42A01SE0028 2.15784 EBY

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ASSESSMENT REPORT, GEO

42A01SE0028 2.15784 EBY

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INVOICE FOR MaxMin EM SURVEY OF JAMES REED CLAIM GROUP IN OTTO AND EBY TOWNSHIPS

A. INTRODUCTION

On August 10-12, 1994, Dec 31, 1994 and January 1, 1995 a MaxMin horizontal loop EM survey was carried out on the Otto-Eby Township property held by James D. Reed, E. L. Reed, N. E. Reed and C. E Reed. Douglas Robinson, the author of this assessment report supervised the field work performed by Douglas Robinson, Graham Robinson, David Robinson and Adam Gasper.

This work was done in conjunction with geological mapping and a total field-magnetic gradient survey to define target areas for advanced gold exploration. Several strong EM conductors appear to mark horizons that could host primary gold mineralization or be chemical-structural traps hosting vein gold deposits. Several out of phase anomalies on strike with strong IP and OP EM anomalies are coincident with Fe-carbonate alteration zones. The intersection EM conductors and two sets of Fe-carbonate alteration zones striking at 080° and 130-145° are prime targets for gold deposits.

B. PROPERTY

The property consists of a single group of 5 claims (8 claim units) consisting of: a single 4 unit claim in the north east quarter of Eby Township (Plan # M-345) and 4 single unit claims in Otto Township (Plan # M-379); all in the Larder Lake Mining Division.

1187002 - S 1/2 of S 1/2 of Lot 1, Conc VI, Eby Tp (4 units)
475259 - NE 1/4 of S 1/2 of Lot12, Conc VI, Otto Tp (1 unit)
475260 - SE 1/4 of S 1/2 of Lot12, Conc VI, Otto Tp (1 unit)
475261 - SW 1/4 of S 1/2 of Lot12, Conc VI, Otto Tp (1 unit)
475258 - NW 1/4 of S 1/2 of Lot12, Conc VI, Otto Tp (1 unit)

C. LOCATION

The claim group is centred at Latitude 48°05'30" and Longitude 80°08'45" (UTM Zone17: 5326500N, 564000E). Refer to the south-central portion of NTS Map Sheet 42 A/1 for the general location of these two groups (Figure 1). The bulk of the proposed work is concentrated on claims 1187002, 475258 and 475261, 700 m South of Highway 66, 10 km west of Kirkland Lake (Figure 2a).

The locations of the property is outlined in Figure 1. General Location of Claim Groups, Figure 2. Claim Map; Eby Tp, Figure 3. Claim Map; Otto Tp and Figure 4a. General Geology.

D. ACCESS

The property is best accessed from Highway 66 at a point 5.3 km west of the intersection of Highways 11 and 66. At this point, park at the Eby-Otto Township line. Walk 400 m south along the clearly cut township line to the #1 post of claim 1187002.

E. SURVEY DATES AND SUPERVISION

The EM survey was supervised by Douglas Robinson the author of this report. Work dates are recorded on the enclosed invoices.

F. DEPOSIT TYPE AND GEOLOGY

Gold is the primary exploration target; however potential exists for platinum or nickel-copper-platinum deposits hosted in coarse grained differentiated gabbro-diorite intrusives.

The western part of the property falls within the north eastern portion of an east-west trending 3 X 1.5 km zone of mafic rock mapped as intrusive gabbro and diorite (Map P.448). 1994 mapping (this group and a second group 1km to the west) by the author confirmed this unit and defined sub-units consisting of dark green diorite, pale coloured feldspathic rocks mapped as anorthosite and coarse grained hornblendite. These formations appear to have crosscutting relationships and are locally intercalated as alternating bands consistent with intrusive rocks. Fine grained Mg-tholeiitic flows are prominent in the north east quarter of the survey area. A chloritic unit of uncertain origin was mapped between the gabbro-diorite intrusive and the Mg-tholeiitic flows. This unit is characterized by quartz grains in a dark green chloritic matrix. The quartz grains, comprising 1-5% of the rock, range from barely visible to several mm diameter. Locally this quartz appears to be angular interstitial grains that survived chloritization of the gabbro-diorite. Locally, rocks within the chlorite unit have tuff-sediment textures. It is the opinion of the author the chloritic unit is altered rock of intrusive, volcanic and tuffaceous origin where alteration has destroyed most primary textures.

It is this chloritic unit and the extreme south edge of the Mg-tholeiite that appear to host the strong EM conductors located in this exploration area.

