargeability Plan Map at 300 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



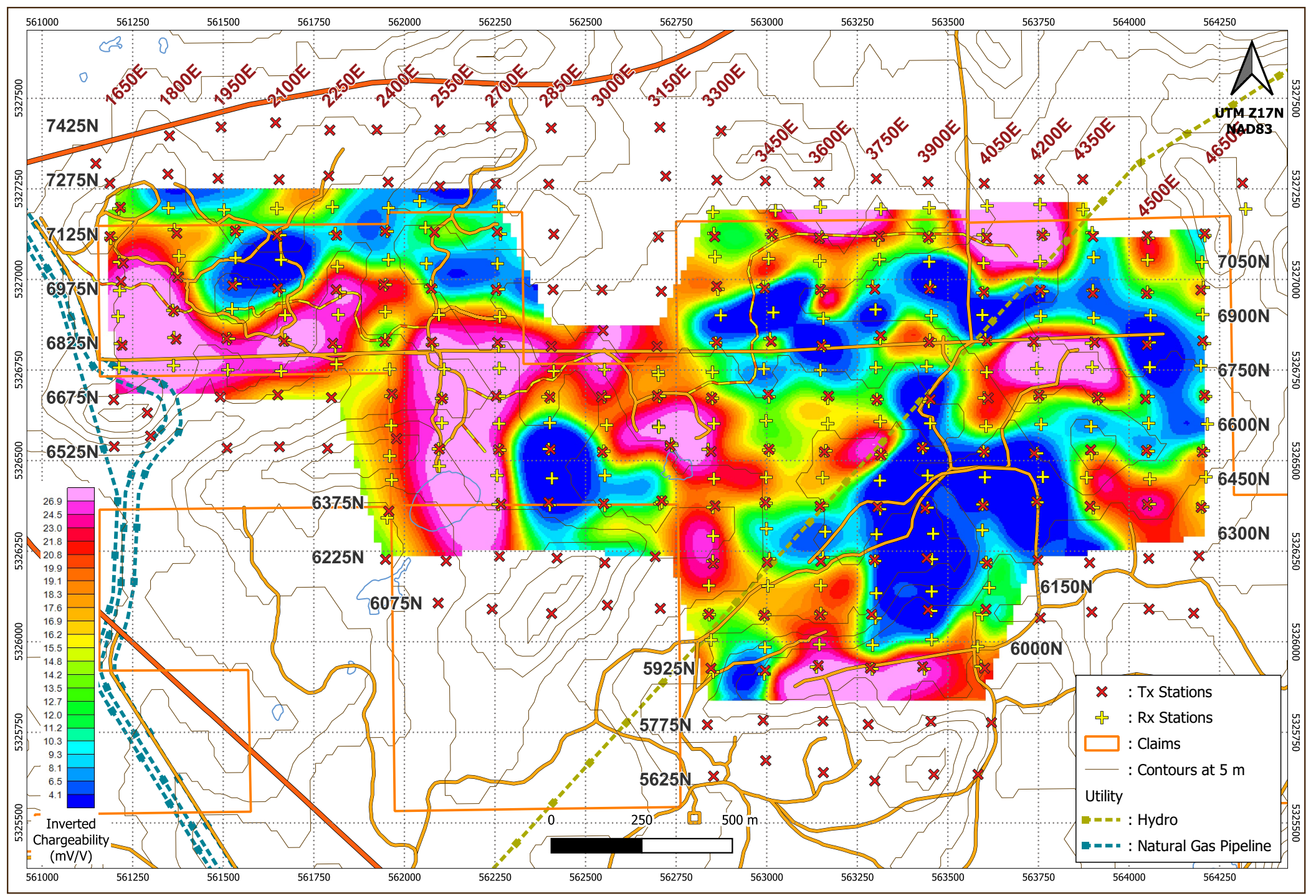
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Chargeability Plan Map at 250 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



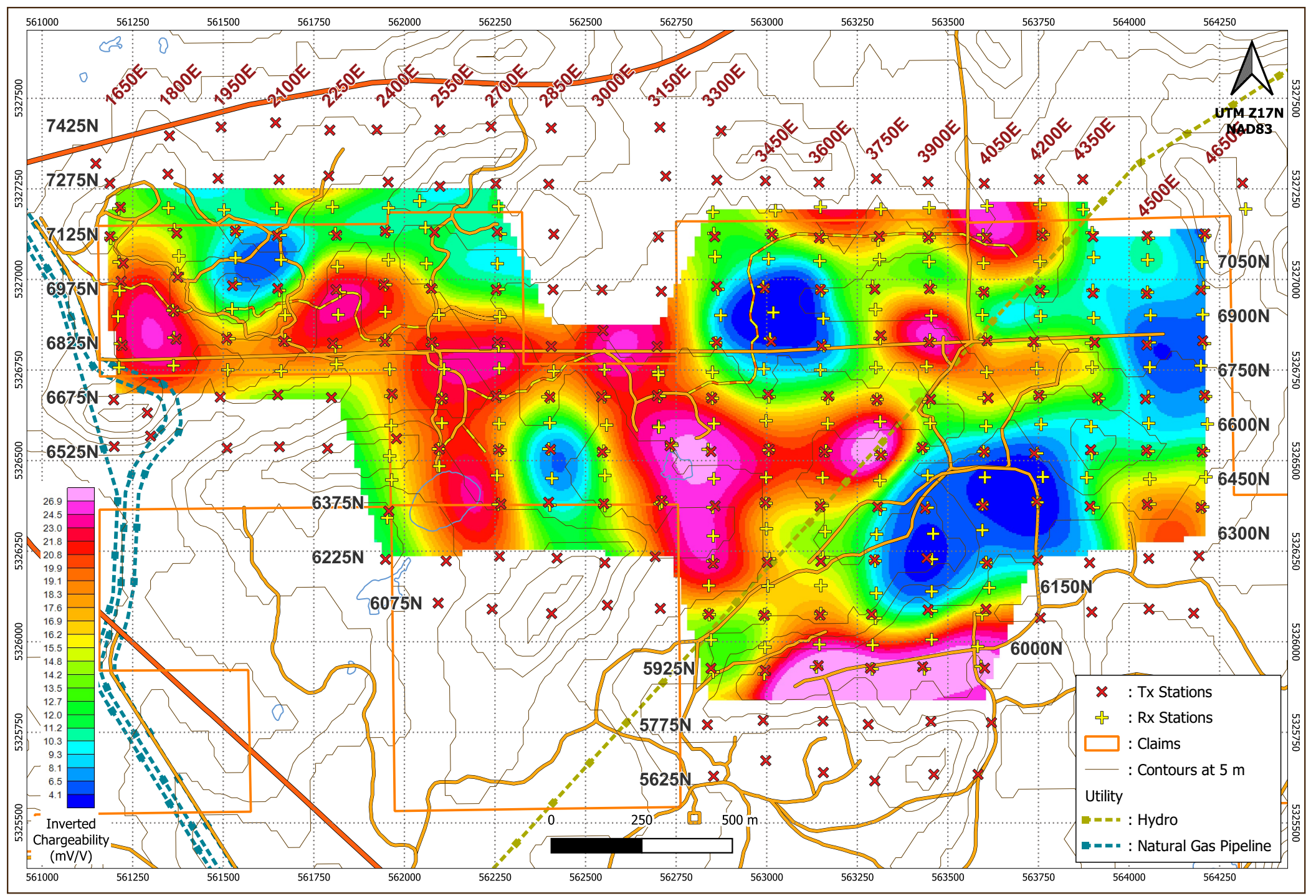
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Chargeability Plan Map at 200 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



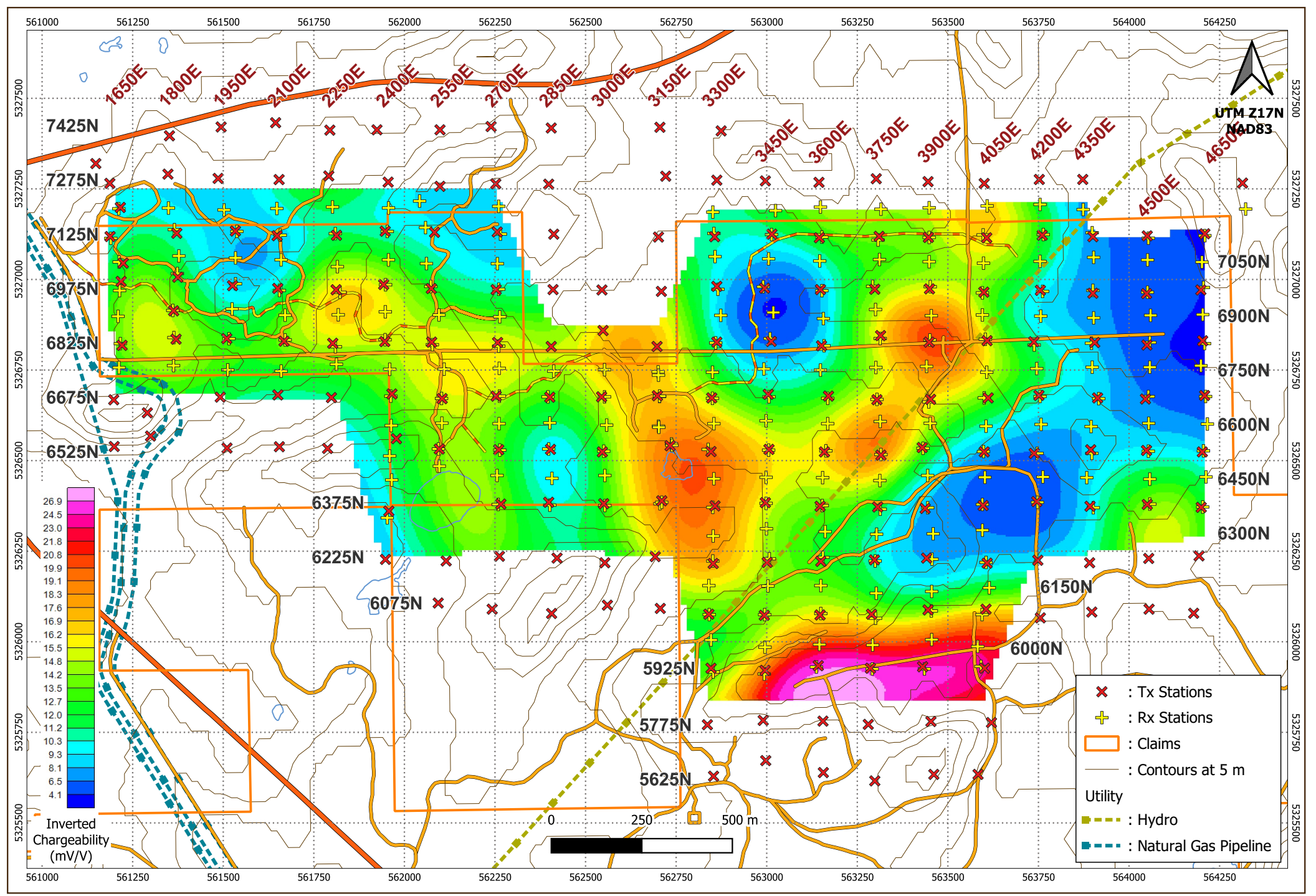
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Chargeability Plan Map at 100 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



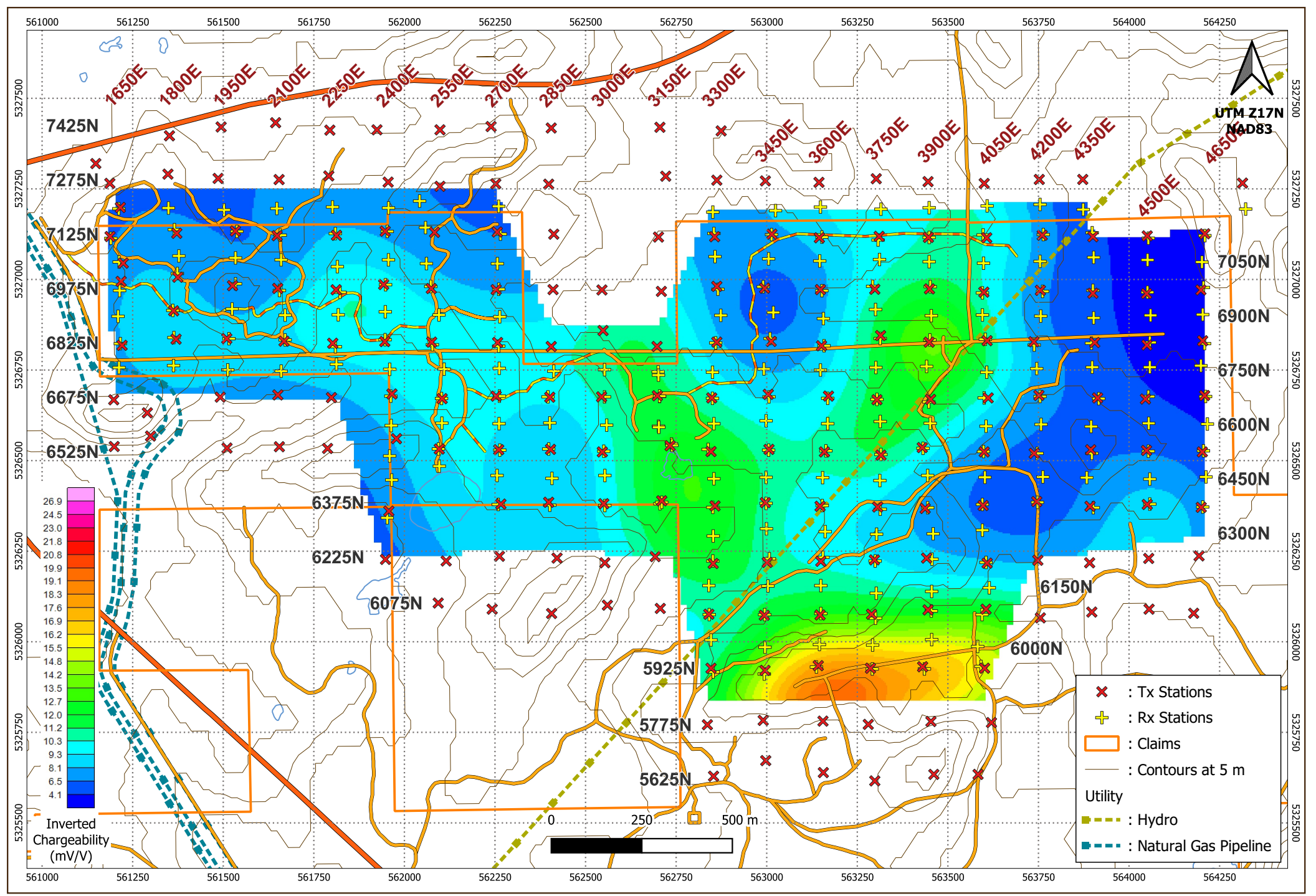
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Reed-Robinson Inverted Chargeability Plan Map at 0 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

DIAS GEOPHYSICAL



Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF

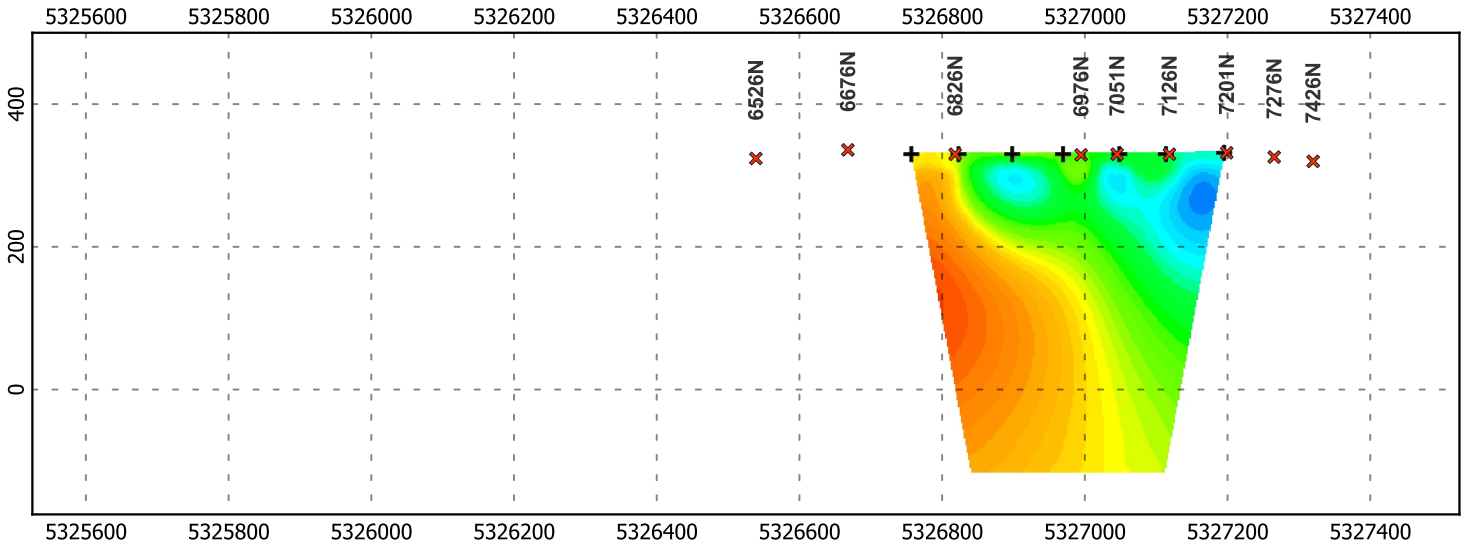
Survey Specifications:
-Array: 3D Distributed CVR
-Configuration: Pole-Dipole
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

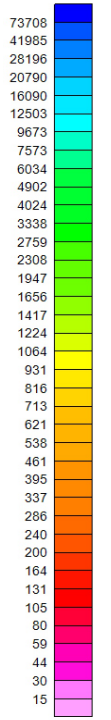
Reed-Robinson Inverted Chargeability Plan Map at -100 m ASL

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.

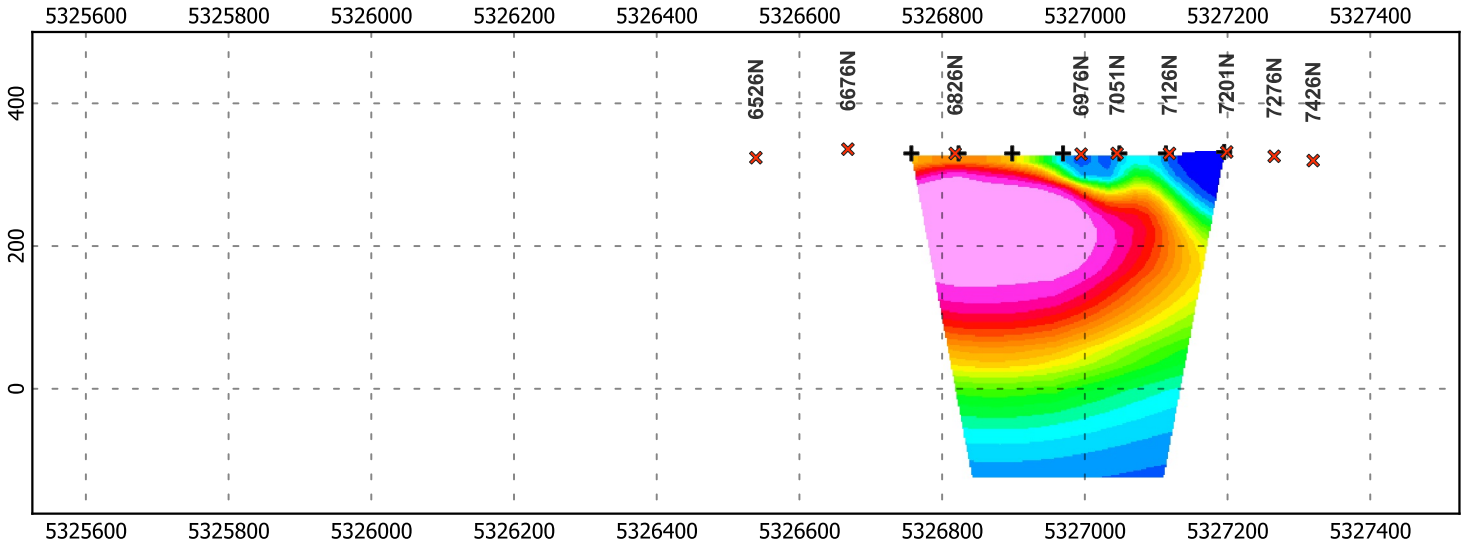
DIAS GEOPHYSICAL

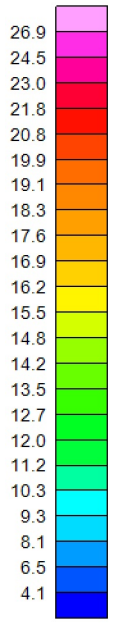
Inverted Resistivity





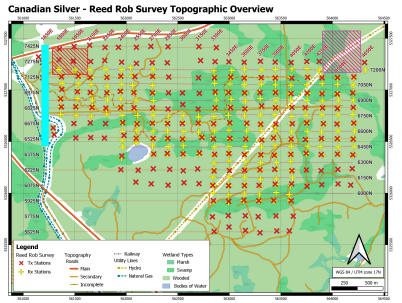
Inverted Chargeability





Reed-Robinson-L1650E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

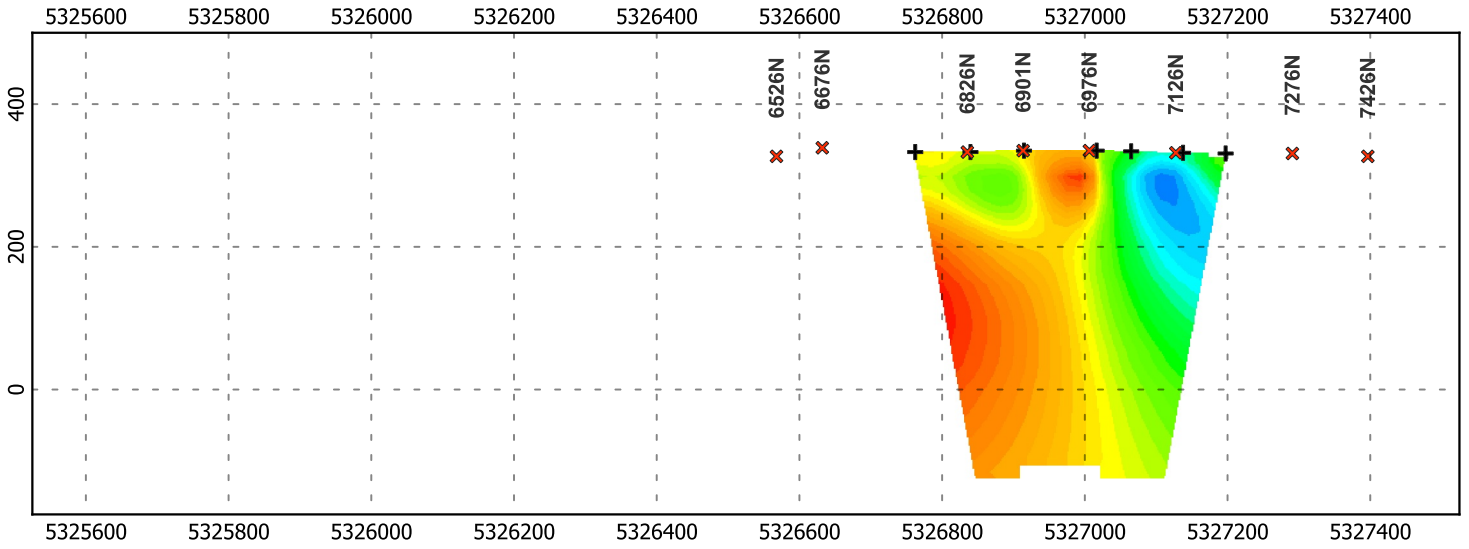
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

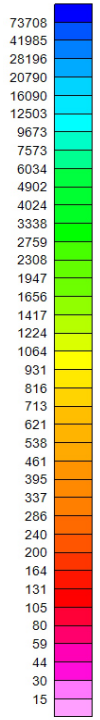
× Injection Stations
\+ Receiver Stations

0 100 200 m

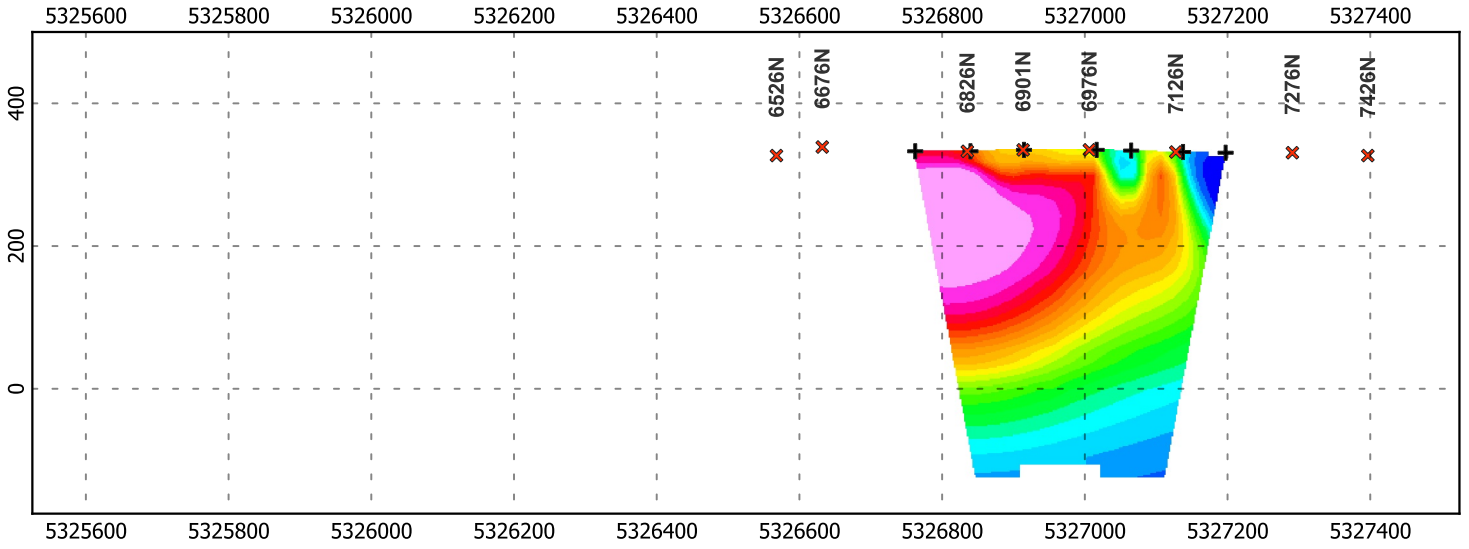
DIAS GEOPHYSICAL

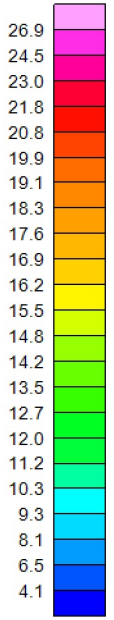
Inverted Resistivity





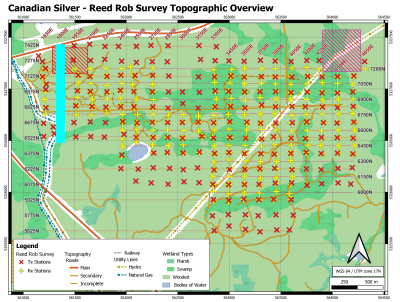
Inverted Chargeability





Reed-Robinson-L1800E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

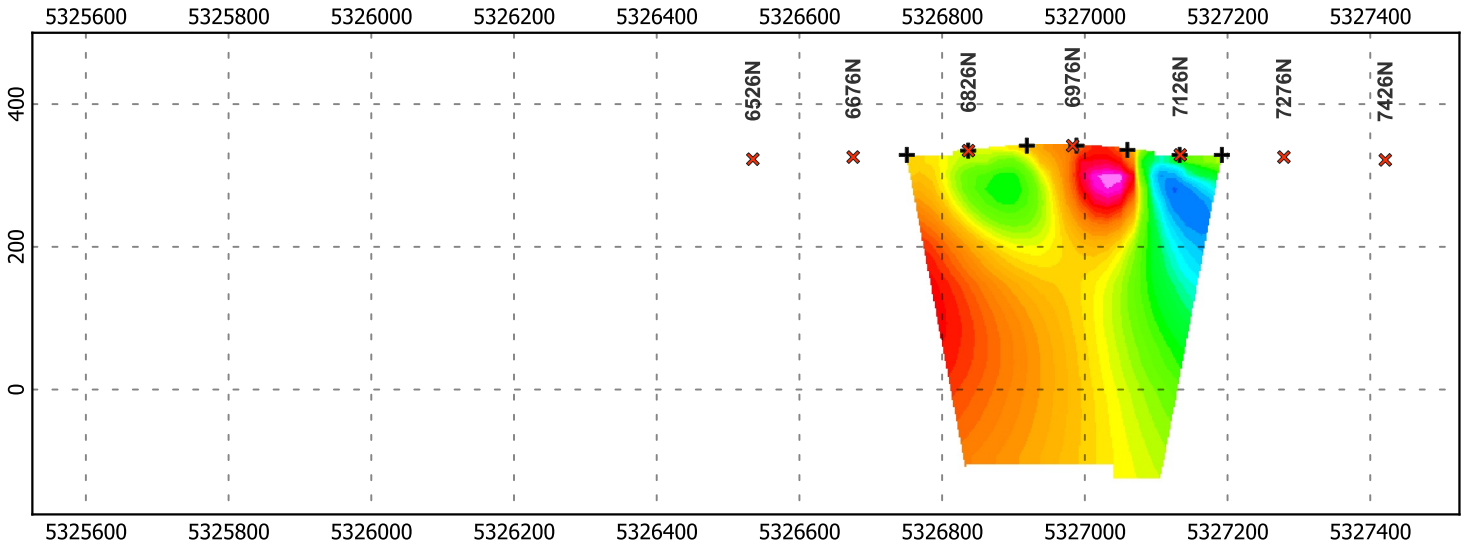
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

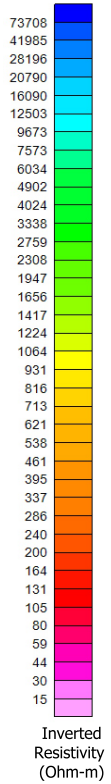
× Injection Stations
\+ Receiver Stations

0 100 200 m

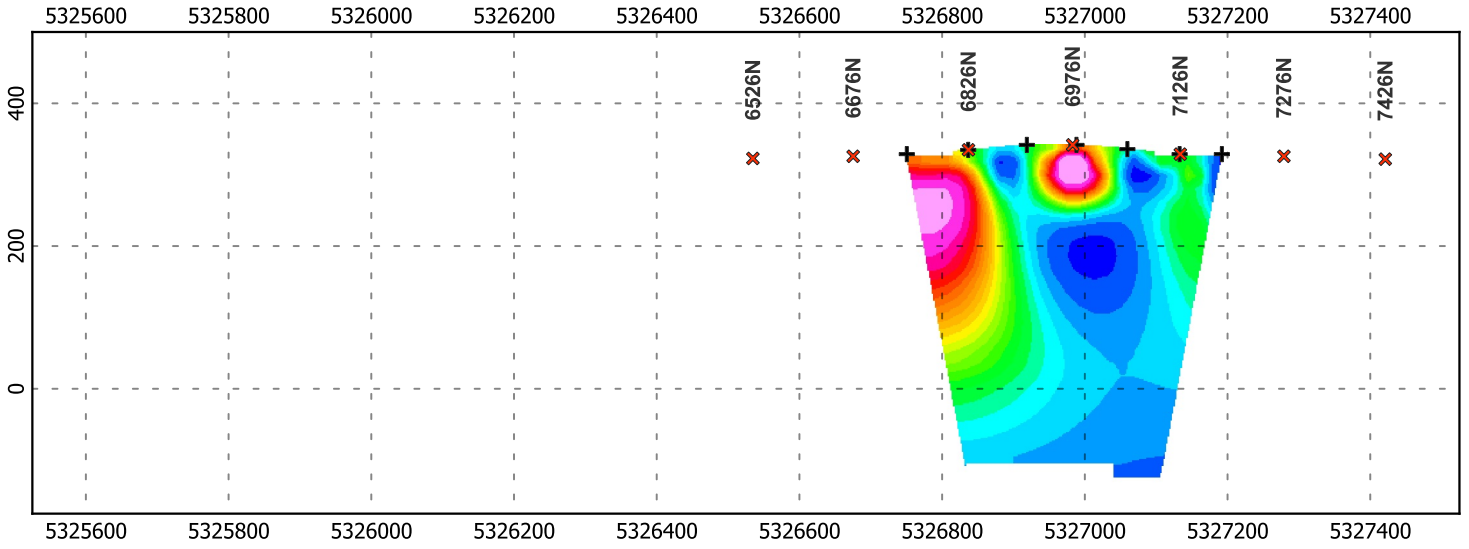
DIAS GEOPHYSICAL

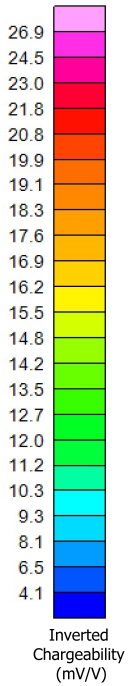
Inverted Resistivity





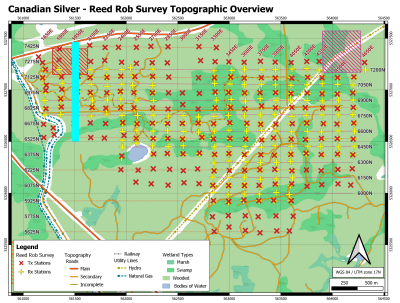
Inverted Chargeability





Reed-Robinson-L1950E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

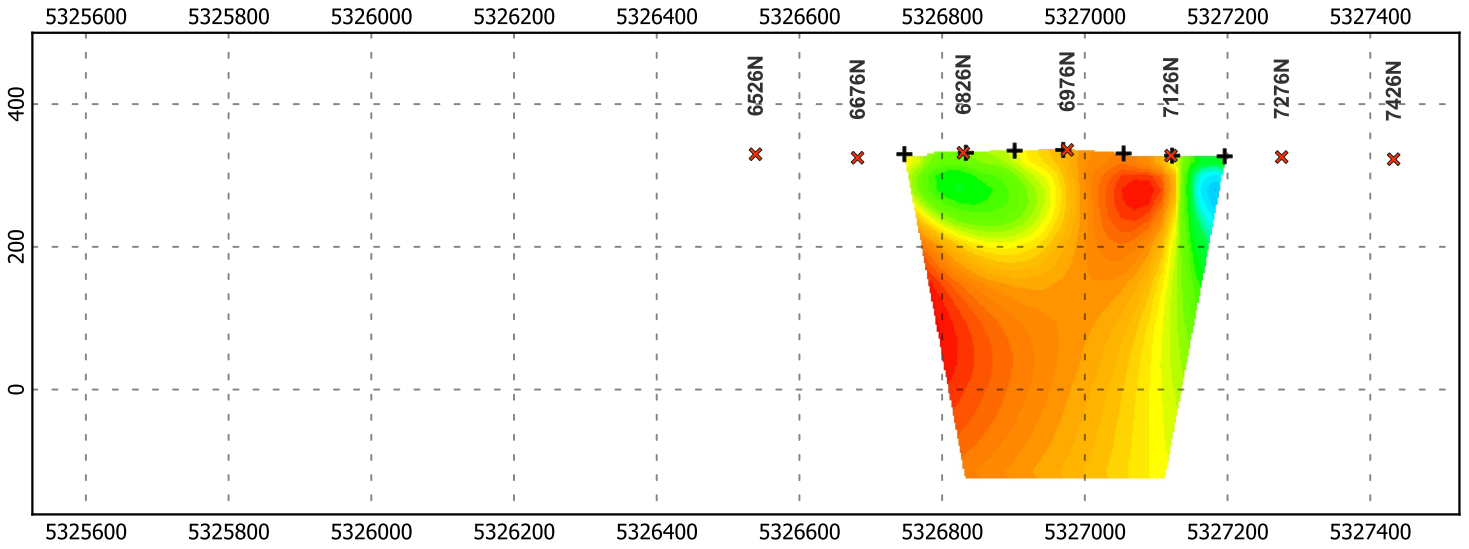
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

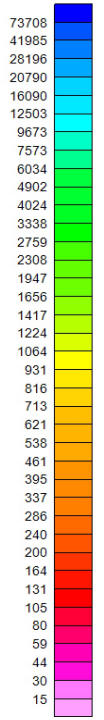
× Injection Stations
\+ Receiver Stations

0 100 200 m

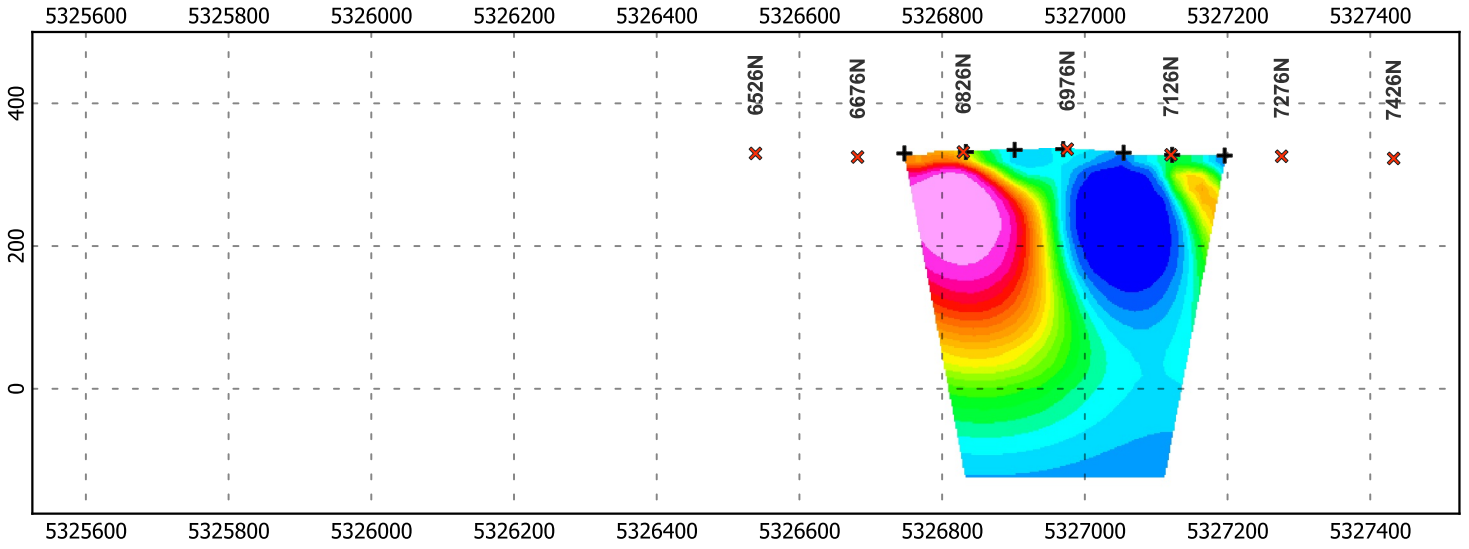
DIAS GEOPHYSICAL

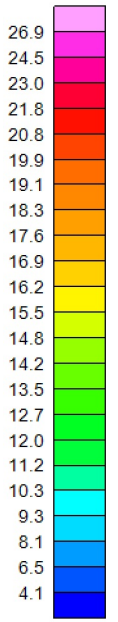
Inverted Resistivity





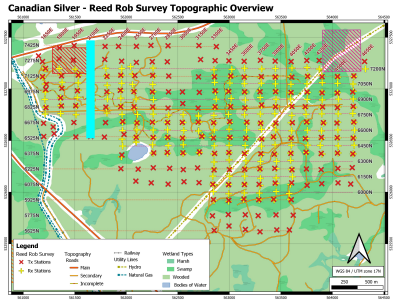
Inverted Chargeability





Reed-Robinson-L2100E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

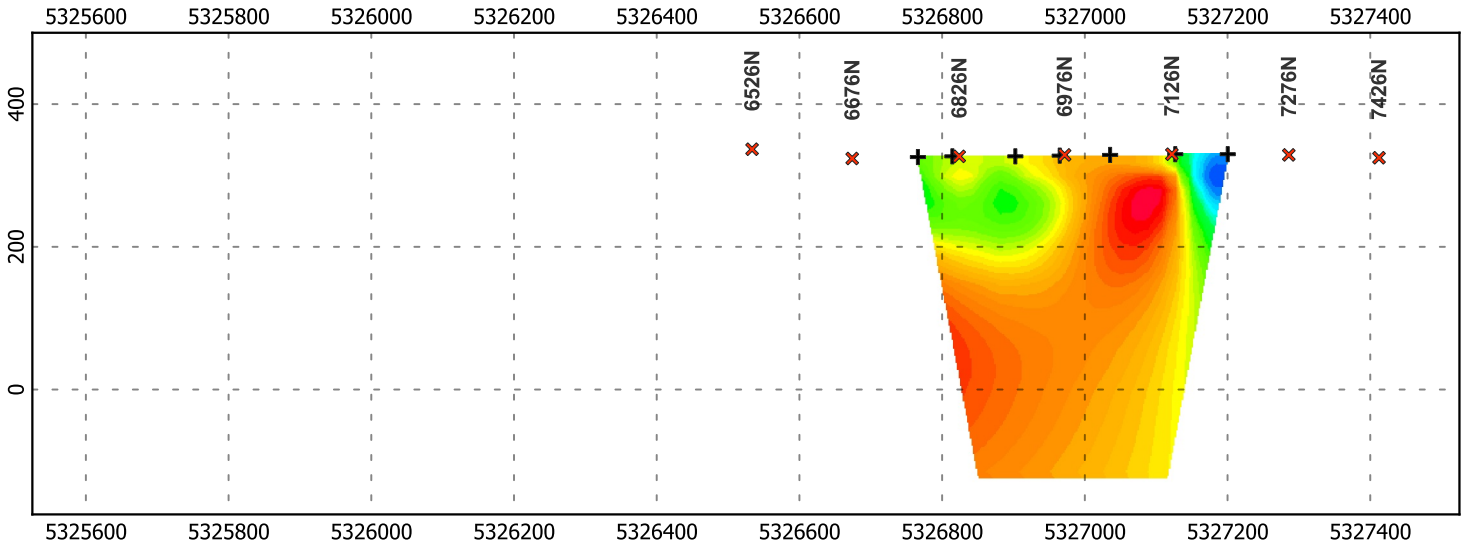
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20: 20,20,40,40,40,40,80,80,80,80,80, 80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

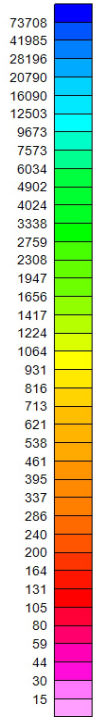
× Injection Stations
\+ Receiver Stations

0 100 200 m

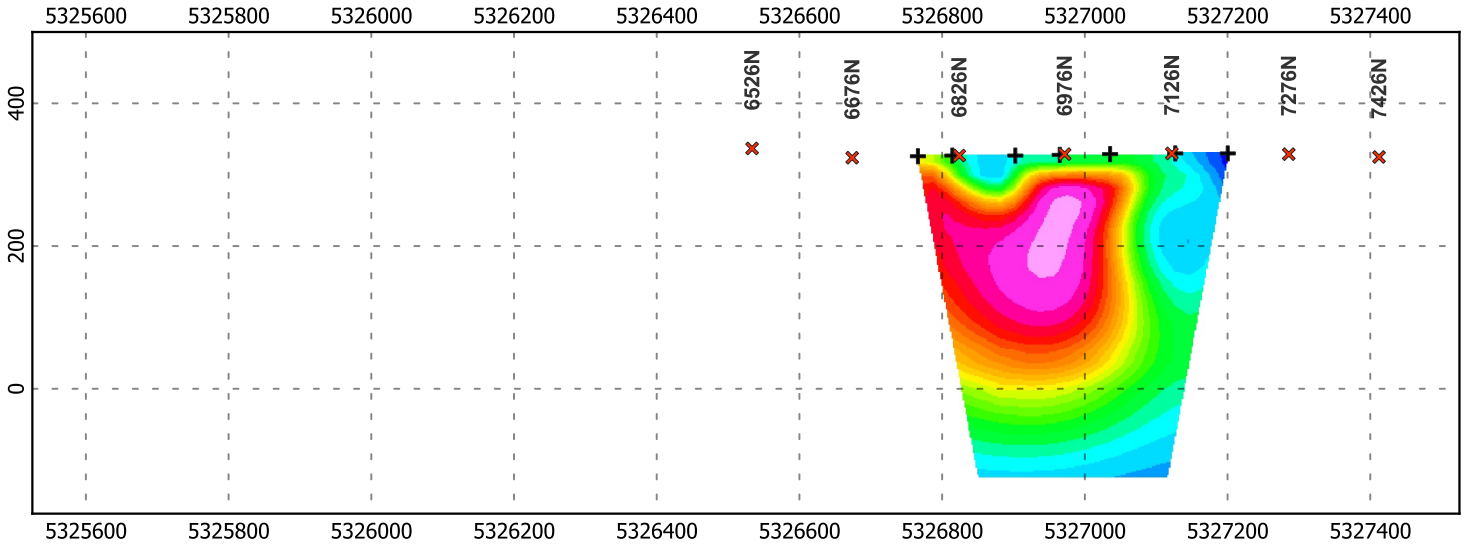
DIAS GEOPHYSICAL

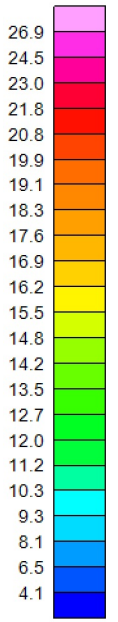
Inverted Resistivity





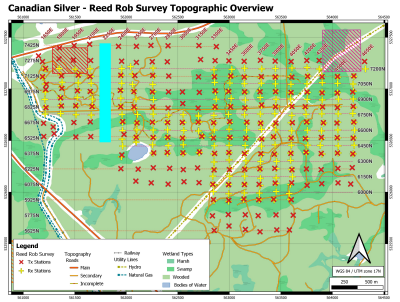
Inverted Chargeability





Reed-Robinson-L2250E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

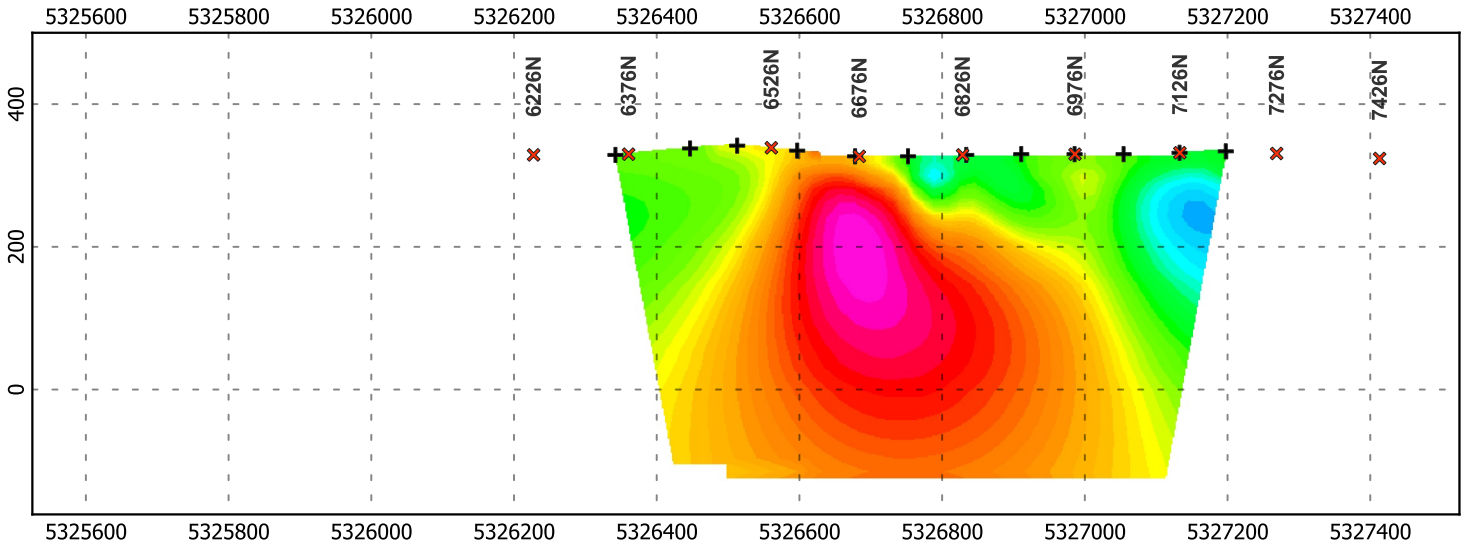
× Injection Stations
\+ Receiver Stations

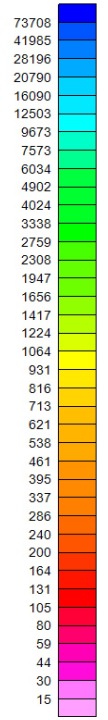
0 100 200 m

DIAS GEOPHYSICAL

Reed-Robinson-L2400E Section extracted from 3D Inverted Model

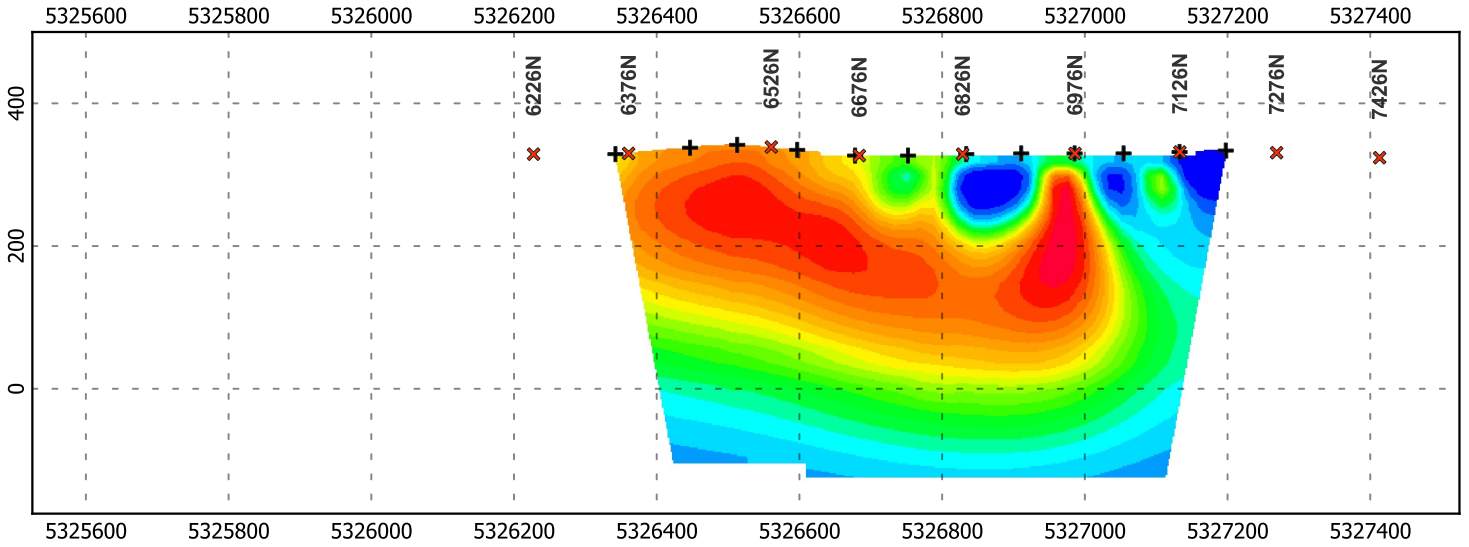
Inverted Resistivity

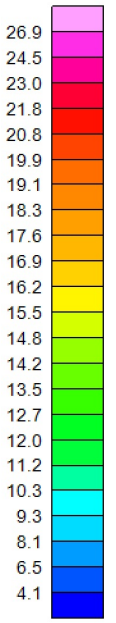




Inverted Resistivity (Ohm-m)