Approximately 40 scattered outcrops of moderate to intense Fe-carbonate alteration were located and hand stripped. 14 samples were analyzed for Au, 13 containing up to 237 ppb Au averaged 63 ppb Au. The fourteenth sample ran 19749 ppb Au.

The following local geology places this property within the Kirkland Lake gold area:

1. the Kirkland Lake Break within 0.8 km to the north.
2. known carbonate-fuchsite on strike 1.8 km to the west.
3 a major carbonate zone on strike 1.6 km to the east (Queenston's Vigras Lake property).
4. visible gold at the intersection of an east trending carbonate alteration and altered oxide iron formation 0.8 km to the south.

Also the Cyprus Zone of the Amalgamated Kirkland property is an equivalent distance south of the Kirkland Lake Main Break.

G. SUMMARY OF PREVIOUS WORK

No prospecting work other than work done by James Reed is recorded in MNDM assessment files. The only evidence of older work is a pit and trench exposing a major quartz vein at 3932E-123N. This ground was staked and explored by James Reed the current clam holder. Mr. Reed mapped, power stripped overburden, conducted magnetic and VLF surveys of his claims and drilled ten drill holes (Reference: Kirkland Lake Assessment file KL-2349). This work was conducted on north-south grid lines spaced at 400 foot centres and both magnetic and VLF readings were taken at 100 foot intervals. Listed below are the holes drilled by Mr . Reed:

1. 80-1 (307 feet) northeast testing a strong graphitic conductor on the east half of claim 475260.
2. 84-1 (114 feet) drilled on claim 1187002
3. 84-2 (117 feet) drilled on claim 1187002
4. 84-3 (119 feet) drilled on claim 475258
5. 84-1 (113 feet) drilled on claim 475258
6. 84-5 (116 feet) drilled on claim 1187002
7. 84-6a(22.5feet) drilled on claim 1187002
8. 84-6b (25 feet) drilled on claim 1187002
9. 84-6c(116 feet) drilled on claim 1187002
10. 84-7 (118 feet) drilled on claim 475258

The above holes tested two target areas. Hole 80-1 tested a graphitic conductor on the southeast quarter of claim 475260. The remaining holes tested quartz veining in a restricted area near the boundary of claims 1187002 and 475258. The majority of the property remains untested by diamond drilling.

H. SUMMARY 1994 WORK

1994 exploration, including line cutting, geological mapping, a MaxMin EM survey and a total field-magnetic gradient survey. Line cutting was performed by James Reed. Detailed mapping and hand stripping with emphasis on alteration and structural lineaments were conducted by the author. A total field-vertical gradient magnetic survey and an MaxMin EM survey were supervised by the author.

I. LINE CUTTING

17.308 km of metric grid with line spacing of 50 m and 25 m station interval was cut by James Reed with assistance from Jean Reed, Ruth Reed and Nat Reed. This work included 14.783 kilometres of cross lines, 1.085 kilometres of base line and 1.440 kilometres of tie lines. Line 40+00E was tied to the Otto-Eby Township boundary at three 1 inch square iron bars located at 40+00E-4+70N (Otto) and 40+00E-4+38S (Otto) and 40+00E-4+52S (Eby). This grid was tied to the contiguous property to the west held by Douglas Robinson where it was tied to the Eby Township survey at a 1 inch square iron bar located at 24+00E-4+37S. Only linecutting on ground held by James Reed is claimed in this report.

Of the 17.308 km of lines cut; only 13.150 km are claimed as assessment work in this report as 4.16 km of grid lines were not traversed by EM.

The following lines are claimed for assessment work in this report:

Total EM traverse	10.625 km
0+00N Base line	1.085 km
N.Tie Line	0.734 km
S.Tie Line	0.706 km
TOTAL	13.150 km

Total Expence Claim = $3985(13.15/17.308) = $3027

J. MaxMin HORIZONTAL LOOP EM SURVEY

A metric grid with a line spacing of 50 m and 25 m station interval was used for positional control during this survey. The MaxMin EM survey was directed to locating the surface trace and character of conductive formations within the grid area. Exploration was concentrated between 36+50 east and 43+50 east as this area had excellent outcrop exposure compared to the remainder of the group which has limited outcrop. Lines 32+65 and 34+00 were cut to confirm airborne anomalies (Otto Township Airborne Electromagnetic Survey, Mp P.2268). These extra lines were cut because two lines of the airborne survey over the main grid identified no anomalies.