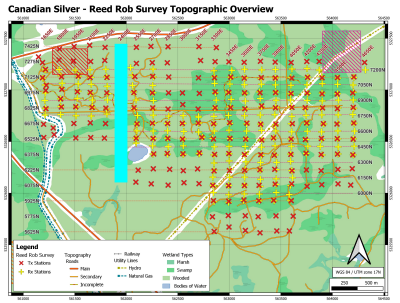
Inverted Chargeability





Inverted Chargeability (mV/V)

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

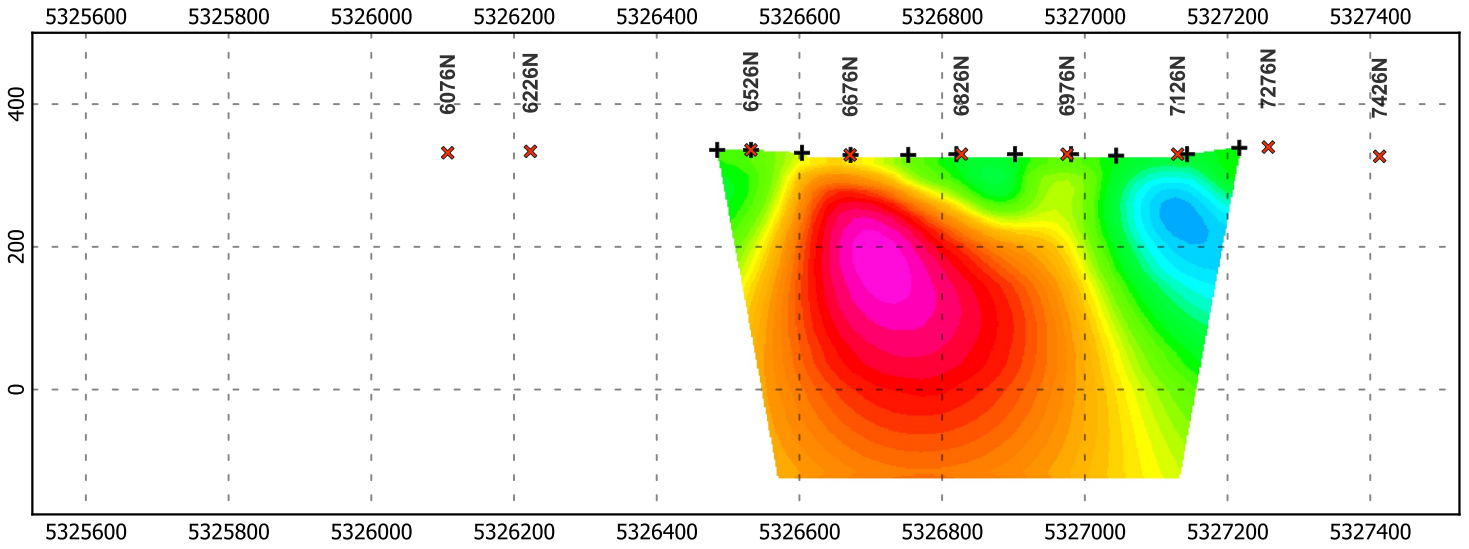
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

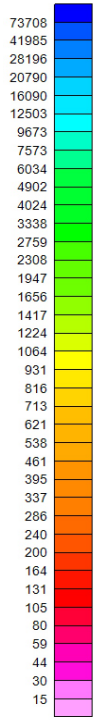
× Injection Stations
\+ Receiver Stations

0 100 200 m

DIAS GEOPHYSICAL

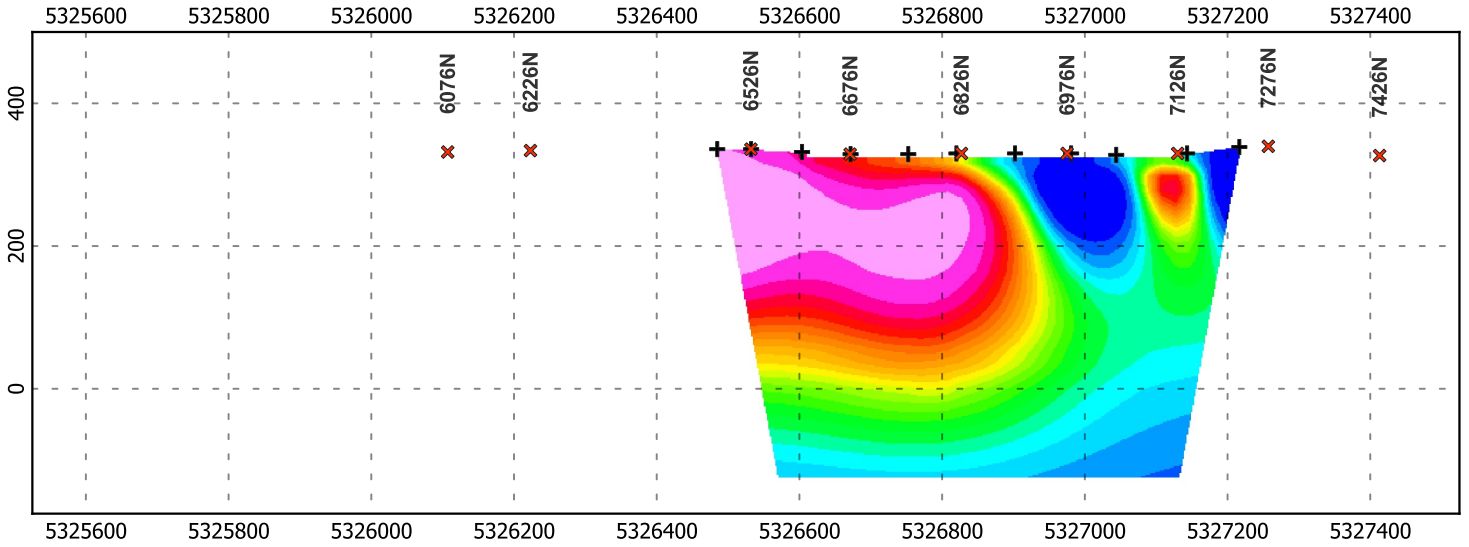
Inverted Resistivity

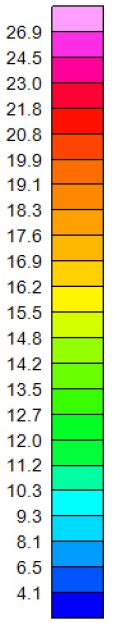




Inverted Resistivity (Ohm-m)

Inverted Chargeability

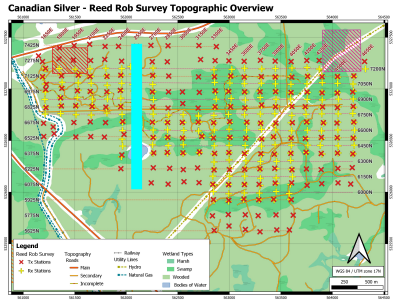




Inverted Chargeability (mV/V)

Reed-Robinson-L2550E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

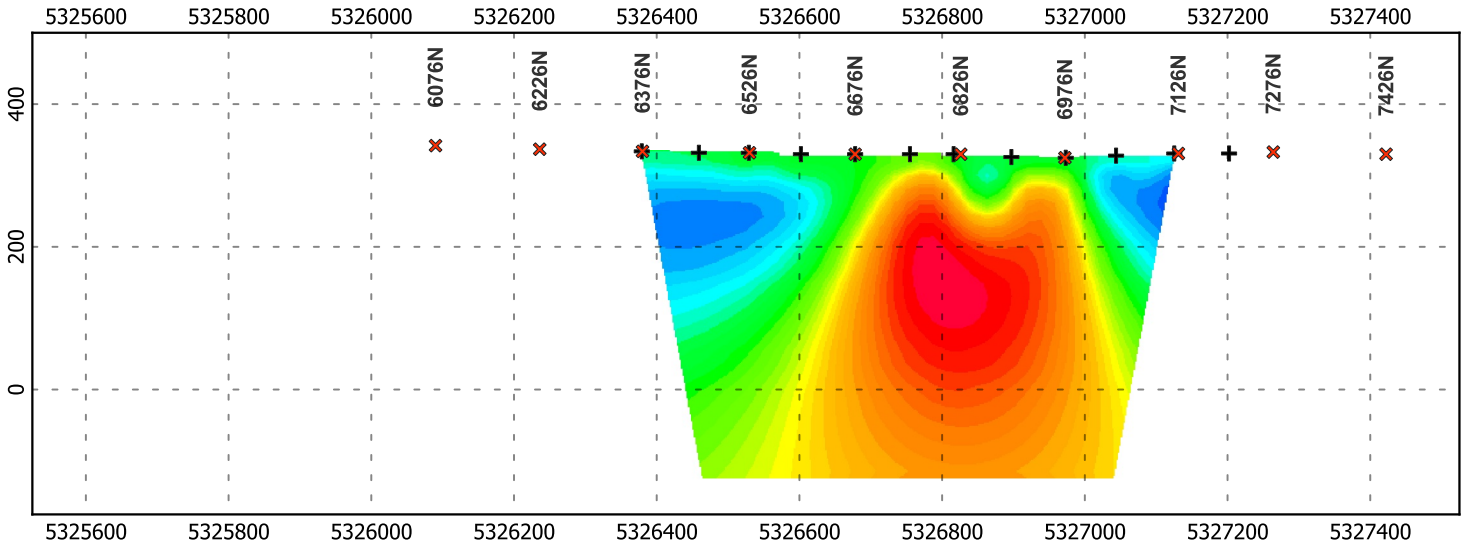
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

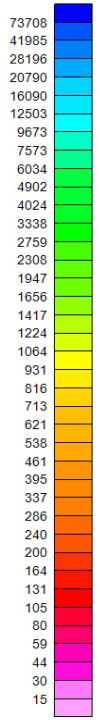
× Injection Stations
\+ Receiver Stations

0 100 200 m

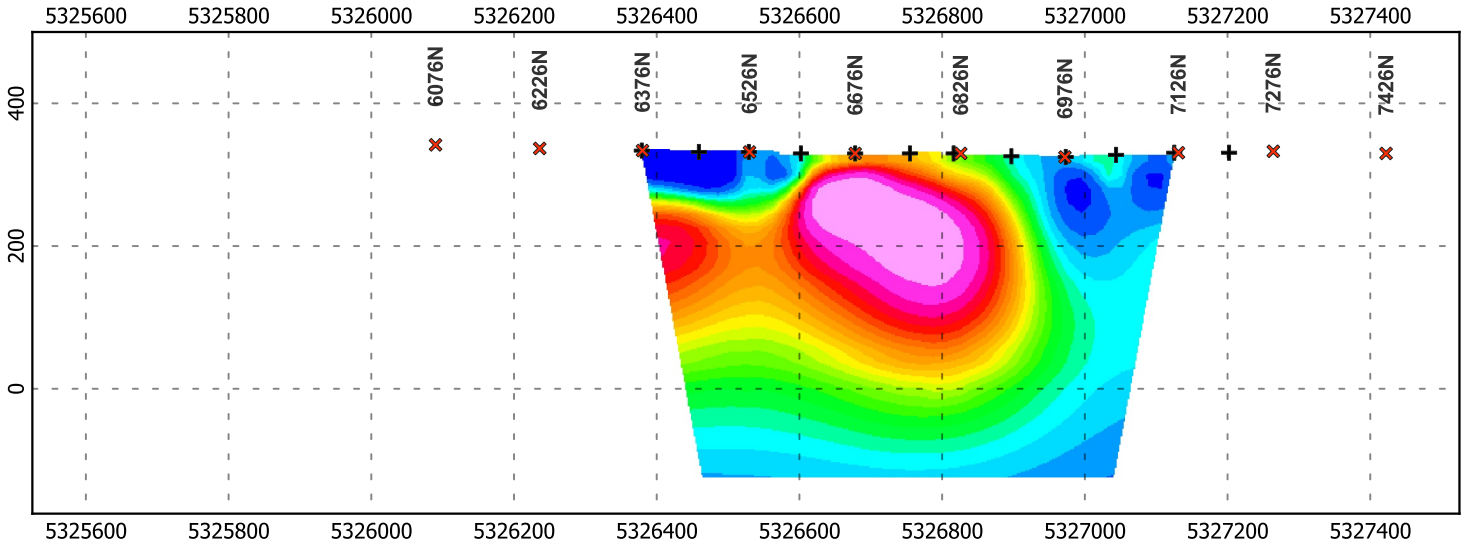
DIAS GEOPHYSICAL

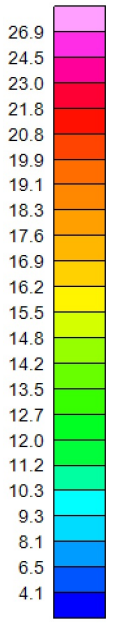
Inverted Resistivity





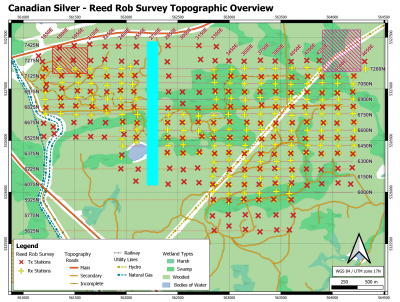
Inverted Chargeability





Reed-Robinson-L2700E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

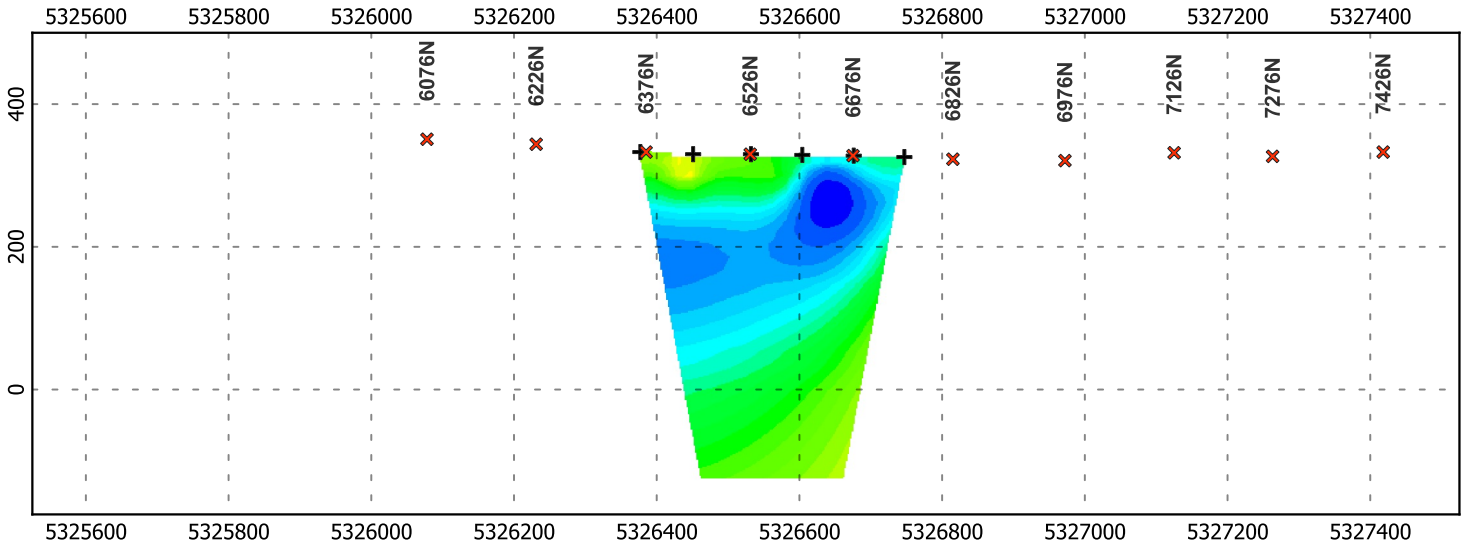
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20: 20,20,40,40,40,40,80,80,80,80,80, 80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

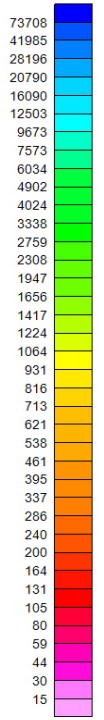
× Injection Stations
\+ Receiver Stations

0 100 200 m

DIAS GEOPHYSICAL

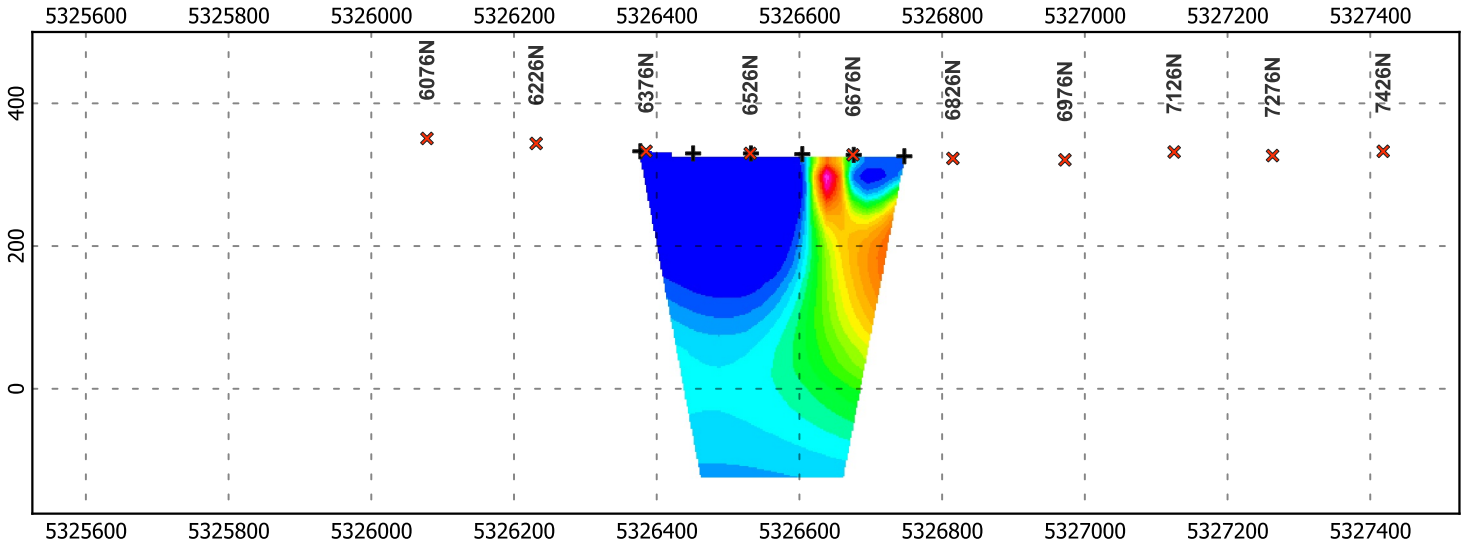
Inverted Resistivity

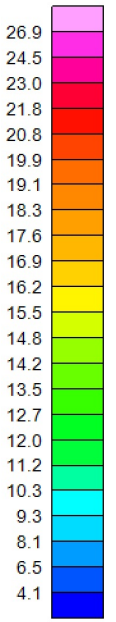




Inverted Resistivity (Ohm-m)

Inverted Chargeability

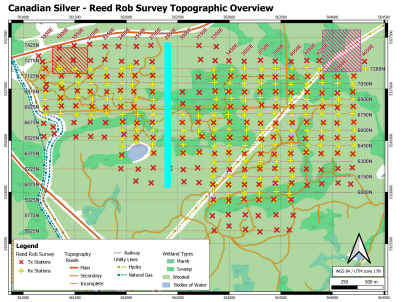




Inverted Chargeability (mV/V)

Reed-Robinson-L2850E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

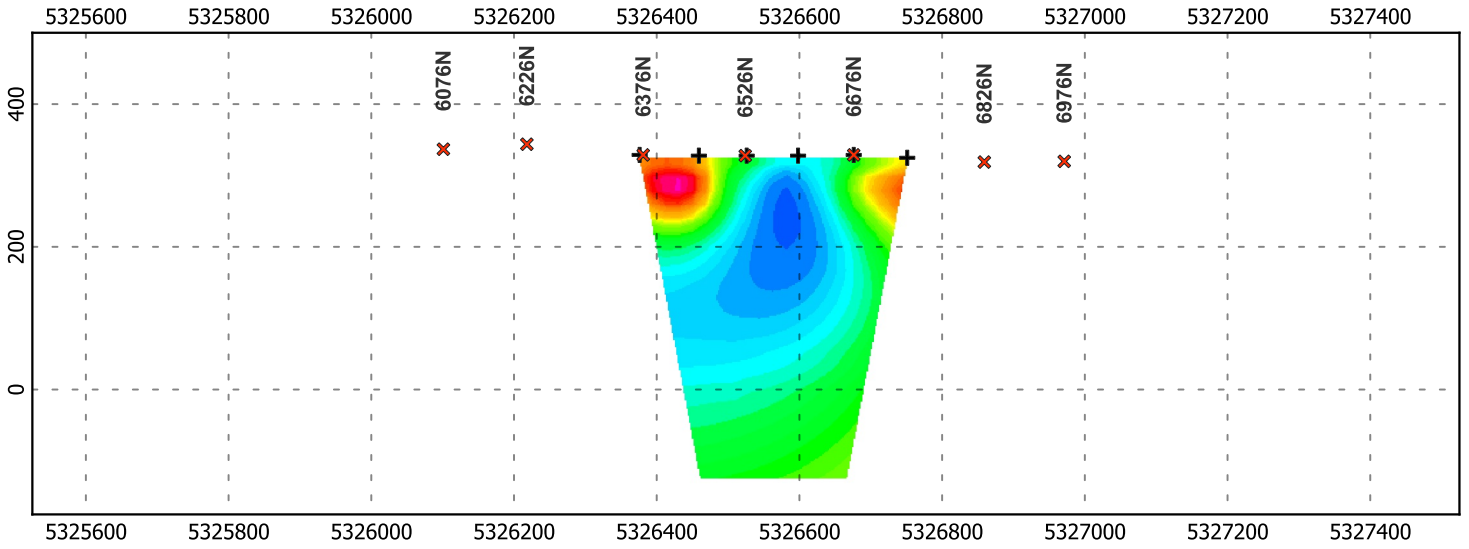
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

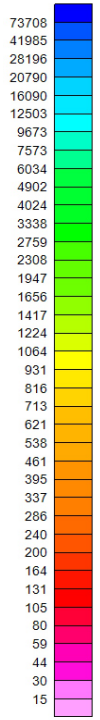
× Injection Stations
\+ Receiver Stations

0 100 200 m

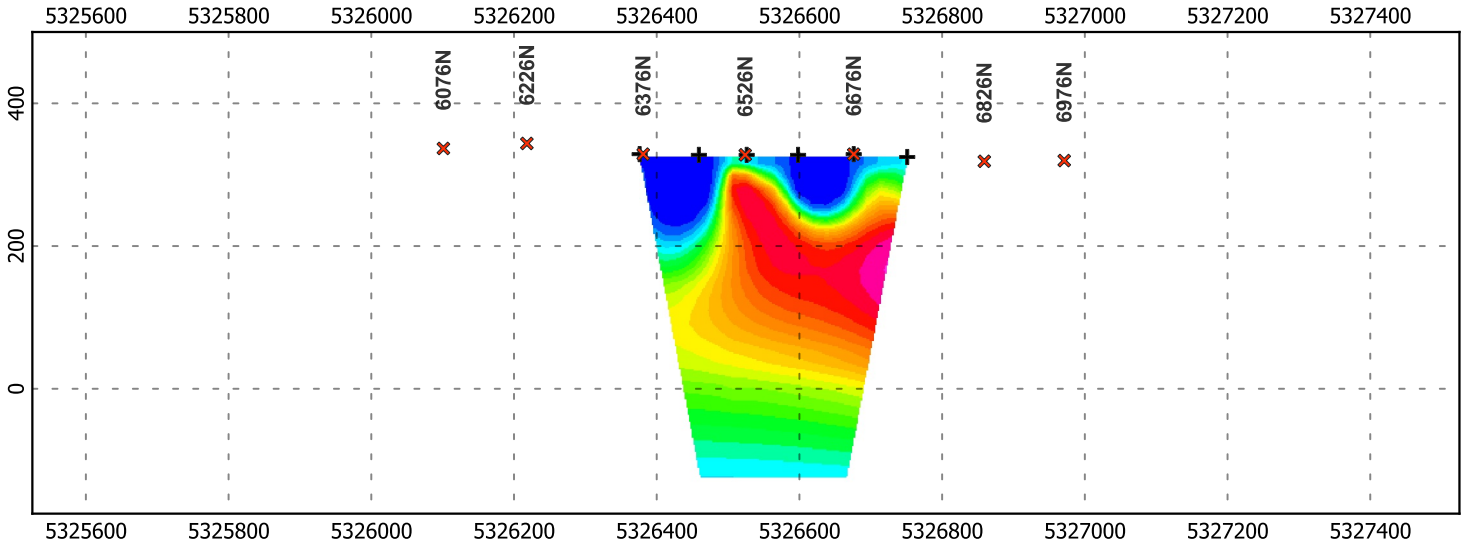
DIAS GEOPHYSICAL

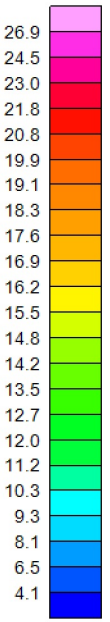
Inverted Resistivity





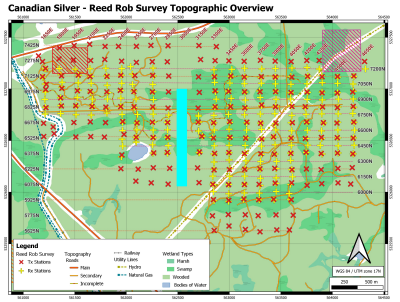
Inverted Chargeability





Reed-Robinson-L3000E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

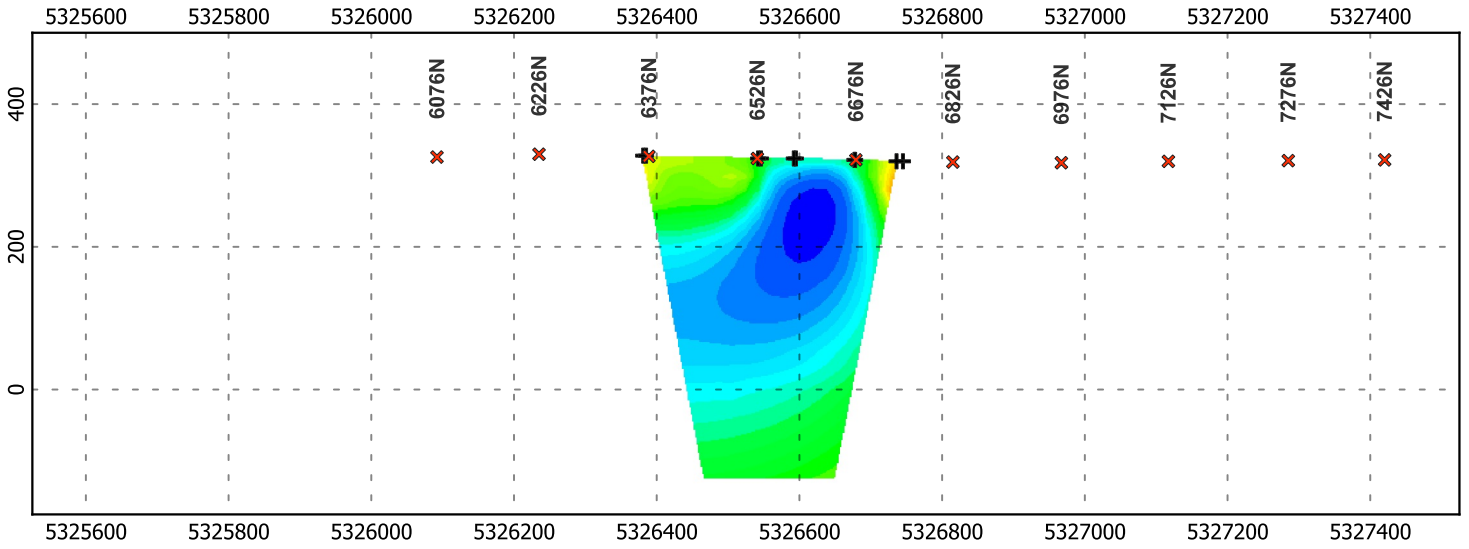
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20: 20,20,40,40,40,40,80,80,80,80,80, 80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

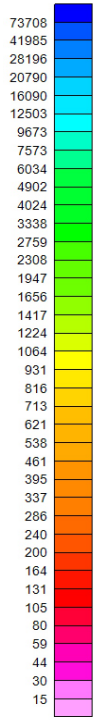
× Injection Stations
\+ Receiver Stations

0 100 200 m

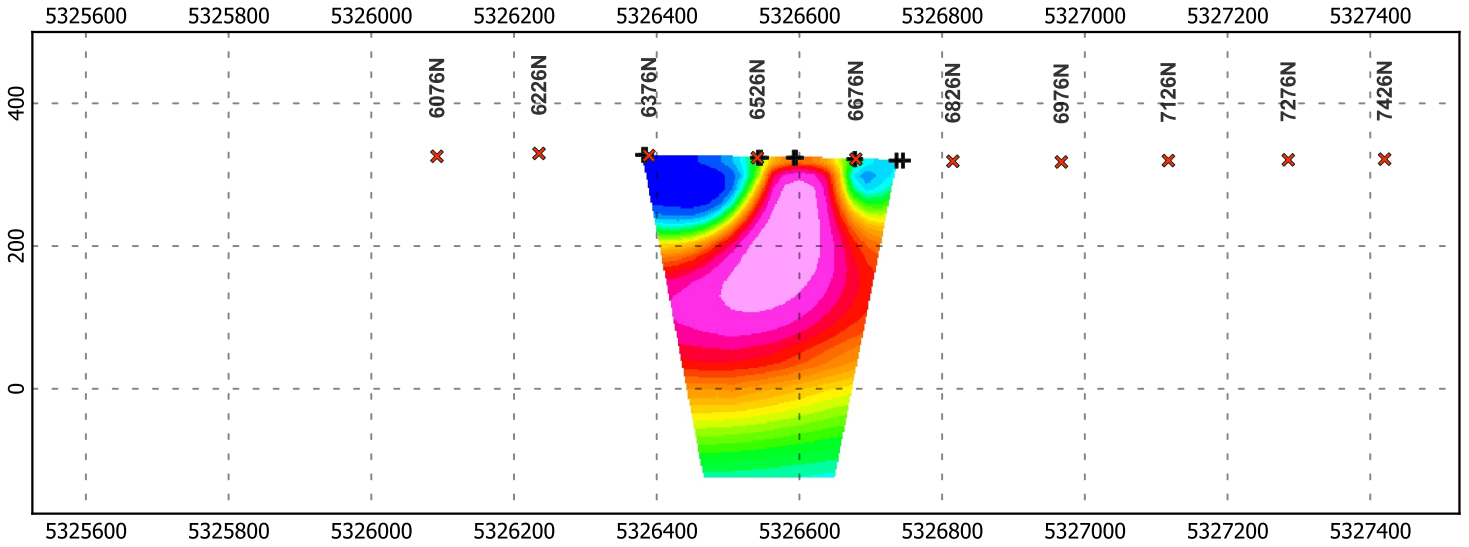
DIAS GEOPHYSICAL

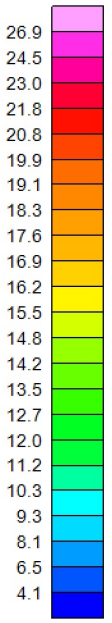
Inverted Resistivity





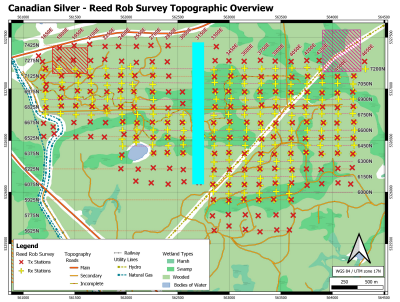
Inverted Chargeability





Reed-Robinson-L3150E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

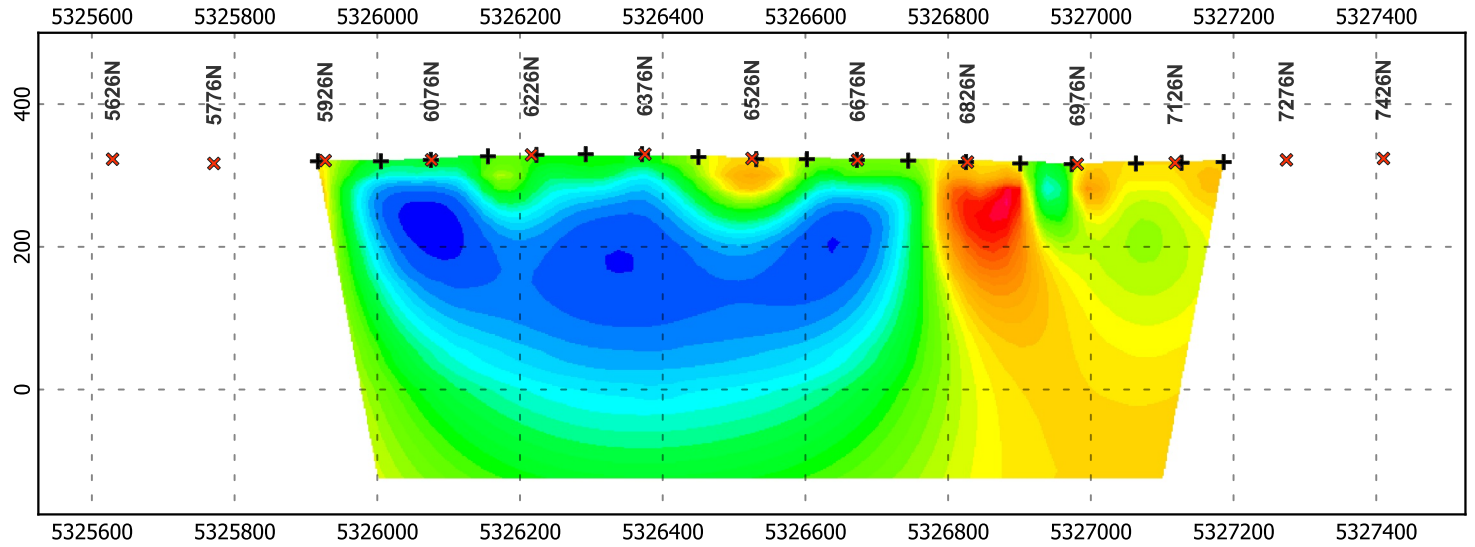
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

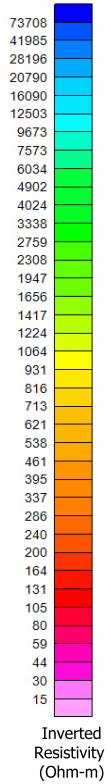
× Injection Stations
\+ Receiver Stations

0 100 200 m

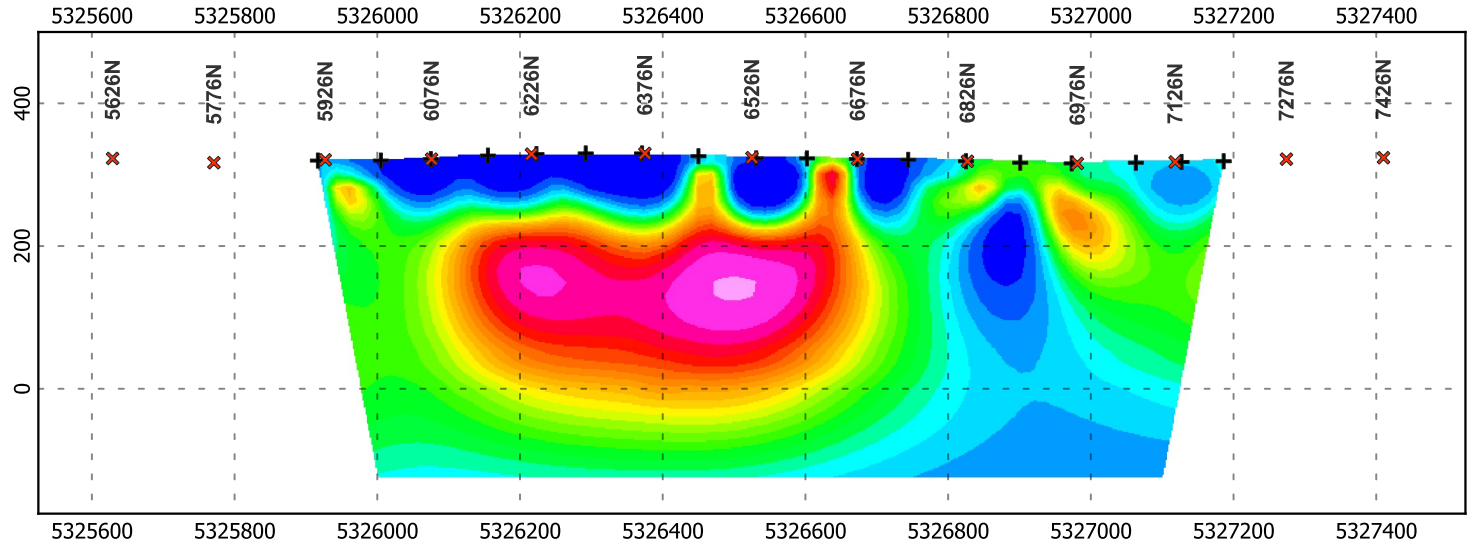
DIAS GEOPHYSICAL

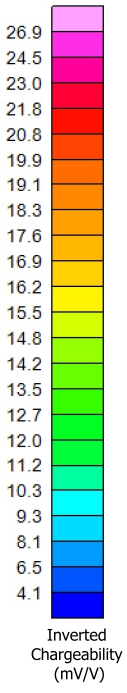
Inverted Resistivity





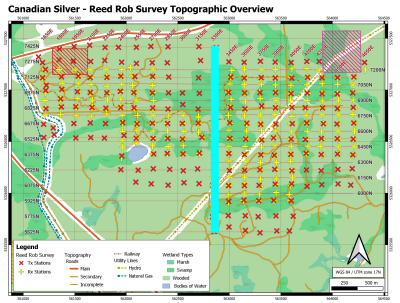
Inverted Chargeability





Reed-Robinson-L3300E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

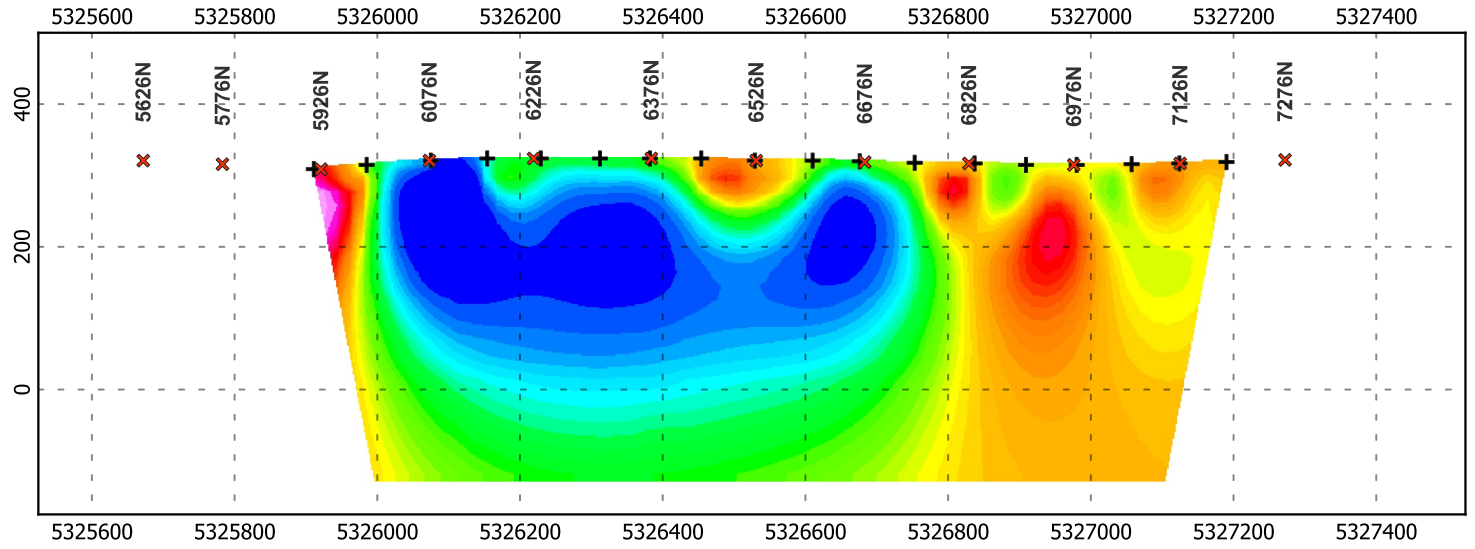
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

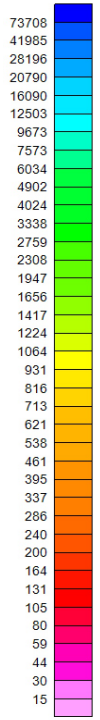
× Injection Stations
\+ Receiver Stations

0 100 200 m

DIAS GEOPHYSICAL

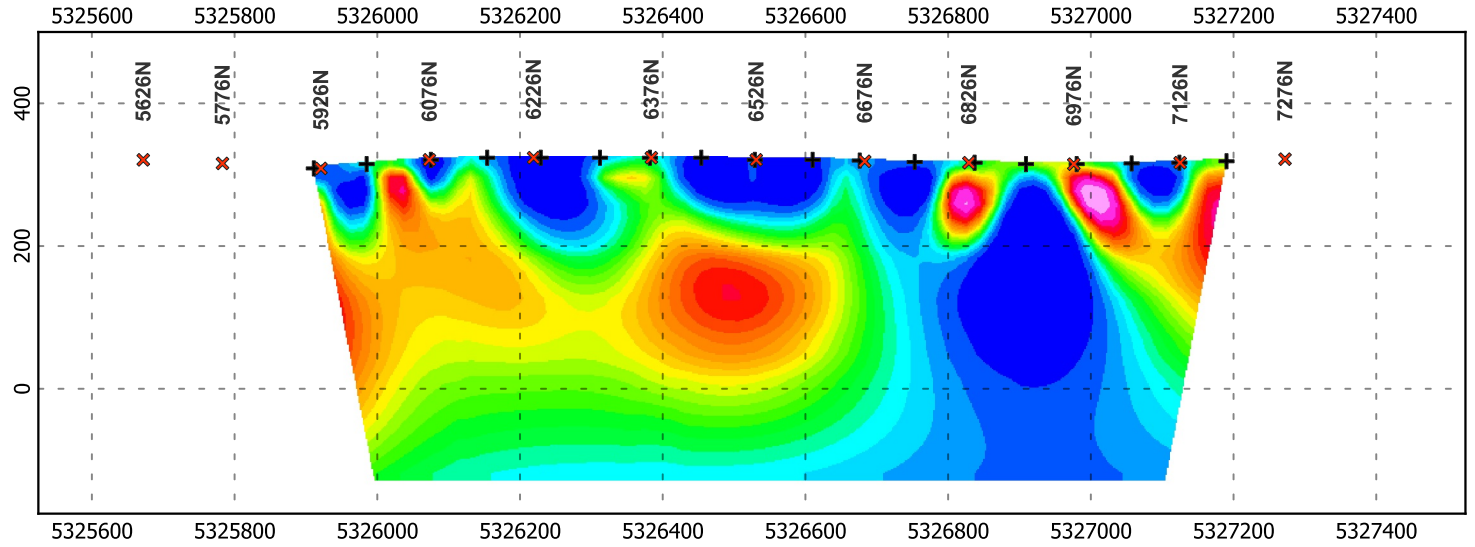
Inverted Resistivity

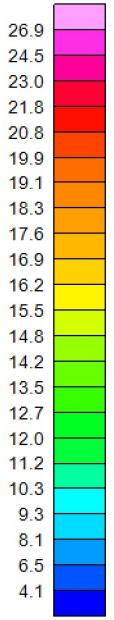




Inverted Resistivity (Ohm-m)

Inverted Chargeability

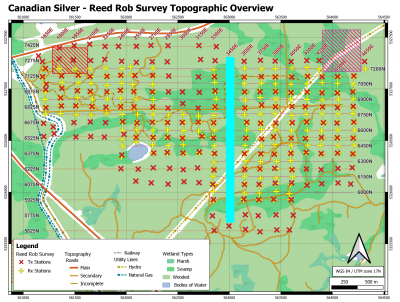




Inverted Chargeability (mV/V)

Reed-Robinson-L3450E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

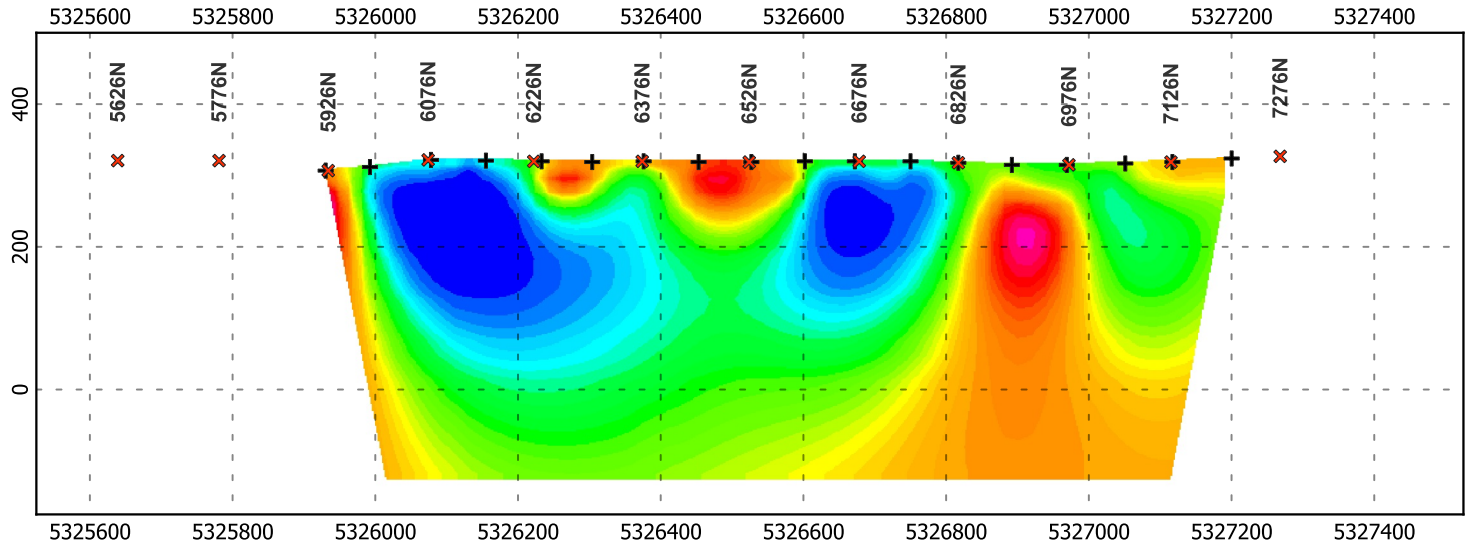
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

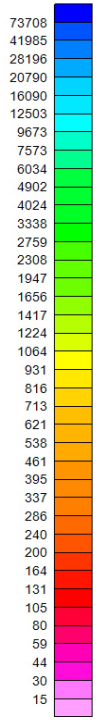
× Injection Stations
\+ Receiver Stations

0 100 200 m

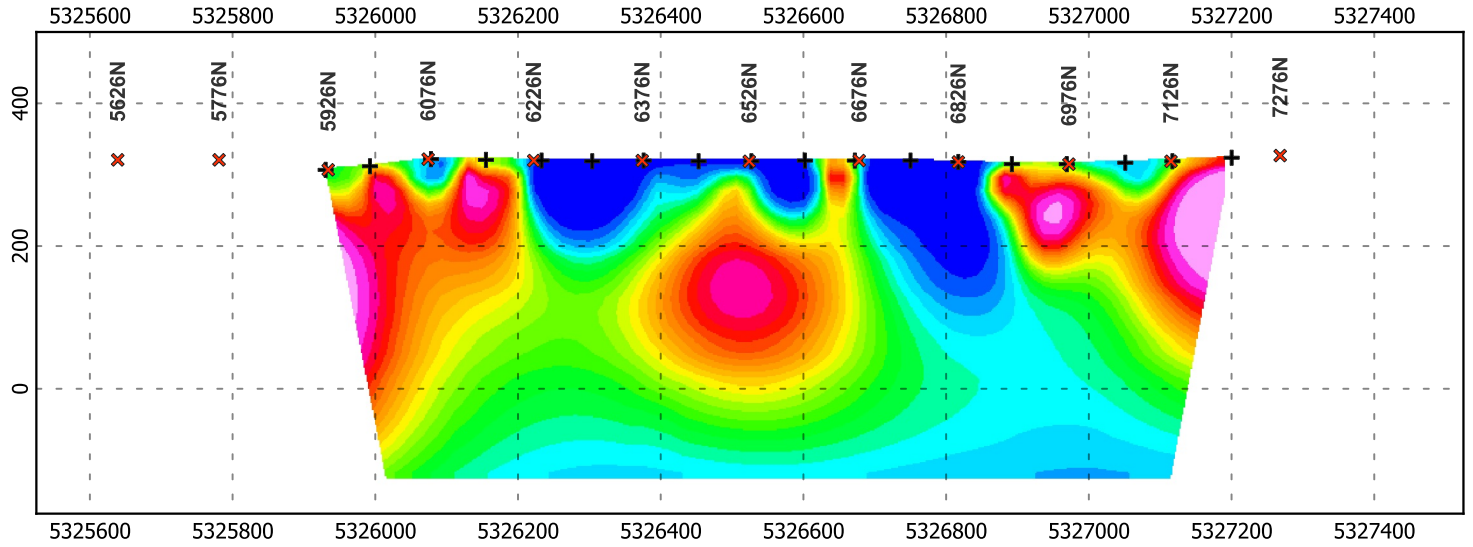
DIAS GEOPHYSICAL

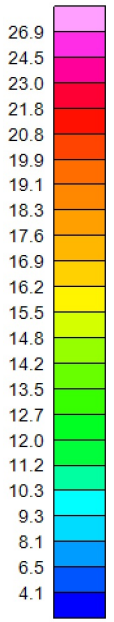
Inverted Resistivity





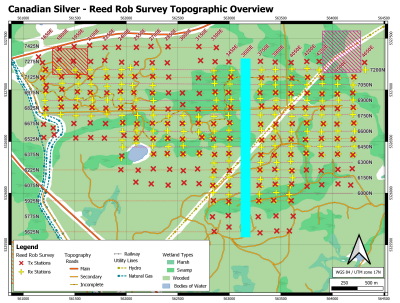
Inverted Chargeability





Reed-Robinson-L3600E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

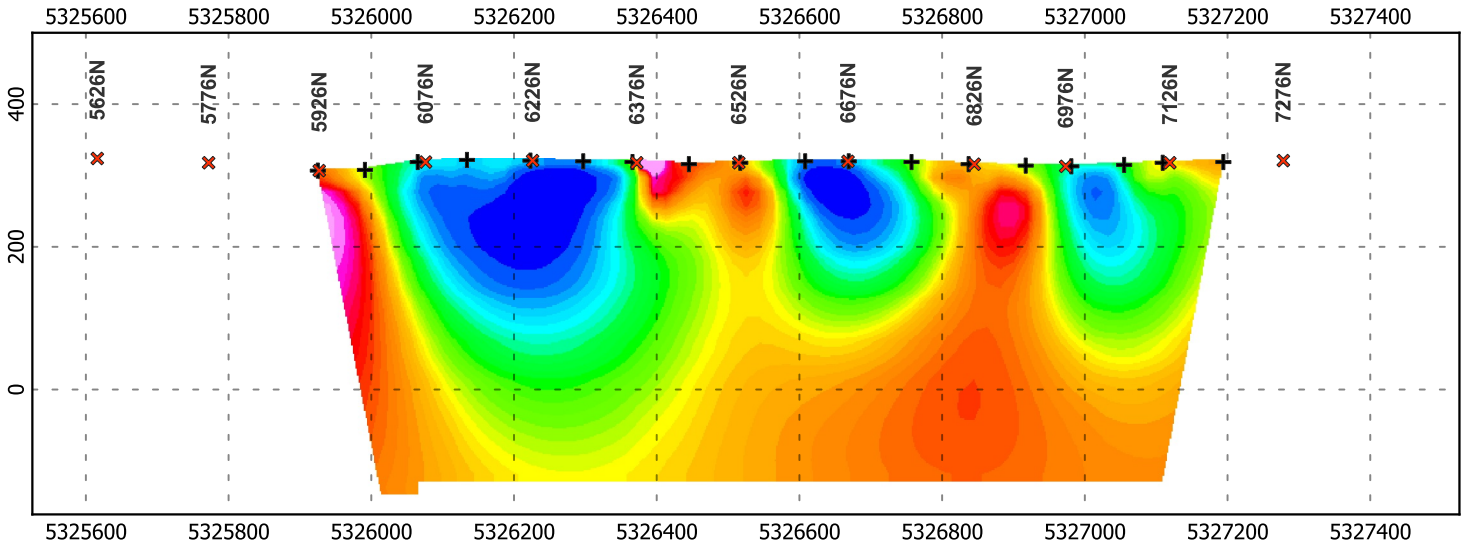
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