The survey was initiated on lines 32+65E and 34+00E at the west end of the grid where airborne anomalies were known to exist. A 200 m coil separation was used on these lines to assure sufficient depth penetration to detect the conductors. A 200 m coil separation was also used to survey Lines 37+00E and 38+00E. The remainder of the grid was surveyed by 100 m coil separation. This shorter separation was also used to reduce the influence of high noise levels from the high tension power lines that crossed through the centre of the target area.

The initial survey was conducted on alternate lines spaced at 100 metre centres. Multiple conductors were located giving ambiguous results. These could be interpreted to strike north east parallel to the regional strike and parallel to the apparent trend of the airborne anomalies. Five intermediate lines were done on December 31, 1994 and January 1, 1995. These confirmed the conductors trend northwest approximately 60° to the apparent trend of the airborne conductors and the regional stratigraphic trend. A portion of line 40+00 east was surveyed using a 50 m cable in an attempt to better resolve the anomalies. No additional lines were tested using the 50 metre as penetration was reduced and the probability of short cable effects increase with shorter cables.

The summer survey was done using three frequencies on each line to establish the signature of the conductors. A greater frequency range was used for the 100 metre coil separation as the high frequencies are less sensitive to noise at shorter cable lengths. One frequency was used in the intermediate lines surveyed in the winter survey to resolve the ambiguous strike and to establish better continuity of anomalies.

A MaxMin 1 rented from Apex Parametrics Limited of Durham, Ontario was used for the summer survey. The winter survey was conducted with a MaxMin 11 rented from Jim Whalen of Kirkland Lake. Excellent resolution of anomalies was achieved from both instruments.

Terrain corrections were performed by recording a running average slope of four station intervals. The coils were maintained coplanar using the average slopes determined in the field during the traverses.

Data was plotted on standard profile plots recording IP and OP curves for each frequency and terrain profile on separate graphs on a common sheet. Data for each line was plotted on a separate sheet. This pressentation was used to accommodate multi-frequency data from variable coil seperations used to accomodate power line noise and differing penetrations depth sought. Also data plotted in this manner is easily reproduced using standard xerox machines.

The transmitter and receiver were reversed under the power lines to reduce noise levels.

LINE	COIL SEPARATION (m)	TRAVERSE LENGTH (m)	TOPOGRAPHY MEASURED (m)	FREQUENCY MEASURED
32+65	200	700	700	(440,880,3520 Hz)
34+00	200	850	850	(440,880,3520 Hz)
37+00	200	625	625	(440,880,3520 Hz)
38+00	200	700	700	(440,880,3520 Hz)
38+50	100	500	500	(3555 Hz)
39+00	100	675	675	(440,1760, 7040 Hz)
39+50	100	600	600	(3555 Hz)
40+00	100	625	625	(440,1760, 7040 Hz)
40+00	50	325	325	(440,1760, 7040 Hz)
40+50	100	550	550	(3555 Hz)
41+00	100	500	500	(440,1760, 7040 Hz)
41+50	100	900	900	(3555 Hz)
42+00	100	400	400	(440,1760, 7040 Hz)
42+50	100	875	875	(440,1760, 7040 Hz)
43+00	100	925	925	(3555 Hz)
43+50	100	875	875	(440,1760, 7040 Hz)
Total		10625	10625	

K. ANOMALIES

Ground EM consisting of MaxMin EM surveys were directed to locating the surface trace and character of conductive formations within the grid area. The following anomalies were identified:

Anomaly A	
A38.5	220N
A39	215N
A39.5	210N
A40	200N
A40.5	180N
A41	161N
A41.5	163N
A42	130N
A42.5	106N
A43	075N
A43.5	040N
Anomaly B	
B37	138N
B38	070N
B38.5	040N
Anomaly C	
C32.6	125N
C34	060N
Anomaly D	
D39	093N
D39.5	085N
D40	088N
D40.5	087N
Anomaly E	
E40	395N
Anomaly F	
F43.5	200N
Anomaly G	
G39	075S
Anomaly H	
41.5	127S
Anomaly I	
42.5	150S
Anomaly J	
J41.5	296S

Conductors A to J have been identified by this MaxMin survey. Of these conductors A, B, C, and D appear to be strong bedrock sources containing sulphides and/or graphite. Conductors E, F, G, H, I and J are weak to very weak and may trace wet shears, strong bedrock relief or alteration zones that could host Au mineralization.

None of the conductors are exposed in outcrop and the conductors generally follow swampy depressions. Commonly Fe-carbonate alteration and quartz filled gash fractures occur at the break of slopes bordering depressions indicating the presence of shearing and related gold style alteration zones centred in these depressions. Conductors A, B, C and D have both strong in phase (IP) and out of phase (OP) responses and narrow widths indicating narrow strongly conductive bedrock sources that would overwhelm any responses from alteration zones or conductive overburden, including swamps.

Conductor A appears to occur along or near the contact between Mg-tholeiite to the north and chloritic alteration-diorite to the south. The west end of the conductor is aligned with two VLF responses from a VLF survey conducted during the early 1980's. A abrupt change of geology west of line 38+50E indicates a north trending fault may truncate the conductor at this point. If a north trending fault exists it probably also shifts alteration zones that host Au mineralization. An intrusive contact could also explain the change of geology and the termination of conductor A west of line 38+50.

Conductors B and C are strong conductors assumed to strike at 115° and 122° respectively. This assumption is tenuous and must be verified by additional survey lines. If these conductors are offsets of conductor A, two north trending faults of 200 m offsets may exist. The geology and strike direction indicate they are independent of conductor A. In either case additional survey lines would resolve much of the existing ambiguity. If these conductors are natural short conductors independent of conductor A, they have enhanced probability of being Au-sulphide, Ni-Cu-Pt or base matal deposits.

Mapping by the author indicates conductor D is located near the projection of strong shearing having an 080° azimuth and directly south of prominent Fe-carbonate alteration. This association combined with is discordant strike relative to the other conductors indicate this is a prime gold target; possibly the Larder Lake Break. If this discordant strike is real, any EM response from this conductor to the west would be masked by conductor B and similarly conductor A would mask it's response to the east.

Conductor E is an OP response less than 25 metres wide beneath 100 metres of swamp. This response appears to be caused by either a channel within the swamp or shearing and/or alteration. A long linear swamp of azimuth 120° projects directly to conductor F. The EM profiles between conductors E and F indicate a vague OP response that is to weak to classify as a conductor, however this swamp may mark a significant horizon that could host alteration and/or shearing.

Conductor F appears to be a strong bedrock response related to sulphides and/or graphite, The profiles indicate Conductor F could either be a conductor 160 metre north of Conductor A or much of the 160 metres between 040N and 200N is a broad conductive zone. The OP profiles of lines 42+50E and 43+00E between conductor A and 200N is conductive. This appears to be an area of shallow swamp over deep overburden. It is inconclusive if this conductive zone north of conductor A is a real bedrock response, however, it should be considered seriously considering the strength of conductor F on the north east edge of this response.

Conductor G is not strong, however it has sufficient IP response to indicate a bedrock source. It is also coincident with a prominent alteration Fe-carbonate alteration zone and should be considered seriously.

Conductors H, I and J are weak conductors associated with till covered ground. H and J are weak OP responses only, indicating sheared ground or alteration. Conductor I is a weak IP response, possibly detecting either a deep or very narrow sulphide or graphitic source rock. Conductor J is closely

associated with bedrock occurrences of Fe-carbonate alteration and prominent float having intense alteration. It has a high probability of being associated with the bedrock source of the prominent alteration in nearby float. Conductors H and I are on strike with conductor B and may reflect a shear extension of this conductor. It is reasonable to expect shears extending beyond the ends of certain bedrock conductors.

L. RECOMMENDATIONS

An additional 15 lines should be cut to complete coverage of the property. A MaxMin EM survey having a 100 m coil separation should be extended to all of the grid including those lines not covered in this survey. The high density of anomalies and ambiguity resulting from a 100 m line spacing justify the recommended 50 m line density. The 100 m coil separation has been found to be the best compromise between topographic influences, penetration depth and resolution. Other coil separations can be used to resolve specific problems.

Other recommended activities include extension of detailed mapping, hand stripping and magnetic surveys to cover the extended grid. Mapping should include sampling of all alteration zones and areas of mineralization to determine the distribution of gold. Follow up power stripping by excavator should be utilized to extend alteration zones along strike and expose the full width of alteration zones which are commonly centred in depressions with alteration exposed only at the base of slopes on either side. OP EM conductors lacking IP responses should also be power stripped to determine their source.