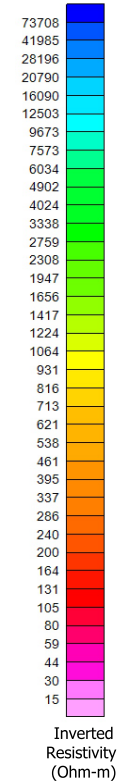
× Injection Stations
\+ Receiver Stations

0 100 200 m

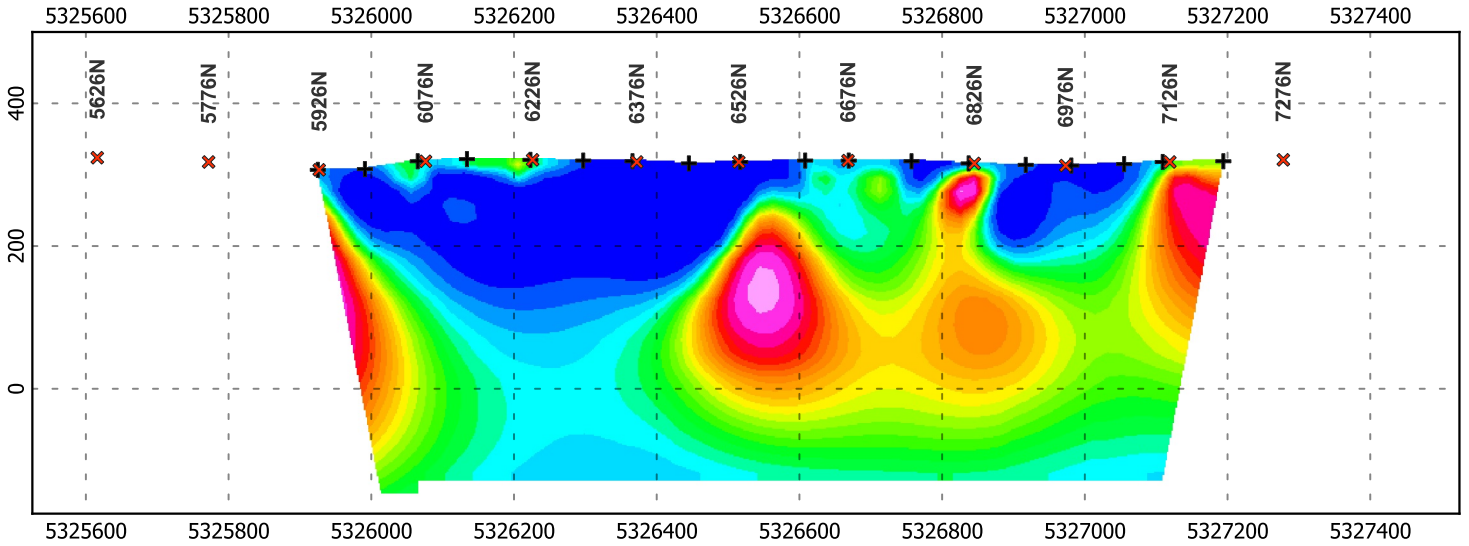
DIAS GEOPHYSICAL

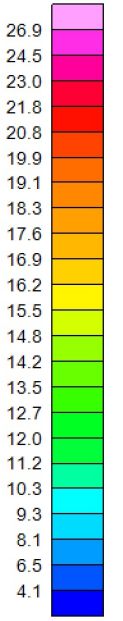
Inverted Resistivity





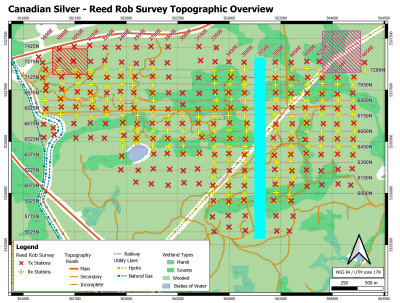
Inverted Chargeability





Reed-Robinson-L3750E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

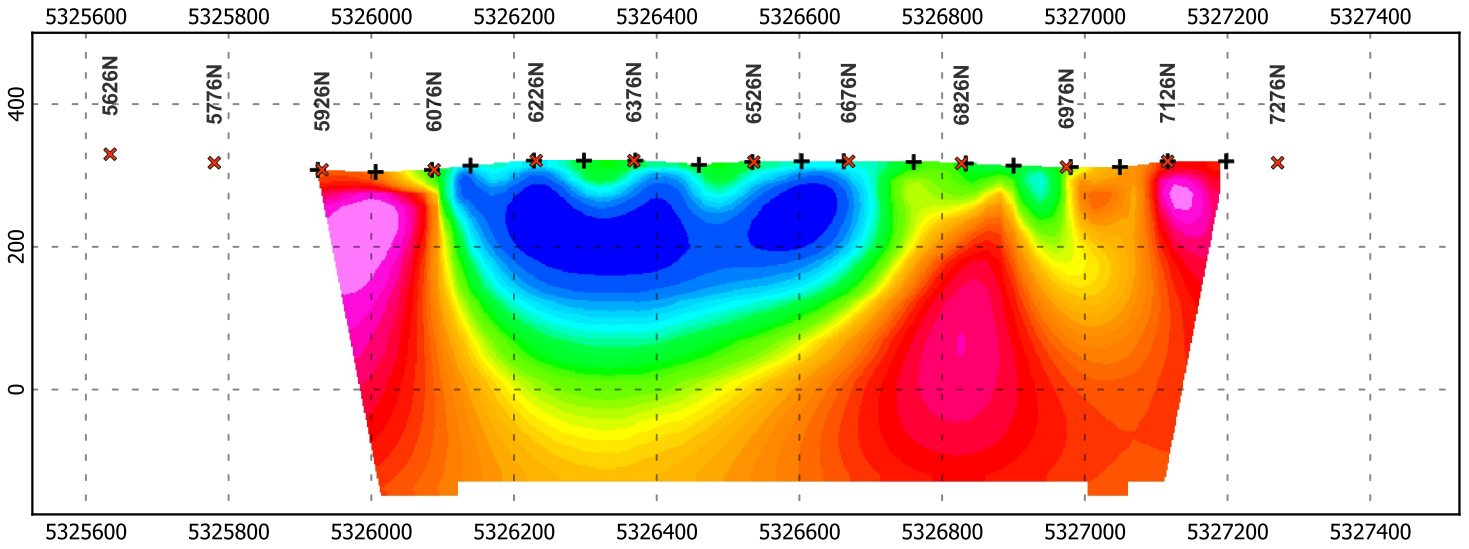
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

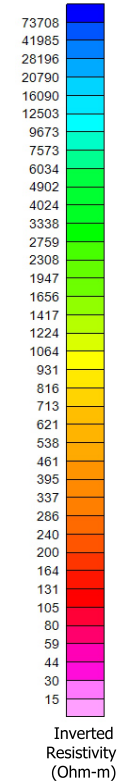
× Injection Stations
\+ Receiver Stations

0 100 200 m

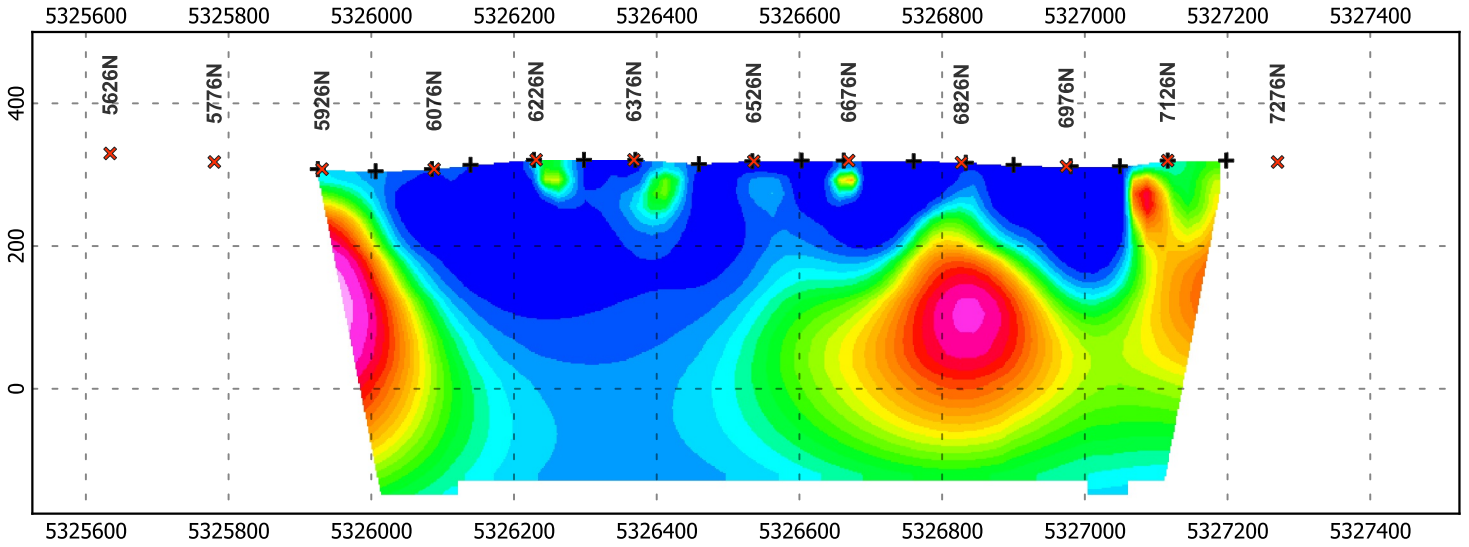
DIAS GEOPHYSICAL

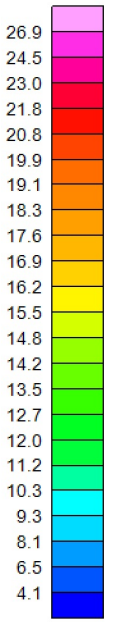
Inverted Resistivity





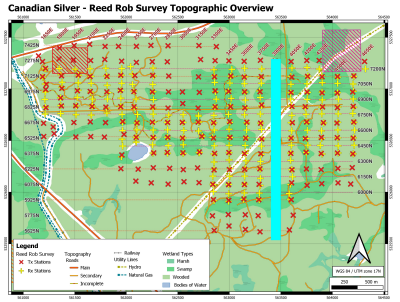
Inverted Chargeability





Reed-Robinson-L3900E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

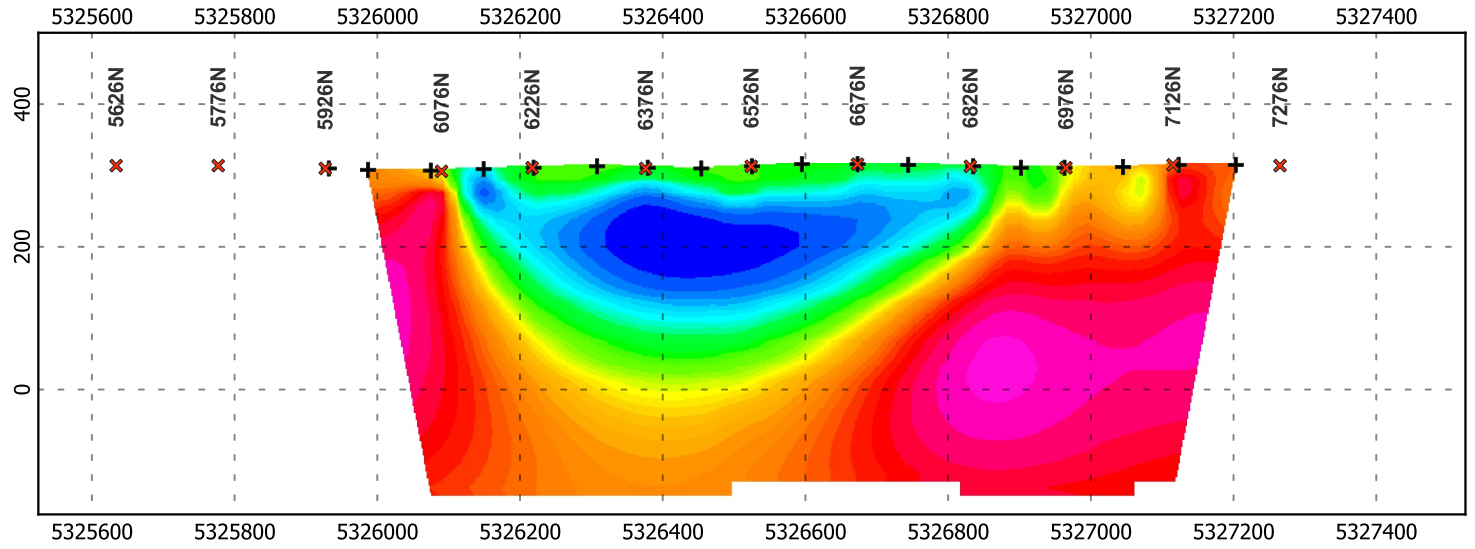
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

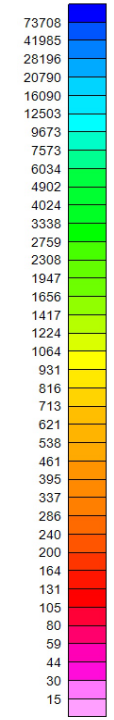
× Injection Stations
\+ Receiver Stations

0 100 200 m

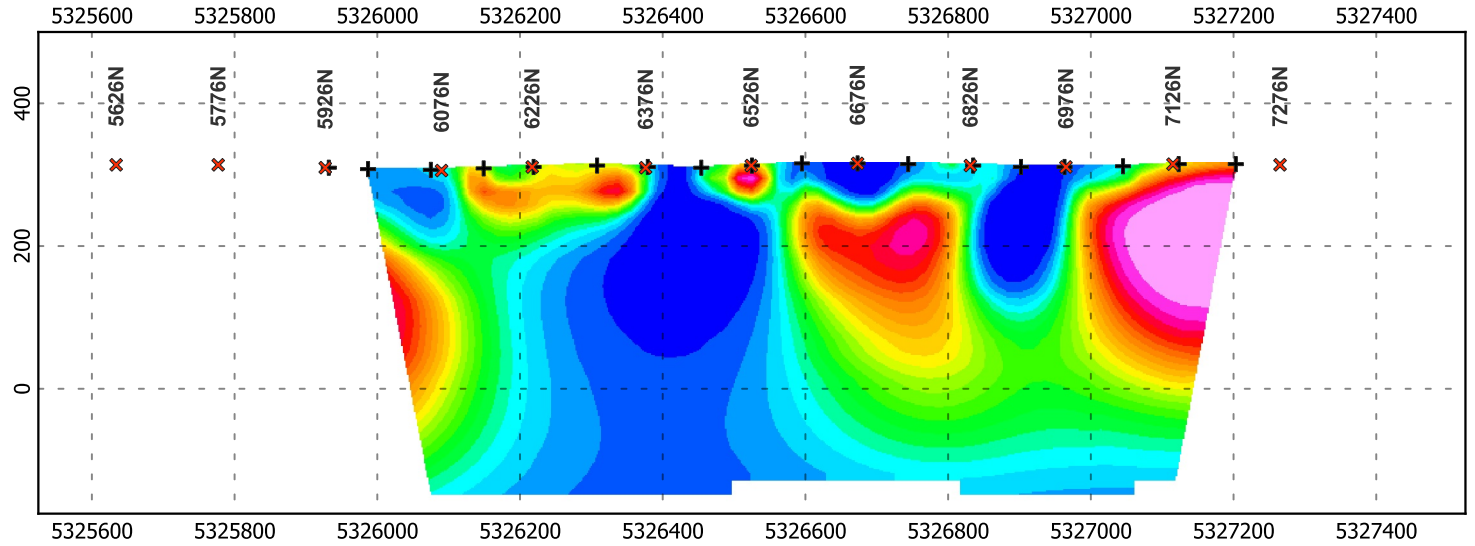
DIAS GEOPHYSICAL

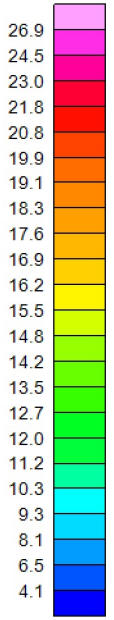
Inverted Resistivity





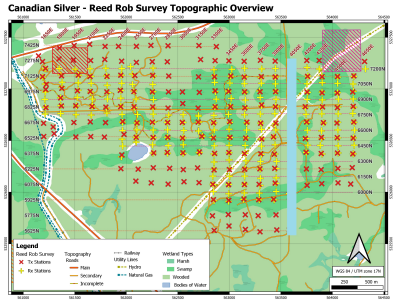
Inverted Chargeability





Reed-Robinson-L4050E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

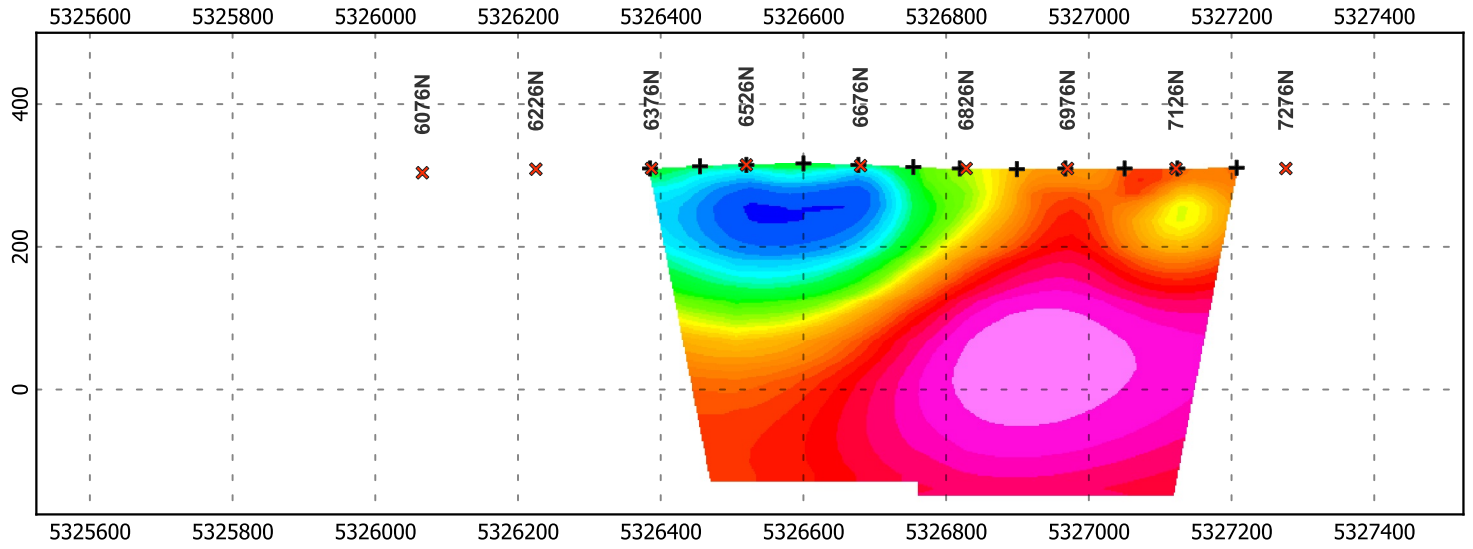
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

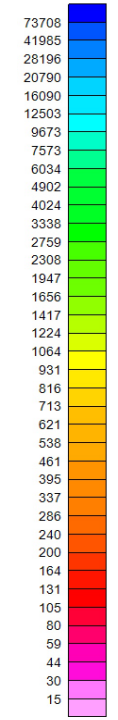
× Injection Stations
\+ Receiver Stations

0 100 200 m

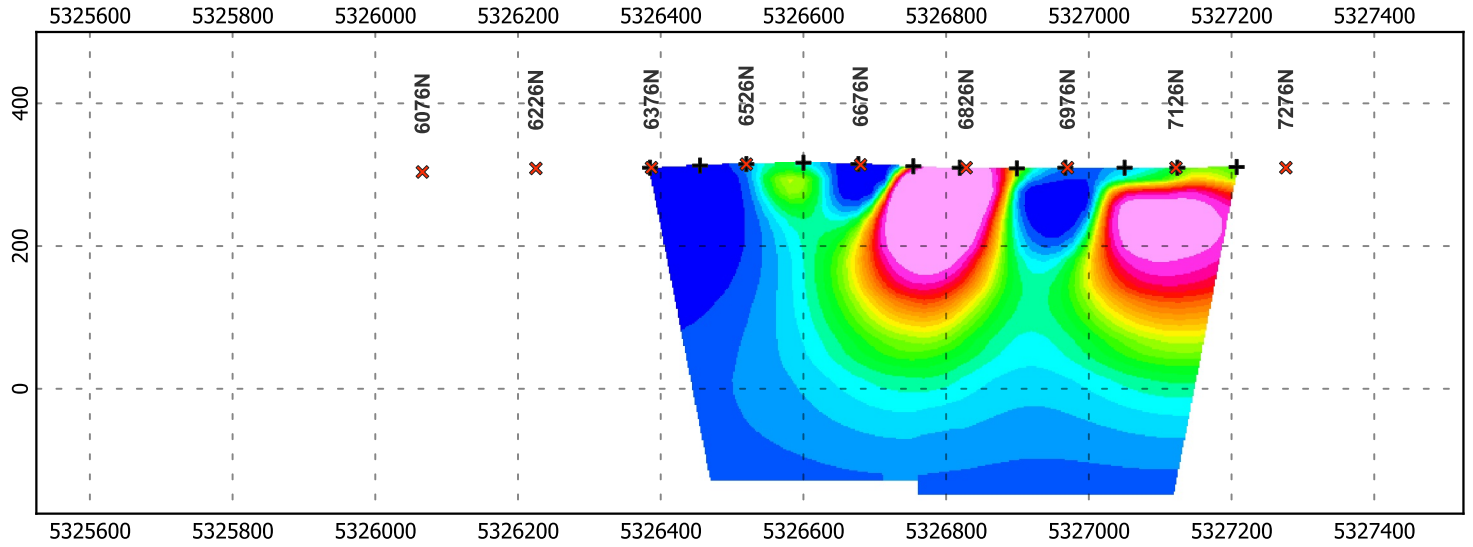
DIAS GEOPHYSICAL

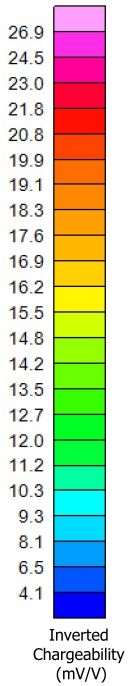
Inverted Resistivity





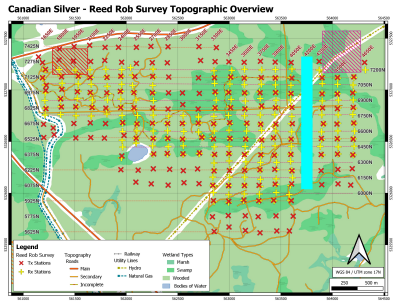
Inverted Chargeability





Reed-Robinson-L4200E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

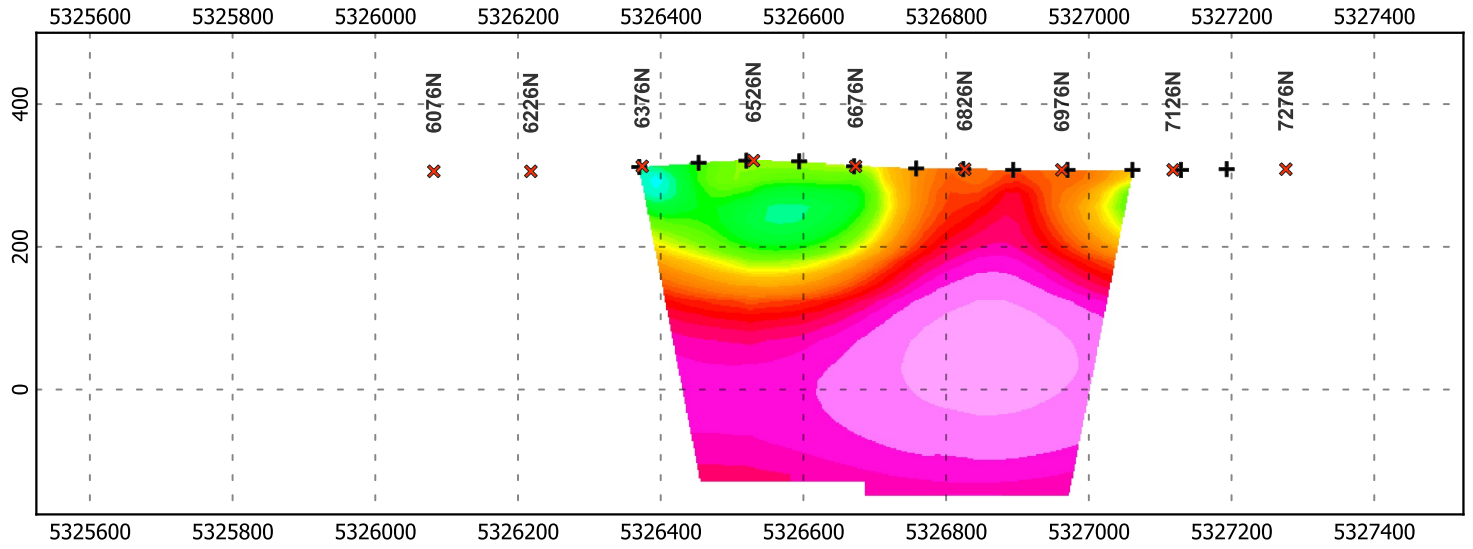
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

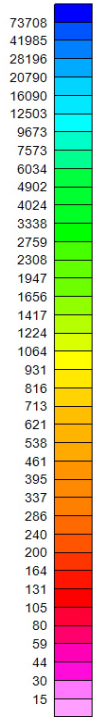
× Injection Stations
\+ Receiver Stations

0 100 200 m

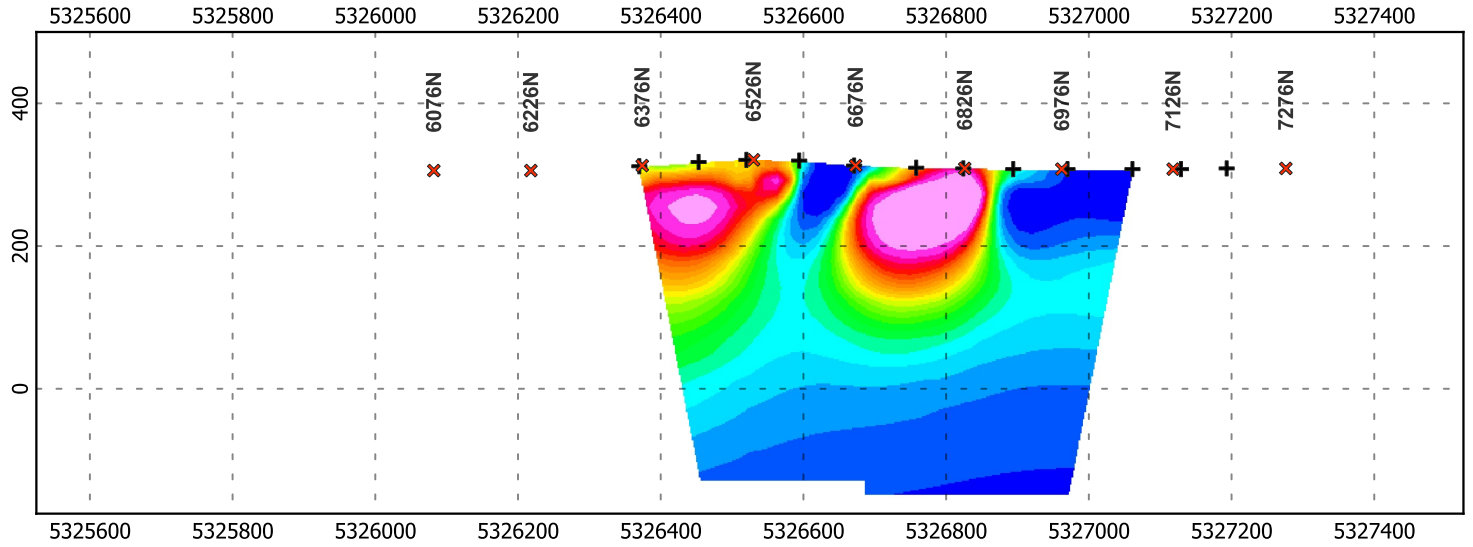
DIAS GEOPHYSICAL

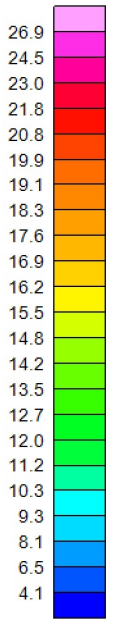
Inverted Resistivity





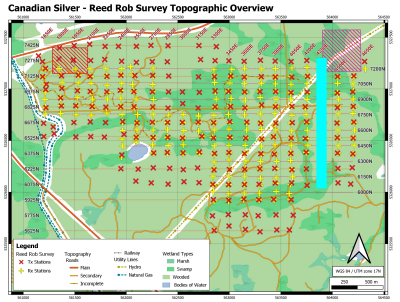
Inverted Chargeability





Reed-Robinson-L4350E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

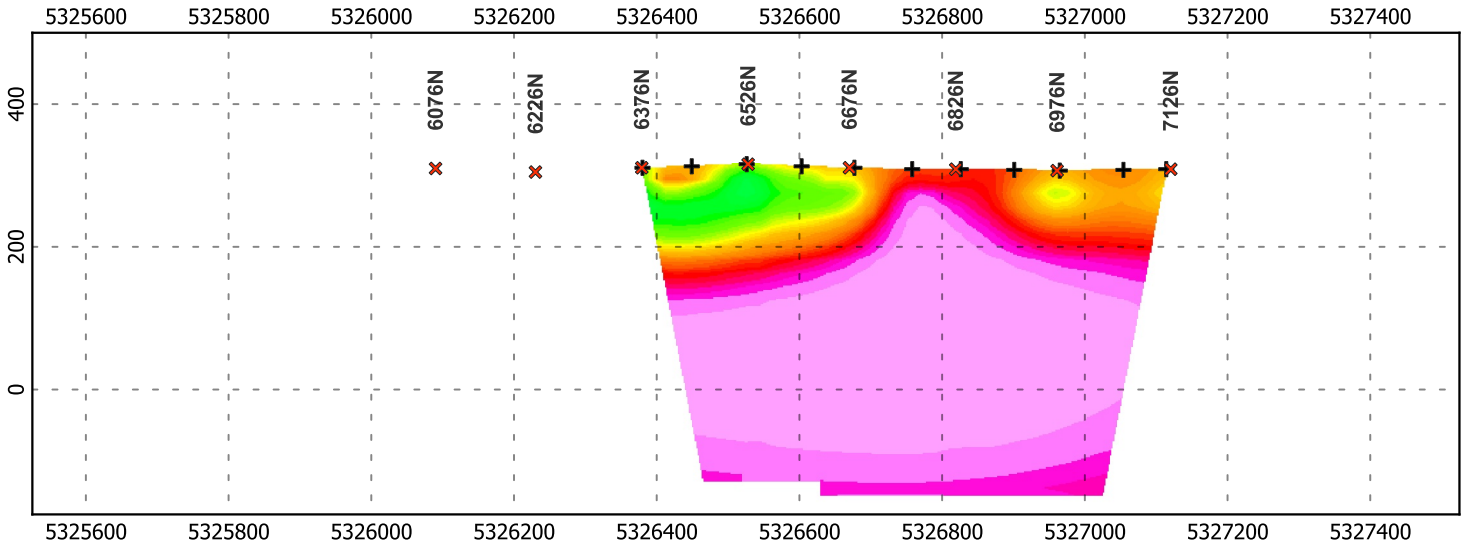
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

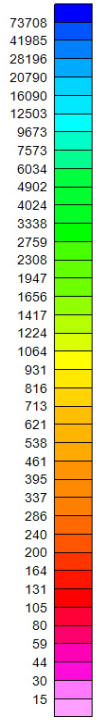
× Injection Stations
\+ Receiver Stations

0 100 200 m

DIAS GEOPHYSICAL

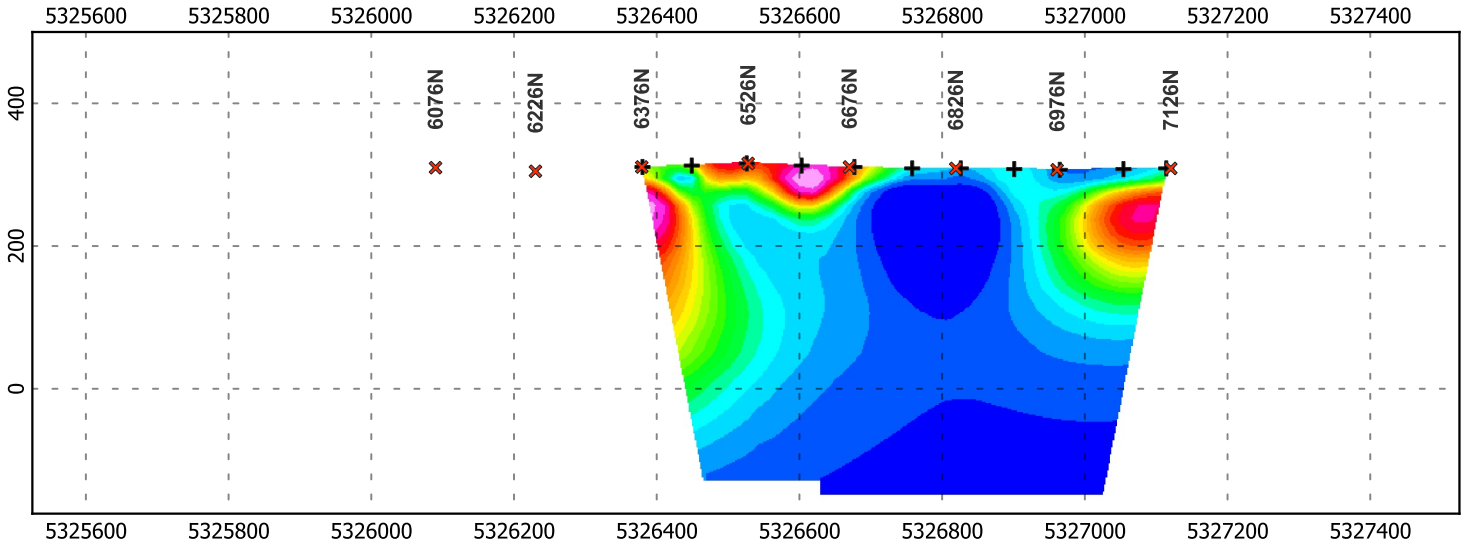
Inverted Resistivity

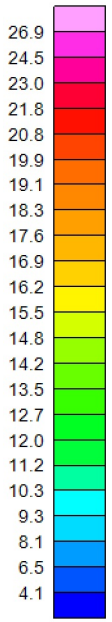




Inverted Resistivity (Ohm-m)

Inverted Chargeability

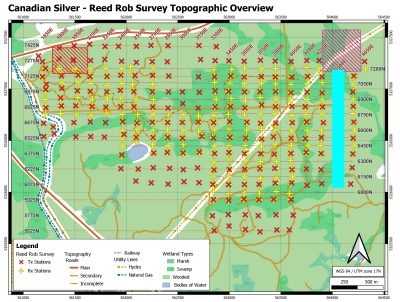




Inverted Chargeability (mV/V)

Reed-Robinson-L4500E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

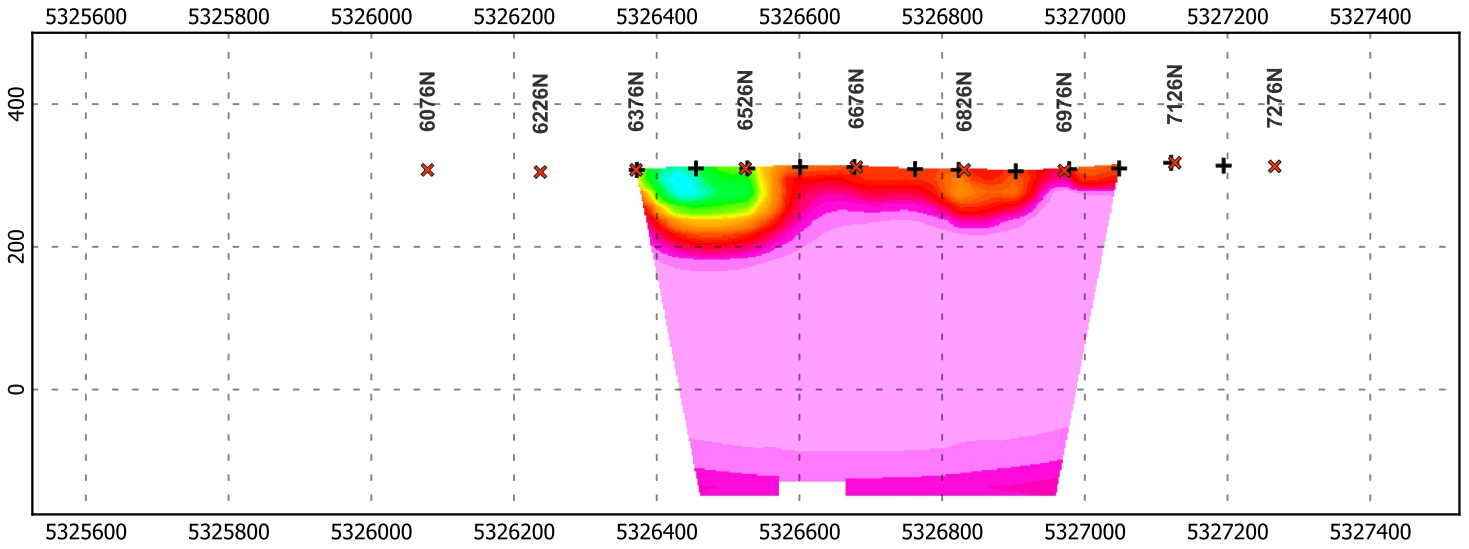
Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

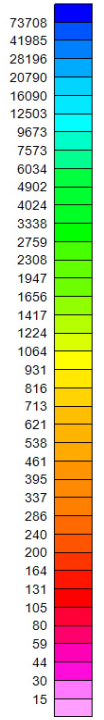
× Injection Stations
\+ Receiver Stations

0 100 200 m

DIAS GEOPHYSICAL

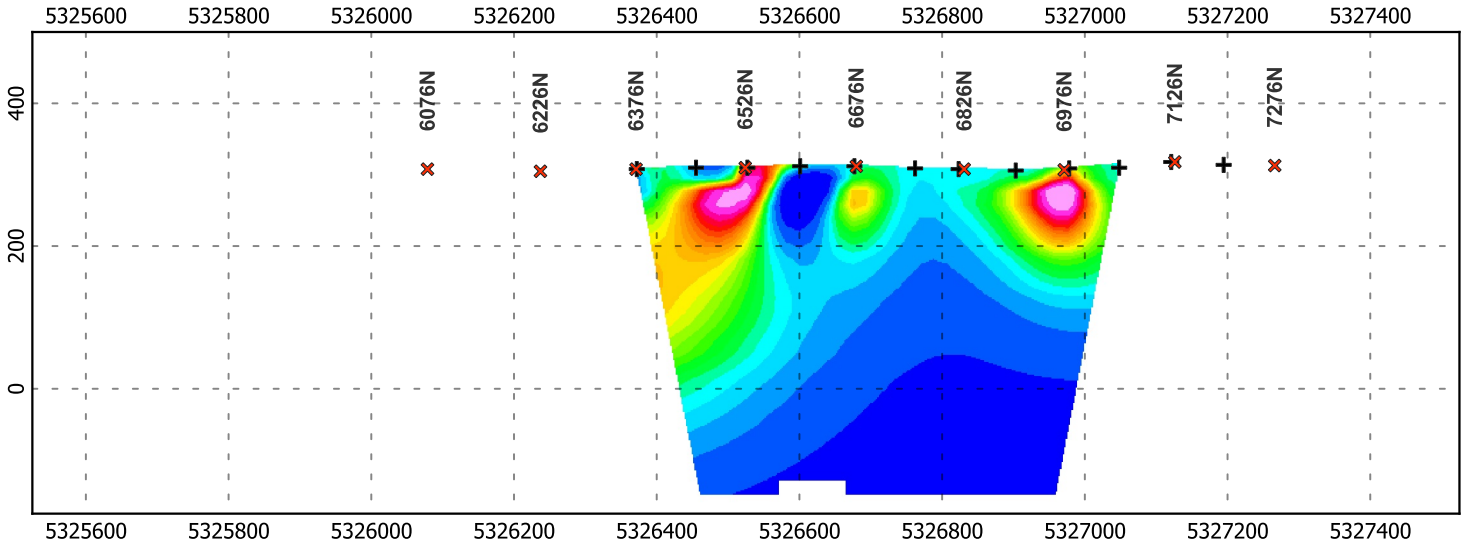
Inverted Resistivity

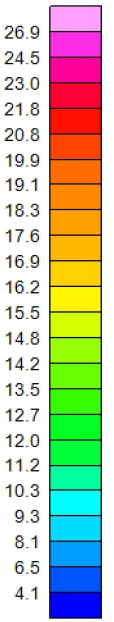




Inverted Resistivity (Ohm-m)

Inverted Chargeability

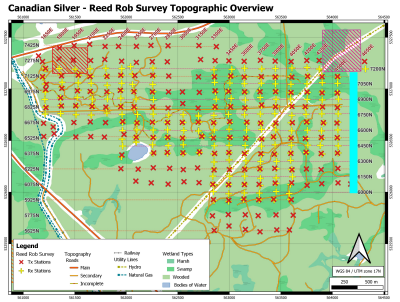




Inverted Chargeability (mV/V)

Reed-Robinson-L4650E Section extracted from 3D Inverted Model

Survey Date: 22 Oct - 16 Nov 2022
Mapping Date: December 2022
Surveyed By: Dias Geophysical Limited
Surveyed For: Canada Silver Cobalt Works Inc.



Survey Specifications:
-Array: Distributed CVR
-Configuration: Pole-Dipole
-Type: 3D
-Receiver Spacing: 75 m
-Current Injection Spacing: 150 m

Instrumentation:
- Receiver: DIAS-32-1 Single Channel Receiver
- Transmitter: Dias GS5000, 30kW
- Time Base: 2s ON/2s OFF
- 20 Time Windows - 40 ms delay
- Continuous Integration Window Widths: M1 to M20:
20,20,40,40,40,40,80,80,80,80,80,
80,80,80,160,160,160,160,160,160
- Integration window: 220-1940 ms

× Injection Stations
\+ Receiver Stations

0 100 200 m

DIAS GEOPHYSICAL

Appendix B

Dias Geophysical Logistics Report

Canada Silver Cobalt Works Inc.

LOGISTICAL REPORT

REED-ROBINSON PROJECT

ONTARIO, CANADA

3D DC RESISTIVITY AND

INDUCED POLARIZATION SURVEY

WORK PERIODS: OCTOBER 22 – NOVEMBER 16, 2022

UTM ZONE 17N NAD83

Prepared by: Dias Geophysical Limited
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Saskatchewan, S7L 7E1
Tel: +1.416.795.1263

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1. Introduction

Between October 22nd and November 16th, 2022, Dias Geophysical Limited carried out a 3D DC-resistivity and induced polarization (DCIP) program on the Reed-Robinson project for Canada Silver Cobalt Works Inc. ("Canada Silver Cobalt") using the DIAS32 system. The Reed-Robinson project sits within the Eby-Otto property located 10 km southwest of Kirkland Lake in Ontario, Canada.

The geophysical program carried out by Dias Geophysical Limited was designed to detect the electrical resistivity and chargeability signatures associated with potential targets of interest. This was achieved using the DIAS32 acquisition system in conjunction with one GS5000 transmitter. The 3D program, covering an area of approximately 3.75 km^2, was completed using a rolling distributed partial 3D DCIP array with a pole-dipole configuration.

This report provides a summary of the survey procedures, logistics and personnel and describes the equipment specifications, data acquisition procedures, processing procedures, and deliverables.

2. Property Location and Access

The Reed-Robinson project is located approximately 11 km south-west of Kirkland Lake. (**Figure 1** and **Table 1**). Accommodations were at the Prospector's Inn in Kirkland Lake. The drive to and from the grid was approximately 30 minutes.

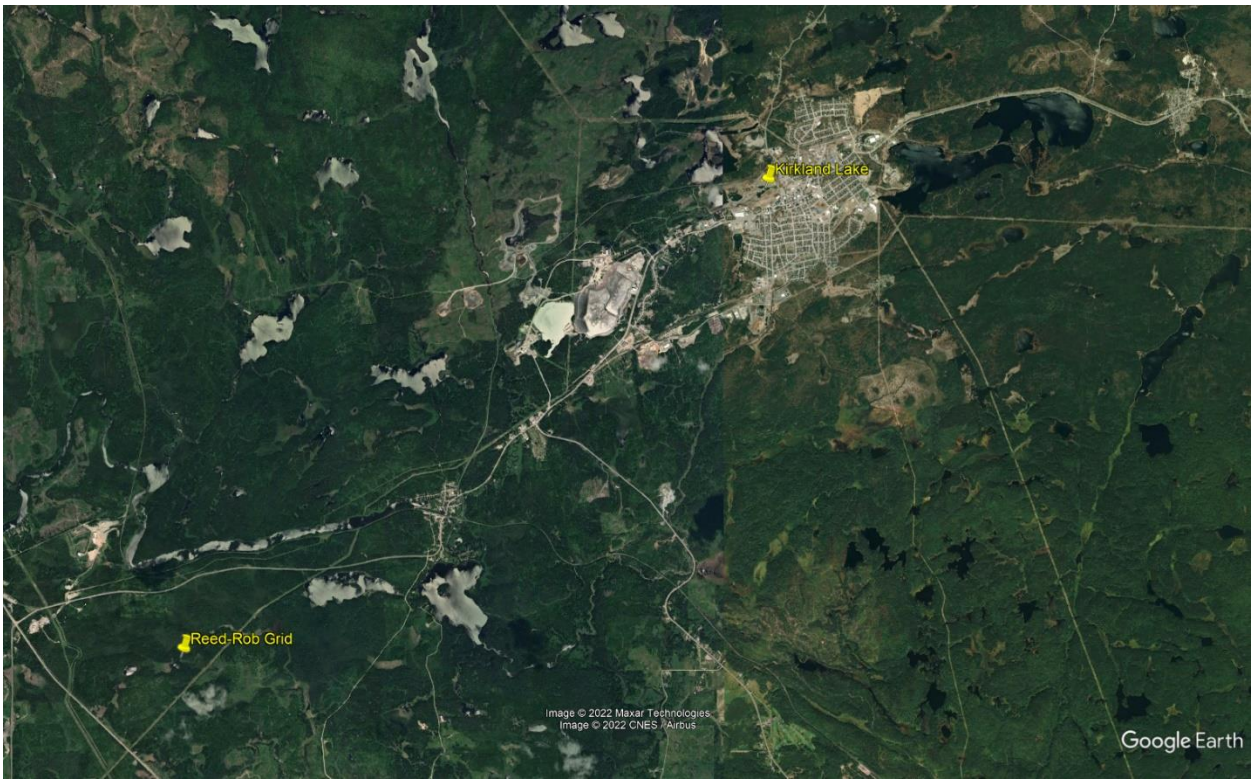


Figure 1: Locations of the Reed-Robinson Grid Relative to Kirkland Lake

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Table 1: Reed-Robinson Project Location & Access

Nearest Community:	Kirkland Lake, ON
Base of Operations:	Prospector's Inn – Kirkland Lake
Grid Location :	80° 9'21.43"W/48° 5'21.80"N
Transportation:	Grid Accessed via Truck Intra-grid movement via UTV

2.1 Physiography and Climate of Kirkland Lake, ON

The Reed-Robinson project is in the Province of Ontario, Canada at approximately 80° 9'W/48° 5'N. The area is in a boreal climate. The grid was between approximately 240 m and 300 m above msl. Over the course of this project, the air temperature varied between -3 ° and 15 °C, with precipitation in the form of rain and snow later in the season.

Climate data for Kirkland Lake (1981–2010) [hide]

Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Year
Record high °C (°F)	8.0 (46.4)	12.0 (53.6)	18.5 (65.3)	29.0 (84.2)	35.6 (96.1)	37.5 (99.5)	38.9 (102.0)	36.7 (98.1)	32.8 (91.0)	26.1 (79.0)	18.9 (66.0)	14.5 (58.1)	38.9 (102.0)
Average high °C (°F)	−10.3 (13.5)	−7.2 (19.0)	−0.7 (30.7)	7.6 (45.7)	16.2 (61.2)	21.3 (70.3)	23.9 (75.0)	22.1 (71.8)	16.3 (61.3)	9.0 (48.2)	0.2 (32.4)	−6.9 (19.6)	7.6 (45.7)
Daily mean °C (°F)	−16.9 (1.6)	−14.3 (6.3)	−7.4 (18.7)	1.6 (34.9)	9.7 (49.5)	14.9 (58.8)	17.8 (64.0)	16.3 (61.3)	11.2 (52.2)	4.7 (40.5)	−3.6 (25.5)	−12 (10)	1.8 (35.2)
Average low °C (°F)	−23.4 (−10.1)	−21.4 (−6.5)	−14 (7)	−4.4 (24.1)	3.1 (37.6)	8.4 (47.1)	11.7 (53.1)	10.6 (51.1)	6.1 (43.0)	0.5 (32.9)	−7.4 (18.7)	−17.2 (1.0)	−4.0 (24.8)
Record low °C (°F)	−47 (−53)	−43.5 (−46.3)	−41 (−42)	−28.9 (−20.0)	−12.2 (10.0)	−2.8 (27.0)	0.0 (32.0)	−1.0 (30.2)	−9.5 (14.9)	−13 (9)	−31.5 (−24.7)	−42 (−44)	−47 (−53)
Average precipitation mm (inches)	68.5 (2.70)	54.1 (2.13)	54.8 (2.16)	49.9 (1.96)	74.4 (2.93)	84.9 (3.34)	91.5 (3.60)	96.9 (3.81)	90.3 (3.56)	78.9 (3.11)	62.2 (2.45)	76.9 (3.03)	883.4 (34.78)
Average rainfall mm (inches)	2.2 (0.09)	1.4 (0.06)	10.9 (0.43)	27.5 (1.08)	72.8 (2.87)	84.9 (3.34)	91.5 (3.60)	96.9 (3.81)	90.3 (3.56)	74.9 (2.95)	23.8 (0.94)	3.0 (0.12)	580.0 (22.83)
Average snowfall cm (inches)	66.3 (26.1)	52.7 (20.7)	44.0 (17.3)	22.4 (8.8)	1.6 (0.6)	0.0 (0.0)	0.0 (0.0)	0.0 (0.0)	0.0 (0.0)	4.0 (1.6)	38.5 (15.2)	73.9 (29.1)	303.4 (119.4)
Average precipitation days (≥ 0.2 mm)	14.9	10.5	9.2	8.8	12.1	13.9	14.1	14.1	15.3	14.4	14.1	16.5	157.8
Average rainy days (≥ 0.2 mm)	0.31	0.44	1.7	5.3	11.9	13.9	14.1	14.1	15.3	13.0	4.0	0.87	95.0
Average snowy days (≥ 0.2 cm)	14.7	10.3	8.3	4.1	0.56	0.0	0.0	0.0	0.0	2.1	10.4	15.6	66.0

Figure 2: Kirkland Lake, ON, Canada, Climate

Source: https://en.wikipedia.org/wiki/Kirkland_Lake

2.2 Personnel

The Dias crew was comprised of a crew lead, one Dias Geophysical operator and an average of six field technicians. Few crew rotations occurred over the course of the project. All Dias personnel were trained on Dias' HSE policies and procedures relevant to the DIAS32 system and its application to the project. **Table 2** lists the personnel that were involved on the project.

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Table 2: Project Personnel

Field Staff	
Crew Supervisor:	Sam Rivera
Operator:	Nirab Sarma, Sam Rivera
Field Technicians:	Naomi Ratt, Moses Ballantyne, Sean Gunne, Finnigan Duffield, Josh McLeod, Kamal Abojnah, Michael Caisse, Naomi Ratt
HSE Representative:	Nirab Sarma
Office Staff	
Data Processing:	Charlotte Thibaud
Quality Control:	Charlotte Thibaud
Operations:	Aaron Snider, Liam McKinnon
Reporting:	Nirab Sarma and Charlotte Thibaud

3. Methodology and Procedures

3.1. HSEC

Dias Geophysical employs eCompliance, an online resource for the training, control, recording, and analysis of HSEC matters. Dias Geophysical carried out the following activities relating to HSEC over the course of the survey:

- Assign a designated health and safety representative (HSR) to the work site who oversees onsite Health and Safety and the OHS regulatory requirements. Nirab Sarma was assigned this responsibility.
- Completion of a Job Action – Job Plan
- Daily toolbox HSEC meetings
- Daily recording of Take 5s, Incident Reports, and Daily Check Lists
- Observance of the appropriate COVID-19 protocols

HSEC challenges included the following:

- Weather – The crew was exposed to variable weather over the course of the surveys, from moderate temperatures to cold and snowy conditions. Protective measures included dressing in appropriate layers, building a fire if having to wait in the field, and returning to the transmitter base station to warm up if getting too cold.
- Terrain – Muskeg, dense forest, and swamps. Appropriate footwear was used to stay warm and dry.
- High Voltage – Current transmission lines and active current electrodes. Protective measures included the use of a thorough current start-up and shut-down procedure between the field-based current crew and the geophysical operator.

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- COVID-19 – Risk of transmission between Dias crew members and people in town. Protective measures included the use of masks when proper physical distance could not be maintained and daily symptom monitoring.

3.2. Equipment

The DIAS32 DCIP system is described in **Table 3**. Further descriptions and specifications for this equipment are given in **Appendix A.**

Table 3: Systems Description

	System	#	Description
Safety			
	DIAS-LS System	3	Lightning mitigation system
	PPE	6	Personal protective equipment
Acquisition			
	DIAS32 Receiver	100	Single channel mesh network time-series receiver
	Control Computer	1	Operator's receiver control computer
	Electrodes	200	45 cm flat steel electrode
	Potential Wire	15 km	Insulated 16 AWG wire
Transmission			
	Generator	2	12.5 kW generator
	Transmitter	2	DIAS GS5000 transmitter
	Control Computer	1	Operator's transmitter control computer
	Electrodes	15	1-meter steel rod electrodes (including electrodes used for remote)
	Transmitter Wire	15 km	Insulated 16 AWG wire

3.3. Survey Methodology and Specifications

Dias Geophysical completed the Reed-Robinson grid using a 3D rolling distributed array in common voltage reference (CVR) mode as described below and summarized in **Table 4**. Characteristics of the survey layouts are as follows:

- The grid included 21 lines spaced 150m apart and of length varying between 0.45 to 1.275 km. All lines were oriented south-north with an azimuth of 0 °.
- All survey lines, labelled 3200E through 6400E, were used as both receiver and transmitter lines.
- Along the lines, receiver stations were spaced 75 m apart.
- Transmission stations were spaced 150 meters apart along each line, coincident with every second receiver station. Two extensions were done, when possible, to the north and south end of each line to improve depth resolution along the edges of the grid.

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- The current remote station was located approximately 1.75 km east of the eastern-most survey line (**Figure 3**).

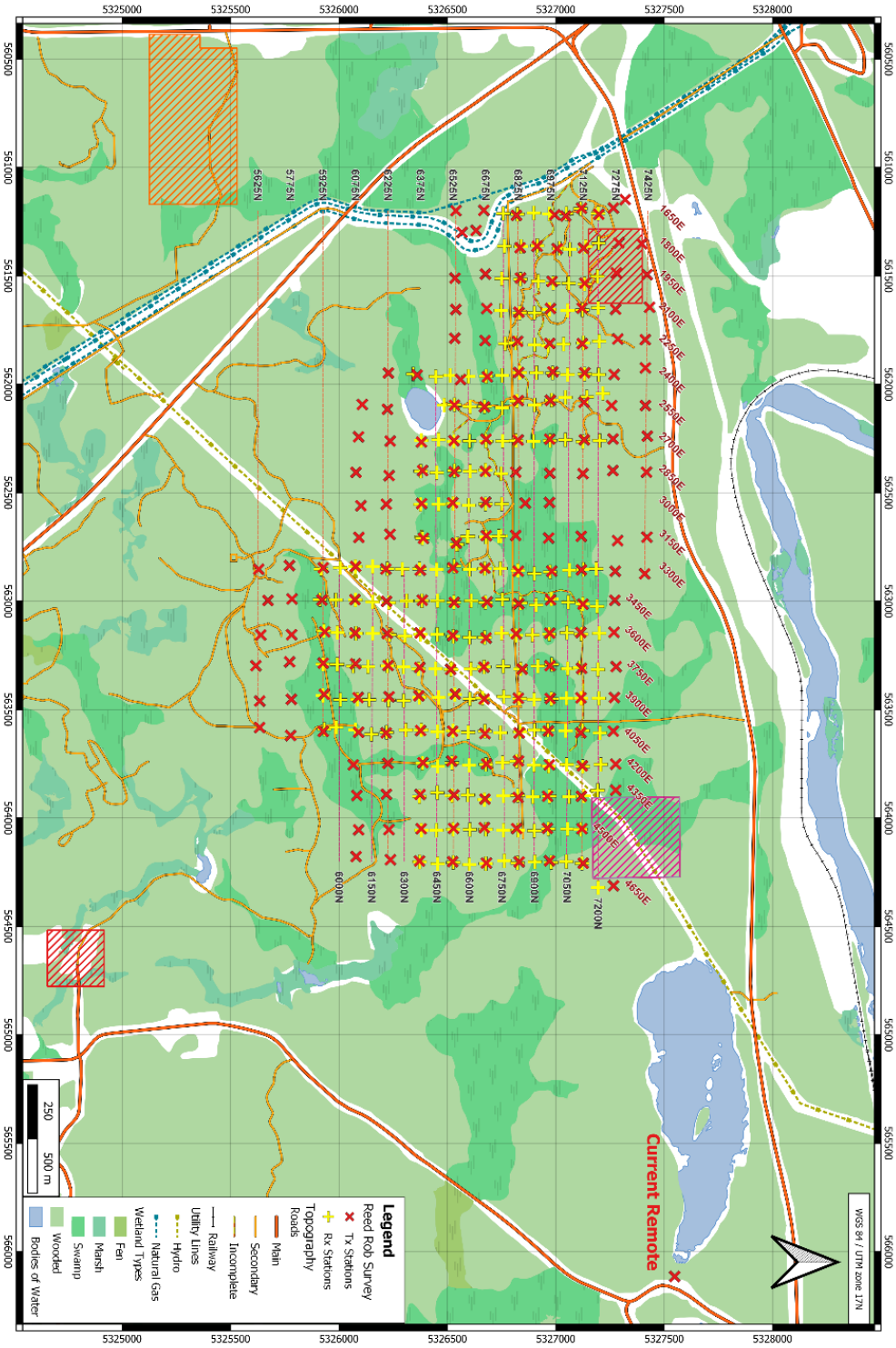


Figure 3: Reed-Robinson survey grid with current remote

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The survey procedures are as follows:

- The project was completed using a Pole-Dipole configuration.
- For each injection on the grid, a minimum of three receiver lines were active (see **Figure 4)**.
- When injecting current at a given station, the receiver located at this station was deactivated to avoid damages.
- Following the completion of an injection line, the receiver line configuration was incremented in preparation for the next line of injections by picking up the completed injection line and infilling the new injection line with receivers.

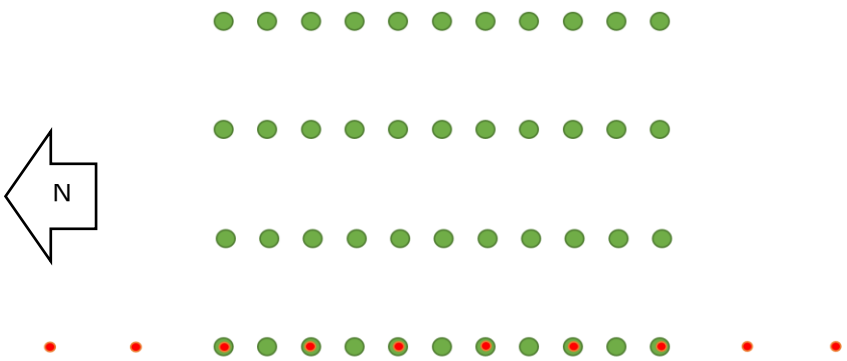


Figure 4: Generalized Survey Layout

The green and red dots represent the receiver transmitter stations, respectively. Transmits and receivers were setup along the same lines and were spaced 75 and 150 m apart. At any given transmit station, the coincident receiver was disabled to prevent damages. Up to two current injection extensions were carried out off the southern and northern edges of the lines.

Table 4: Survey Specifications

General Specifications	
Survey Mode:	Rolling Distributed 3D survey with CVR
Array Type:	Pole-Dipole
Receiver Specifications	
Electrode 'a'/line spacing:	75 m/150 m
Electrodes per injection:	21 to 65
Receiver Sampling Interval:	150 samples per second
Transmitter Specifications	
Current injection/line spacing	150 m/150 m
Current Remote Location:	566115E / 5327548N/320 m (NAD83Z17U)
Transmitter waveform:	50 % duty cycle, square wave
Transmitter base frequency:	0.125 Hz (8 second cycle)
Transmitter Injection Location:	Coincident with every second receiver station

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3.4. Survey Procedures

Grid Setup

All stations were established by the field crew using handheld Garmin 64s GPS devices. The coordinates of the actual stations were recorded and stored for data processing.

Electrode Installation

Dias deploys flat, stainless-steel electrodes driven into the ground at receiver stations. This type of electrode provides low noise characteristics for the band width of the survey. Electrodes are installed by driving the steel electrodes vertically into the ground to a minimum of 30 cm. The contact resistance of each electrode is tested, where the resistance exceeds 10,000 Ω the electrode is moved, or a second electrode is installed to reduce the contact resistance.

The local current electrode is comprised of two separate steel cylindrical 1-meter rods driven vertically into the ground. Where the ground contact was quite high salt water was added at the injection site. This was a result of rocky ground as well as freezing conditions. The remote site was comprised of 6 steel cylindrical 1.2-meter rods. The rods were placed in damp ground. Both the local current and current remote were deployed using 16 AWG transmission wire to the transmitter site.

Common Voltage Reference (CVR)

Dias employs a common voltage reference (CVR). Each receiver station has a dedicated DIAS32 receiver node connected to the CVR and a single receiver electrode. This allows each receiver node to record the voltage difference between the grounded electrode and the CVR wire. This produces a lower overall dipole measurement since the common voltage in the CVR wire are subtracted in the dipole computation.

Acquisition

CVR wire is deployed along all receiver lines to provide a CVR to receivers. Current injection wire is run from the transmitter site to the current remote location, where it terminates at the current remote stakes. A second current injection wire acts as the current feed and is run from the transmitter site to the active injection site. Two electrodes are driven into the ground at the active current injection site and are connected to the current feed wire. The procedure for power transmission is then initiated. Once the reading is complete and the procedure for ceasing power transmission is concluded, the current injection electrodes are removed and the crew advances to the next injection point. DIAS32 nodes and electrodes are installed before any injections take place and stay out for all injections.

Signal Transmission

A Dias GS5000 transmitter was used for the project to provide output up to 10.0 kW and 4000 V. The transmitted current ranged from ~100 mA to ~4.2 A for the grid (**Figure 5**) The current transmission was maintained for a recording time of 4 minutes per station, with the injection time being a function of current injected at each site. Since the injection site is coincident with the receiver locations, before injections, the receiver at that site was disconnected.

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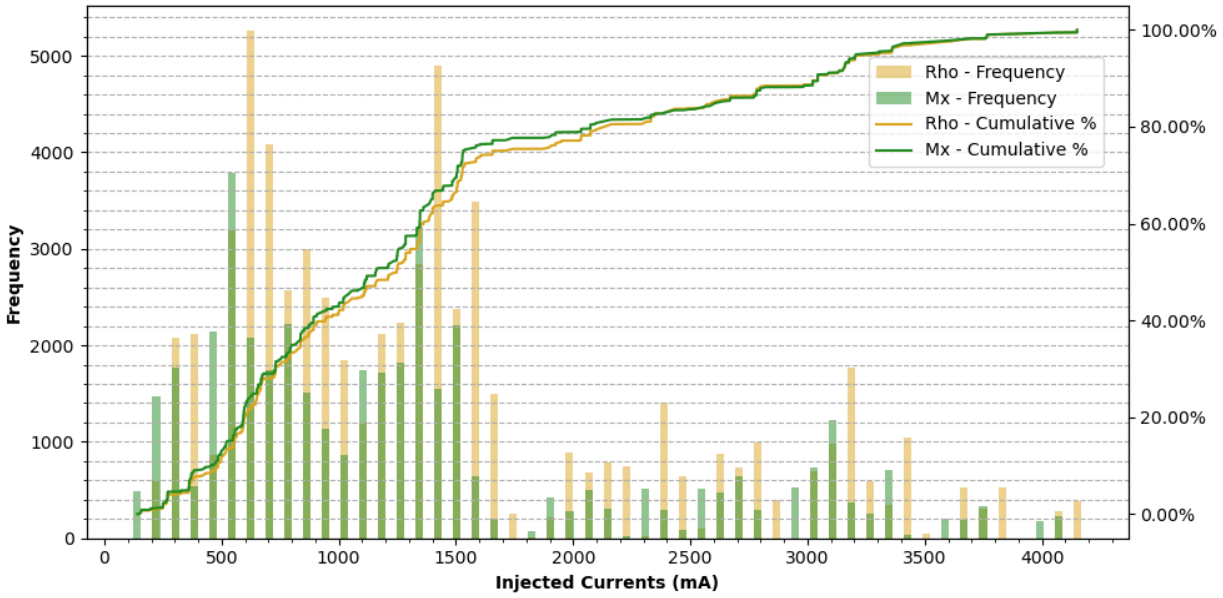


Figure 5: Transmitted Currents

In presence of high noise levels and/or low signal, longer readings were collected to help support the rejection of compromised segments of signal. In some areas of higher ground resistance, receivers located near the current injection tend to overvoltage, thus compromising data reliability. In these circumstances double injections are carried out: a first, 4 to 6 min injection at maximized current intensity with nearby receivers disconnected to provide good signal quality at medium and far offset, and a second, 2 min injection at a current amplitude low enough to prevent over-voltaging of the nearby receiver.

Where the current varied by more than 10% during this recording time, the transmission was terminated, the injection electrode contact was improved, and the transmission re-started to provide a stable current for the duration of the recording.

3.5. Survey Production and coverage

Following the completion of setup and barring any weather delays, production was consistent over the duration of the survey. A summary of the production notes can be found in **Appendix B**. Details of the survey coverage for the grid is given **Table 5**, respectively and illustrated on **Figure 6.**

Table 5: Receiver and Injection coverage over Reed-Robinson grid

Line	Rx			Tx		
	Station (From)	Station (To)	Length (m)	Station (From)	Station (To)	Length (m)
1650	7200	6750	450	7425	6975	450
1800	7200	6750	450	7275	6675	600
1950	7200	6750	450	7425	6525	900
2100	7200	6750	450	7425	6525	900
2250	7200	6750	450	7425	6525	900
2400	7200	6375	825	7425	6225	1200
2550	7200	6375	825	7425	6075	1350
2700	7200	6375	825	7425	6075	1350
2850	6750	6375	375	7425	6075	1350

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3000	6750	6375	375	6975	6075	900
3150	6750	6375	375	7425	6075	1350
3300	7200	5925	1275	7425	5625	1800
3450	7200	5925	1275	7275	5625	1650
3600	7200	5925	1275	7275	5625	1650
3750	7200	5925	1275	7275	5625	1650
3900	7200	5925	1275	7275	5625	1650
4050	7200	5925	1275	7275	5625	1650
4200	7200	6375	825	7275	6075	1200
4350	7200	6375	825	7275	6075	1200
4500	7125	6375	750	6975	6075	900
4650	7200	6375	825	7275	6225	1050
		Total	**16,725**	**Total**		**25,650**

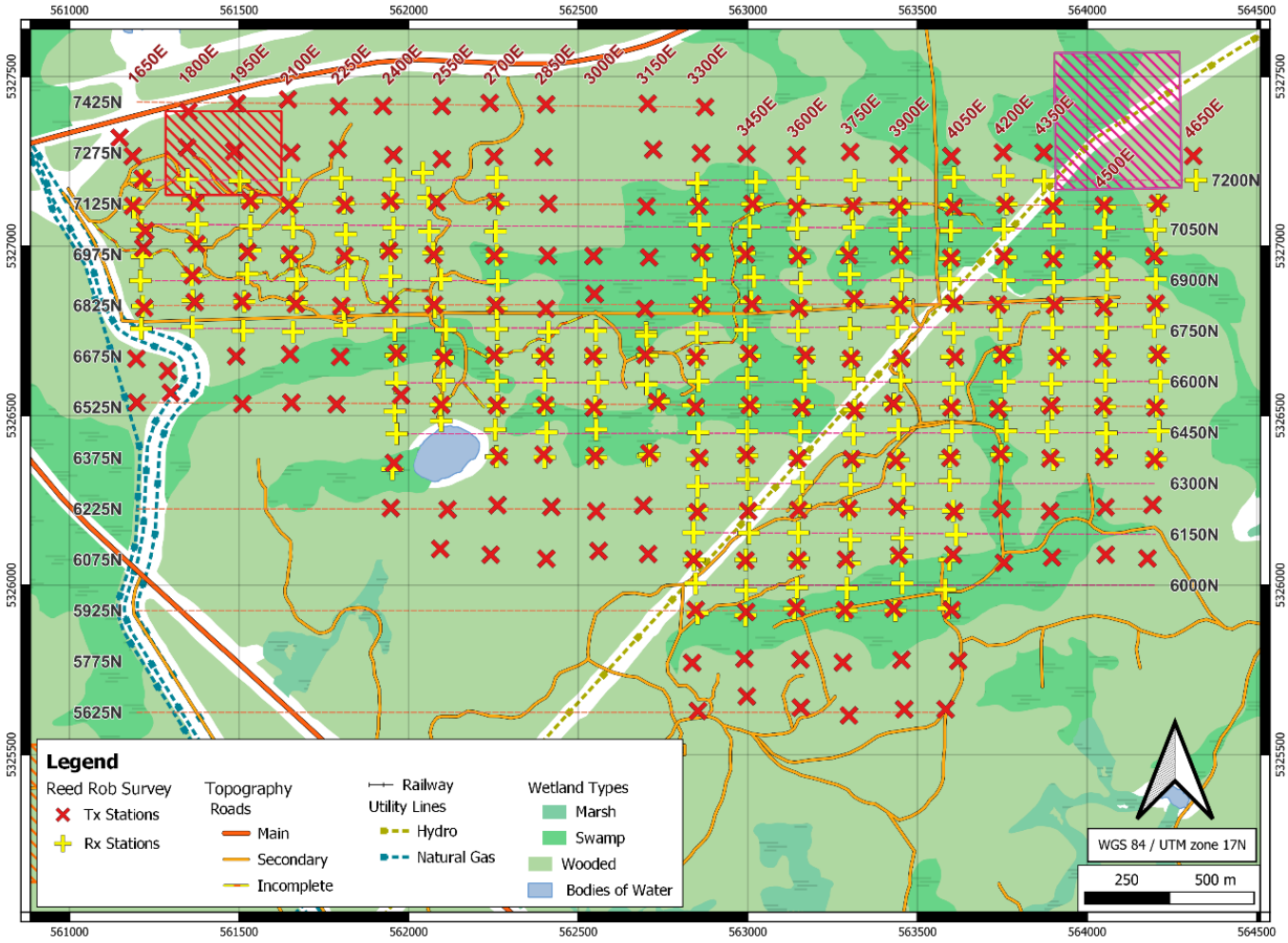


Figure 6: Overview of Reed-Robinson Grid

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4. Data Processing and Presentation

The DIAS32 receivers automatically record time series data stamped with GPS time and location information. In addition, time series recording of the current waveform is conducted at the current injection point. These two sets of time series data are processed using proprietary algorithms. A wide range of processing techniques are available (statistical rejection, ensembles, deep stacking, etc.). The most suitable processing technique will be determined based on the type of interference affecting the signal.

For the Reed-Robinson project the signal was processed using two different processing techniques. For most injections Overlapping Ensembles were use: the time series recorded by each receiver during each reading was split into 11 overlapping segments – or ensembles. Each ensemble was then analyzed for spikes and other statistical inconsistencies. The ensembles showing inconsistencies were then discarded and the remaining "clean" ensembles were stacked.

A few injections showed some isolated spikes that lead to noisy stacked signal. As a result, Statistical Rejection was used to process the signal as it is more stringent than Overlapping Ensembles when most of the recorded stacks are relatively clean. During the Statistical Rejection process, the dipole waveform is analyzed by half-period increments and all segment of the signal showing statistically abnormal noise levels are discarded. The remaining portion of the waveform is then stacked. This technique is particularly effective for injections where a low count of stacks showing high noise levels is observed.

The following information with each reading:

- current electrode location
- potential electrode locations
- primary voltage
- integrated normalized secondary voltages (i.e. chargeabilities) in milliseconds (ms)
- the transmitter current amplitude
- number of stacks
- standard deviation of the stacks
- time of the reading
- the amount and width of the secondary voltages (**Table 5**)

The signal was processed using regular stacking.

Table 6: Standard 2 second time-base time sample intervals

Sample #	Start Time (ms)	End Time (ms)	Sample #	Start Time (ms)	End Time (ms)
Delay	0	40	**11**	450	510
1	40	60	**12**	510	570
2	60	80	**13**	570	660
3	80	100	**14**	660	750
4	100	140	**15**	750	840
5	140	180	**16**	840	970
6	180	220	**17**	970	1100

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7	220	270	**18**	1100	1260
8	270	330	**19**	1260	1420
9	330	390	**20**	1420	1580
10	390	450	**21**	1580	1760
			22	1760	1940

The total integrated chargeability is computed as the sum of each normalized secondary voltage multiplied by the length of its sample interval, divided by the total sample interval (i.e., 1.9 s for the 2 seconds time-base data). In the case of the Reed-Robinson data the apparent chargeabilities were calculated using a reduced integration window (220-1940ms). All georeferenced results for this survey were provided in UTM Z17N WGS84.

Following is a general description of the workflow for the daily processing, verification, and imaging of the survey data.

- The time series data that are stored on the individual receivers are downloaded to the processing computer at the end of each production day. Each file is a self-sufficient fully described file which contains all meta-data, including location, time, and recording units.
- Once downloaded, these individual signal files are loaded into the Dias Processing Software environment for dipole creation and stacking:
    - Dipoles are generated based on a range of lengths input by the user (i.e. all receivers within that range of lengths will be paired up to form dipoles). The choice of lengths depends on the receiver station spacing, both along and across lines. Although this is highly dependent on the needs of the project and survey configuration, it is customary to generate dipoles that extend over 2x the station spacing both along and across lines. Two approaches are available:
        - Blanket dipole generation: all possible dipoles between the minimum and maximum dipole lengths are generated using all available receivers for each injection. This option generates the maximum number of dipoles and is well suited for medium to high resistivity environments. It is also the most computer-intensive and lengthy option.
        - Smart dipole generation: the user enters a minimum and maximum dipole length for the close-offset dipoles. This range will be adjusted automatically to increase with the distance to the current injection. This option allows to maximize the signal/noise ratio and is best suited for more conductive environments. It also minimizes computing time, focusing on generating dipoles that will yield the strongest possible signal.
    - Where no data irregularities are encountered, the data are processed using proprietary processing algorithms that stack the data, apply noise reduction strategies, and compute apparent resistivity and chargeability.
    - The error on the Vp is also calculated during this step. It is based on the mean difference between the sampled values over the window used for the Vp calculation and is designed to represent the stability of the signal. The same is done for the current and the

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combination of the two errors (Vp error/I error) is assigned as the error on apparent resistivity as used by certain inversion algorithms (UBC GIF for example).

- The resulting data are then concatenated in a single database where they can easily be displayed for verification, processing, and visualization.
- The processed data are organized by their respective survey grid and displayed in a point-cloud format along with all other data from that grid.
- Data quality control included an assessment of the following outputs and factors:
  - Locations: all receiver/transmitter locations, including elevations, are compared to corresponding hand-held GPS locations to ensure consistency. Grid coordinates are assigned to each survey station. Occasionally, the GPS elevations are replaced by elevations extracted from a NTS digital elevation model[1].
  - Transmitter current stability: the amplitude of the injected current needs to remains stable over the course of the reading. If the injection were to vary or become abnormal the signal can be trimmed to only retain the sound portion of the injection
  - Waveform stacks: gives a quick snapshot of the signal/noise ratio
  - Spectral analysis: represents the signal in frequency domain to identify the frequency associated with potential cultural noise (power lines in particular) so proper signal procedure can be devised
  - Final decay: during the QC process the data set is run through a Cole-Cole rejection algorithm and the decays that are deemed untrustworthy are automatically rejected. During this process the Mx error is calculated based on the standard deviation of the measured decay relative to its Cole-Cole fit. Note that once the Cole-Cole rejection is complete the rejected decays are inspected one-by-one. Most rejected decays will receive further signal processing such as statistical rejection or ensemble stacking to try and eliminate the potentially bad cycles responsible for the noise in the decay. This technique reduces manual quality control time while maximizing data recovery.
  - Resistivity statistics: the rho values are plotted versus their corresponding mx values to obtain an estimate of the general data distribution. Any tailing values (i.e. very high/low rho/mx) are then automatically rejected.
  - Measurement point clouds: a final visual check is carried out on the data to ensure that the data look consistent and detect potential inconsistencies in the data distribution. Individual data points in the point clouds can be analyzed interactively to determine the source of any irregularities.
  - Geometry testing: the coupling angle is calculated between the receiver and transmitter dipoles and is compared to the Vp values for each dipole. The poorly/null coupled zone is based on the value of the coupling angle beyond which the Vp value is deemed untrustworthy. Since each project is different (i.e., line/station spacing and layout) the range of the coupling angle is highly project dependent.
- Final processed data were exported as Dias and Geosoft formats as well as xyz point cloud in UTM Z17N/NAD83 coordinates.

[1] https://maps.canada.ca/czs/index-en.html

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For the Reed-Robinson Project dipoles of lengths varying between 75 and 750 m were generated using the blanket approach. In the case of this grid, for each injection with 3 – 4 active receiver lines, approximately 200 – 1500 receiver dipoles were generated, yielding a final dataset with approximately 88120 pole-dipole data points over the entire grid for 231 injection points. The azimuthal distribution of the dipoles (angle between the injection point and the midpoint of the receiver dipoles and the receiver dipole itself) is illustrated in **Figure 7** below.

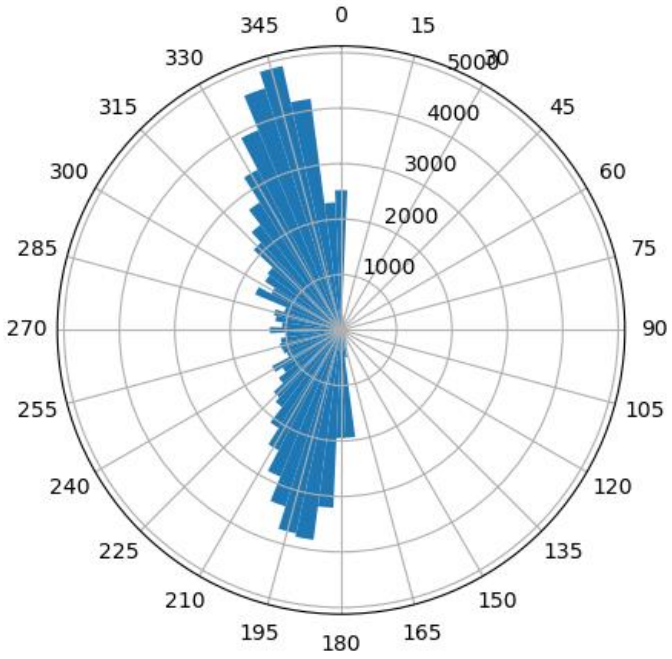


Figure 7: Azimuthal distribution for the Reed-Robinson project.

5. 3D Inversion Modeling

After a thorough quality control, all the "accepted" data were used to produce a set of unconstrained 3D DC and IP models using the SimPEG inversion code (version 1.4 -https://www.simpeg.xyz/).

Following is the general procedure for producing the 3D models:

1. Carry out preliminary unconstrained inversion using a coarse mesh to establish the inversion parameters and identify any remaining data quality issues. The coarse mesh cell size of 1/2 of the closest nominal spacing between receiver electrodes in the horizontal direction. Vertical cell size increases progressively at depth to mimic the loss of sensitivity with a minimum size of ½ of the horizontal cell sizes.

2. Re-process or remove any data points that came up with high residual in the coarse mesh inversion and modify inversion parameters as required based on the results of step 1.

3. Carry out final unconstrained inversion using a fine mesh to yield the final 3D models. The fine mesh size is normally 1/4 of the closest nominal spacing between receiver electrodes in the horizontal and vertical directions.

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4. Modify the inversion parameters as needed to improve the model results until the fine models are considered acceptable.

The parameters used for the Reed-Robinson grid DC and IP fine inversions are listed in **Appendix C**, together with the corresponding fitting parameters. A flat standard deviation error combined with a floor were assigned as uncertainties for both DC (error = 15% and floor = 10th percentile) and IP (error = 15% and floor = 1e-5mV/V) inversions. The DC inversion was carried out first followed by the IP inversion and both inversions used uniform background. The final DC model was used for the IP inversion. IP inversions were carried out with trimmed (220-1940ms) integration windows.

The inversions were carried out in UTM coordinates, and the current remote was included in the inversion calculation. Both coarse and fine inversions were carried out using Topography was also incorporated in the inversion using the same NTS DEM used to update the survey elevations.

Once an inversion completed, all iterations were examined independently, and the most suitable models were chosen. The model whose achieved misfit was closest to the amount of data points used in the inversion were delivered as final model. Intermediate iterations of the inverted data can be made available upon request.

The resulting models were gridded and trimmed using Geosoft Oasis software and then converted into the UBC-GIF Tensor Mesh, XYZ-cell centered and Geosoft Voxel Format. The DC model is expressed in Ohm-m (resistivity model) and Siemens (conductivity model) and the Chargeability model in mV/V.

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6. Deliverables

Following is a list of the deliverables for this project:

1. Logistical report in digital format (PDF).
2. Digital data:
    a) Apparent resistivity, apparent chargeability data (calculated for an integration window spanning from sample #6 to sample #22) for ~75 m to ~ 750 m dipole sizes over the grid, in Dias and Geosoft-compatible formats complete with station locations in UTM Z17N/WGS84 coordinates.
    b) XYZ point cloud of the apparent resistivity and chargeability data for both datasets., provided in UTM Z17N/WGS84 coordinates.
    c) Full grid coordinates in .csv format.
    d) Unconstrained fine 3D inversion models obtained using Tensor mesh SimPEG, in Voxel, UBC and XYZ formats.
    e) Plan and section maps of the inverted Resistivity and Chargeability models

The raw time-series data are recorded and archived at Dias' offices. These data can be made available to the client on request.

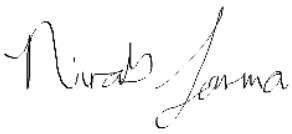
Respectfully Submitted,



Jonathan Rudd, P.Eng.
President



Charlotte A. Thibaud, M.Sc.,
P.Geo, Geophysicist



Nirab Sarma, B.Sc.
Dias Geophysical Operator

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Appendix A– Instrument Specifications

DIAS-32 RECEIVER	
SPECIFICATIONS	
Number of channels:	Single channel, unlimited channels per system
Survey capabilities:	Resistivity and Time domain IP
Acquisition:	Time series recording, up to 200 samples per second
Chargeability windows:	Arithmetic, log, semi-log, IPR-12 and user defined
Synchronization:	GPS PPS-based synchronization with internal clock failover
Noise reduction:	Automatic stacking number
Computation:	Apparent resistivity, chargeability, noise statistics
Size:	16 X 9 X 5 cm (6.3 X 3.5 X 2 in)
Weight:	Receiver: 0.6 kg (1.3 lb); Tablet 1.3 kg (2.9 lb)
Enclosure :	ABS, IP66
Communication :	USB, wireless mesh network, WiFi
Temperature range :	-45 to +50°C (-49 to +122°F)
Environmental:	Dustproof, water resistant
Power:	Lithium-Ion internal rechargeable - >4 days nominal @ 20°C
ELECTRICAL SPECS	
Ground Resistance:	Up to 2 MΩ
Signal waveform:	Time domain, 50% duty cycle square wave, (ON+, OFF, ON-, OFF)
Time base:	0.5, 1, 2, 4 and 8 seconds or custom
Input impedance:	80 MΩ
Voltage Range:	±2.5 V
Voltage measurement:	True differential for common-mode rejection in dipole configuration Resolution 1 µV
Filter:	Low-pass and 50 Hz / 60 Hz notch filters
OPERATOR COMPUTER	
Tablet: **Operating system:** **Quality Information:**	Standard Windows Computer or Tablet equipped with mesh network capability Vp/Vs data, Vp/Vs plots, real-time pseudo sections, current information, full-wave display as needed

The DIAS32 receivers record the time series voltage at each electrode relative to a local reference electrode.

DiasTx GS5000 Transmitter	
GENERAL CHARACTERISTICS	
Enclosure:	iM2620 Pelican Storm Case
Survey capabilities:	Time Domain DCIP, Frequency Domain DCIP, CSAMT
Dimensions:	53.8 cm x 40.6 cm x 26.9 cm
Weight:	31.5 kg (69.5 lbs)
Synchronization:	GPS PPS-based synchronization with internal clock failover
Exterior:	High performance resin
Waveform:	Programmable, current or voltage controlled
Command and control:	Wired external power on/off/kill, wireless control tablet
Temperature range:	-45 to +50°C (-49 to +122°F)
Environmental:	Dustproof, water resistant
Power:	External – up to two input sources
ELECTRICAL CHARACTERISTICS	
Input Power:	Up to 25 kW in single unit mode, up to 100 kW in combination
Input Sources:	DC, 3-phase, single phase (power is derated with single phase)
Output Current:	0.1 A to 20 A per unit; up to 80 A with 4 units combined
Output Voltage:	10 V to 5,000 V
Current Stability:	+/- 0.1%

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Appendix B – Production Summary

Survey Production		
Total 3D Coverage	3,75 km^2	
Dedicated Set-up Dates	Oct 25, Nov 12, 14 - 16	
Production Dates	26 Oct – 11 Nov, 13 Nov	
Standby Dates (Including partial)	NA	
Date	Production (injections)	Mob/Demob/Notes
22-Oct		Josh, Kamal, Sean, Moses, Sam, Finn Mobilize
23-Oct		Josh, Kamal, Sean, Moses, Sam, Finn Mobilize
24-Oct		Josh, Kamal, Sean, Moses, Sam, Finn, Henry, Nirab Mobilize
25-Oct	Setup	
26-Oct	13 injections L1650: 6525 - 7050 L1800: 6975 - 7425	
27-Oct	11 injections L1800: 6525 - 6825 L1950: 6825 - 7425 L2100: 6525 - 6675	
28-Oct	10 injections L1950: 6525, 6975 L2100: 6675 - 7425 L2250: 6525 - 6825	
29-Oct	12 injections L1950: 6525 L2250: 6975 - 7425 L2400: 6625 - 7125	
30-Oct	5 injections L2400: 7275 - 7425 L2550: 6525 - 6825	
31-Oct	18 injections L2550: 5625 - 5775, 6975 - 7425 L2700: 5625 - 7425 L2850: 6525 - 6825	
1-Nov	18 injections L2850: 6075 - 6375, 6975 - 7425 L3000: 6075 - 6975 L3150: 6225 - 6675	
2-Nov	6 injections L3150: 6075, 6825 - 7425	

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3-Nov	14 injections L3450: 5625 - 7425	
4-Nov	8 injections L3450: 5625 - 6675	Moses demobilizes, Abishek Mobilizes
5-Nov	10 injections L3450: 6825 - 7275 L3600: 5625 - 6225, 6825	
6-Nov	16 injections L3600: 6375 - 6675, 6975 - 7275 L3750: 5975 - 7275	
7-Nov	14 injections L3750: 5625 - 7425 L3900: 5625 - 7275	
8-Nov	12 injections L4050: 6525 - 7275	
9-Nov	10 injections L4050: 6525 L4200: 6075 - 7275	
10-Nov	4 injections L4350: 6825 - 7275	Michael, Naomi Mobilize
11-Nov	5 injections L4350: 6075 - 6675	
12-Nov		Setup / Line cutting
13-Nov	9 injections L4650: 6075 - 6525 L4500: 6525, 6375 - 6525	
14-Nov		Setup / Line cutting
15-Nov		Setup / Line cutting
16-Nov		Setup / Line cutting

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Appendix C– Inversion Specifications

Inversion Code Used	SimPEG 3D v2.0
Database used for the fine inversion	ReedRobinson_Finalized_IPDB.dat
Estimated DOI	Approximately 400m below topography
DC Inversion	
Uncertainties	15% standard deviation + 10 percentile floor
Starting/Initial model	Median of Apparent Resistivity data
Reference model	None
Weight	Surface weights (75,50,25,10,5)
Alphas/Length scales	1e-5, 1, 1, 2 (alpha s, x, y, z)
Inverted models' unit	Resistivity: Ohm-m / Conductivity: Siemens (S)
Fine Inverted Conductivity Model	ReedRobinson_Fine_Con.mod
Fine Inverted Resistivity Model	ReedRobinson_Fine_Res.mod
IP Inversion	
Uncertainties	15% standard deviation + floor of 1e-5 mV/V
Starting/Initial model	1e-5 mV/V
Property used for inversion (Mx or Voltage)	Voltage
Starting conductivity model used?	Yes. Iteration 10 (final DC model)
Weight	Surface weights (75,50,25,10,5)
Alphas/Length scales	1e-5, 1, 1, 2 (alpha s, x, y, z)
Inverted model unit	mV/V
Fine Inverted Chargeability Model	ReedRobinson_Fine_Chg.mod

DC misfit parameters:

#	beta	phi_d	phi_m	phi_m_small	phi_m_smoomth_x	phi_m_smoomth_y	phi_m_smoomth_z	phi
1	8.37E-08	1.45E+06	1.38E+08	4.83E+07	1.79E+07	4.65E+03	3.67E+07	7.05E+06
2	1.67E-08	6.92E+05	6.26E+08	1.76E+08	9.13E+07	3.03E+04	2.19E+08	1.45E+06
3	3.35E-09	5.52E+05	2.33E+09	4.10E+08	3.68E+08	1.92E+05	1.23E+09	6.92E+05
4	6.70E-10	4.73E+05	3.10E+09	4.13E+08	5.45E+08	3.40E+05	1.78E+09	5.52E+05
5	1.34E-10	3.88E+05	3.42E+09	4.52E+08	5.90E+08	3.70E+05	2.00E+09	4.73E+05
6	2.68E-11	3.26E+05	4.80E+09	5.40E+08	8.69E+08	6.18E+05	2.88E+09	3.88E+05
7	5.36E-12	3.10E+05	4.90E+09	5.47E+08	8.85E+08	6.40E+05	2.94E+09	3.26E+05
8	1.07E-12	2.99E+05	5.02E+09	5.49E+08	9.10E+08	6.74E+05	3.01E+09	3.10E+05
9	2.14E-13	2.90E+05	5.27E+09	5.66E+08	9.61E+08	7.28E+05	3.17E+09	2.99E+05
10	4.29E-14	2.86E+05	5.43E+09	5.72E+08	9.93E+08	7.69E+05	3.26E+09	2.90E+05

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IP misfit parameters:

#	beta	phi_d	phi_m	phi_m_small	phi_m_smoomth_x	phi_m_smoomth_y	phi_m_smoomth_z	phi
1	1.88E-04	2.73E+05	2.25E+04	6.01E+03	3.07E+03	1.58E+00	8.69E+03	8.34E+05
2	6.27E-05	2.22E+05	4.45E+04	9.20E+03	7.23E+03	5.85E+00	2.12E+04	2.73E+05
3	2.09E-05	2.03E+05	7.70E+04	1.35E+04	1.39E+04	1.34E+01	4.01E+04	2.22E+05
4	6.96E-06	1.94E+05	8.47E+04	1.39E+04	1.64E+04	1.72E+01	4.53E+04	2.03E+05
5	2.32E-06	1.87E+05	8.50E+04	1.39E+04	1.65E+04	1.79E+01	4.54E+04	1.94E+05
6	7.74E-07	1.80E+05	1.38E+05	1.87E+04	2.93E+04	3.50E+01	7.94E+04	1.87E+05
7	2.58E-07	1.78E+05	1.82E+05	2.21E+04	4.02E+04	5.25E+01	1.08E+05	1.80E+05
8	8.60E-08	1.76E+05	1.49E+05	1.93E+04	3.21E+04	4.22E+01	8.68E+04	1.78E+05
9	2.87E-08	1.73E+05	1.77E+05	2.18E+04	3.85E+04	5.12E+01	1.05E+05	1.76E+05
10	9.55E-09	1.72E+05	1.74E+05	2.14E+04	3.82E+04	5.14E+01	1.04E+05	1.73E+05

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Appendix D – Certificate of Qualifications

Jonathan Rudd

I, Jonathan Charles Rudd, of the municipality of Cambridge, region of Waterloo, province of Ontario, hereby certify:

- I am a geophysicist with Dias Geophysical Limited located at 54 Alona Avenue, Cambridge, ON, N3C 3Y4.
- I am a Professional Engineer registered with the Association of Professional Engineers of Ontario (APEO).
- I hold the following university degree: Bachelor of Science in Engineering, Geological Engineering, Geophysics specialization, Queen's University, 1988.
- I have no direct interest in Canada Silver Cobalt Works Inc., or the above-described properties and projects that are the subject of this report, nor do I intend to have any direct interest in these properties and/or projects.

Dated at Cambridge this 9th Day of December 2022.



Jonathan Rudd, B.Sc.,
P.Eng., Geophysicist

Charlotte A. Thibaud

I, Charlotte Anne Thibaud, of the municipality of Vancouver, province of British Columbia, hereby certify:

- I am a geophysicist with Dias Geophysical Limited located at 609-888 West Hastings Street, Vancouver, British Columbia, V6B 4W4
- I am a Professional Geoscientist registered with Engineers and Geoscientists of British Columbia (EGBC).
- I hold the following university degree: Mastère of Earth Sciences, Geophysics specialization, École et Observatoire des Sciences de la Terre (EOST), Université de Strasbourg et CNRS, 2007.
- I have no direct interest in Canada Silver Cobalt Works Inc., or the above-described properties and projects that are the subject of this report, nor do I intend to have any direct interest in these properties and/or projects.

Dated at Vancouver this 9th Day of December 2022.



Charlotte A. Thibaud, M.Sc.,

P.Geo. Geophysicist

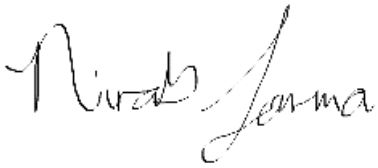
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Nirab Sarma

I, Nirab Sarma, of the municipality of Vancouver, province of British Columbia, hereby certify:

- I am a Dias Geophysical Operator with Dias Geophysical Limited located at 609-888 West Hastings Street, Vancouver, British Columbia, V6B 4W4
- I hold the following university degree: Bachelor of Science Hon. in Geophysics, University of British Columbia, 2021.
- I have no direct interest in in Canada Silver Cobalt Works Inc., or the above-described properties and projects that are the subject of this report, nor do I intend to have any direct interest in these properties and/or projects.

Dated at Vancouver this 9th Day of December 2022.



Nirab Sarma, B. Sc.

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Appendix E – References

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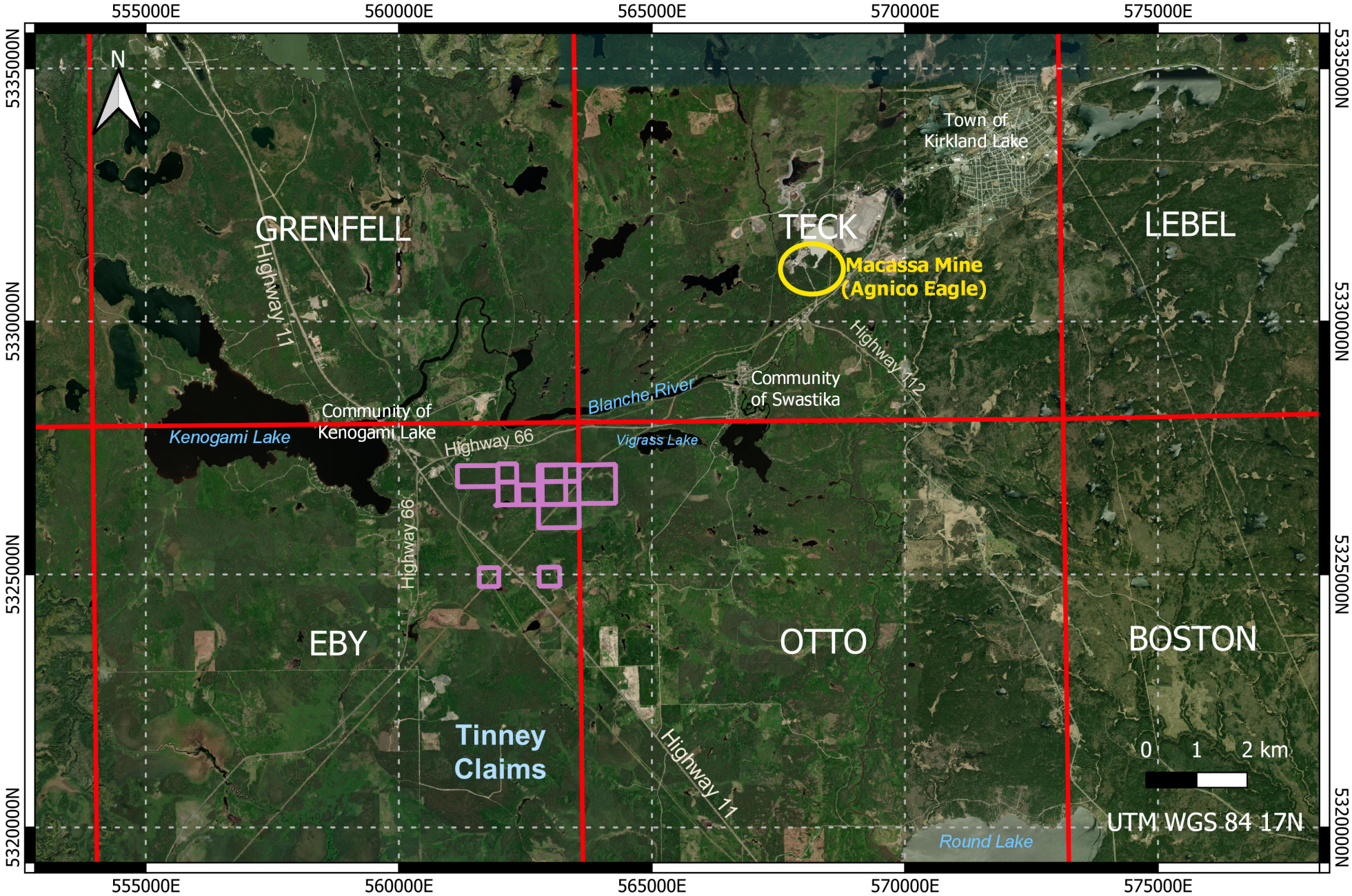
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Appendix C

Invoices


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565000E
570000E
575000E
5335000N
5330000N
5325000N
5320000N
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GRENFELL
TECK
LEBEL
EBY
OTTO
BOSTON
Town of
Kirkland Lake
Macassa Mine
(Agnico Eagle)
Highway 11
Highway 112
Blanche River
Community
of Swastika
Community of
Kenogami Lake
Kenogami Lake
Highway 66
Vigrass Lake
Tinney
Claims
Round Lake
0 1 2 km
UTM WGS 84 17N