Diamond drilling should be employed to test the best geological and geochemical targets with emphasis on those zones having best Au values. The intersection of alteration and mineralized zones with EM conductors are also a preferred drill target.

M. LIST OF CO-HOLDERS

North East Group

James D. Reed
RR #3, Site 3, Box 2
Swastika, Ontario
P0K 1T0

Emmalene L. Reed
RR #3, Site 3, Box 2
Swastika, Ontario
P0K 1T0

Nathanael E. Reed
Box 85
Swastika, Ontario
P0K 1T0

Charles E. Reed
8 Kingsley Court
Guelph, Ontario
N1E 1E3

M. LIST OF CO-HOLDERS

J. D. Reed
RR #3, Site 3, Box 2
Swastika, Ontario
P0K 1T0

E. L. Reed
RR #3, Site 3, Box 2
Swastika, Ontario
P0K 1T0

N. E. Reed
Box 85
Swastika, Ontario
P0K 1T0

C. E. Reed
8 Kingsley Court
Guelph, Ontario
N1E 1E3

N. LIST OF REFERENCES

EBY TOWNSHIP

MEMOIR 131 - Canada Department of Mines
Kenogami, Round, and Larder Lake Areas, Timiskaming District, Ontario, By H. C. Cooke, 1922.

Geological Report 99 - Ontario Department of Mines Preliminary Geology of the Eby and Otto Area, District of Temiskaming
By H. L. Lovell, 1972.

Map P. 448 - Ontario Department of Mines Preliminary Geological Map No. P. 448; Eby Township.
Scale 1 inch = 1/2 mile

Map P. 903 - Preliminary Map P.903; Kirkland Lake Data Series; Eby Township.
Scale 1 : 15 840

Map P. 2268 - Ontario Geological Survey Preliminary Map P.2268 Kirkland Lake Area; Eby Township; Airborne Electromagnetic Survey.

Map P. 2268 - Ontario Geological Survey Preliminary Map P.2268; Kirkland Lake Area; Eby Township; Airborne Electromagnetic Survey; Total Field Magnetic Survey.
Scale 1 : 20 000

OTTO TOWNSHIP

Map P. 330 - Ontario Department of Mines Preliminary Geological Map No. P. 330; Otto Township (North Half)
Scale 1 inch = 1000 feet

Map No. 501 - Preliminary Map No. 501; Otto Township and Northern Part of Marquis Township.
Scale 1 inch = 1/4 mile.

Map P. 717 - Ontario Department of Mines and Northern Affairs; Preliminary Map P. 717; Geochemical Distribution of Acid Soluble Copper in Felsic Plutonic Rocks; Otto Township and Parts of Eby, Marquis and Boston Townships.
Scale 1 inch = 1/2 mile

Map P. 718 - Ontario Department of Mines and Northern Affairs; Preliminary Map P. 718; Geochemical Distribution of Acid Soluble Lead in Felsic Plutonic Rocks. Otto Township and Parts of Eby, Marquis and Boston Townships.
Scale 1 inch = 1/2 mile

Map P. 719 - Ontario Department of Mines and Northern Affairs; Preliminary Map P. 719; Geochemical Distribution of Acid Soluble Molybdenum in Felsic Plutonic Rocks. Otto Township and Parts of Eby, Marquis and Boston Townships.
Scale 1 inch = 1/2 mile

Map P. 2269 - Ontario Geological Survey Preliminary Map P.2269; Kirkland Lake Area; Otto Township; Airborne Electromagnetic Survey.

Map P. 2269 - Ontario Geological Survey Preliminary Map P.2269; Kirkland Lake Area; Otto Township; Airborne Electromagnetic Survey; Total Field Magnetic Survey.
Scale 1 : 20 000

CERTIFICATE

I, Douglas Robinson, of 24 Victoria Avenue Swastika, Ontario, hereby certify that:

1. I am a registered professional Engineer of Ontario engaged in my profession for approximately 19 years.

2. I am a graduate of Queen's University in Kingston Ontario with an Honours Bachelor of Science degree in Geological Engineering and
Northern College, School of Mines in Haileybury, Ontario with a Mining Technician Certificate.

3. I personally supervised the EM surveys claimed in this assessment report.

4. I authored this report.

5. My knowledge exploration procedures was acquired through 20 years employment in the mining industry.

6. My knowledge of the properties was acquired by personally mapping the property and reviewing MNDM assessment reports.

Douglas Robinson

Douglas Robinson, P. Eng
January 8, 1995.



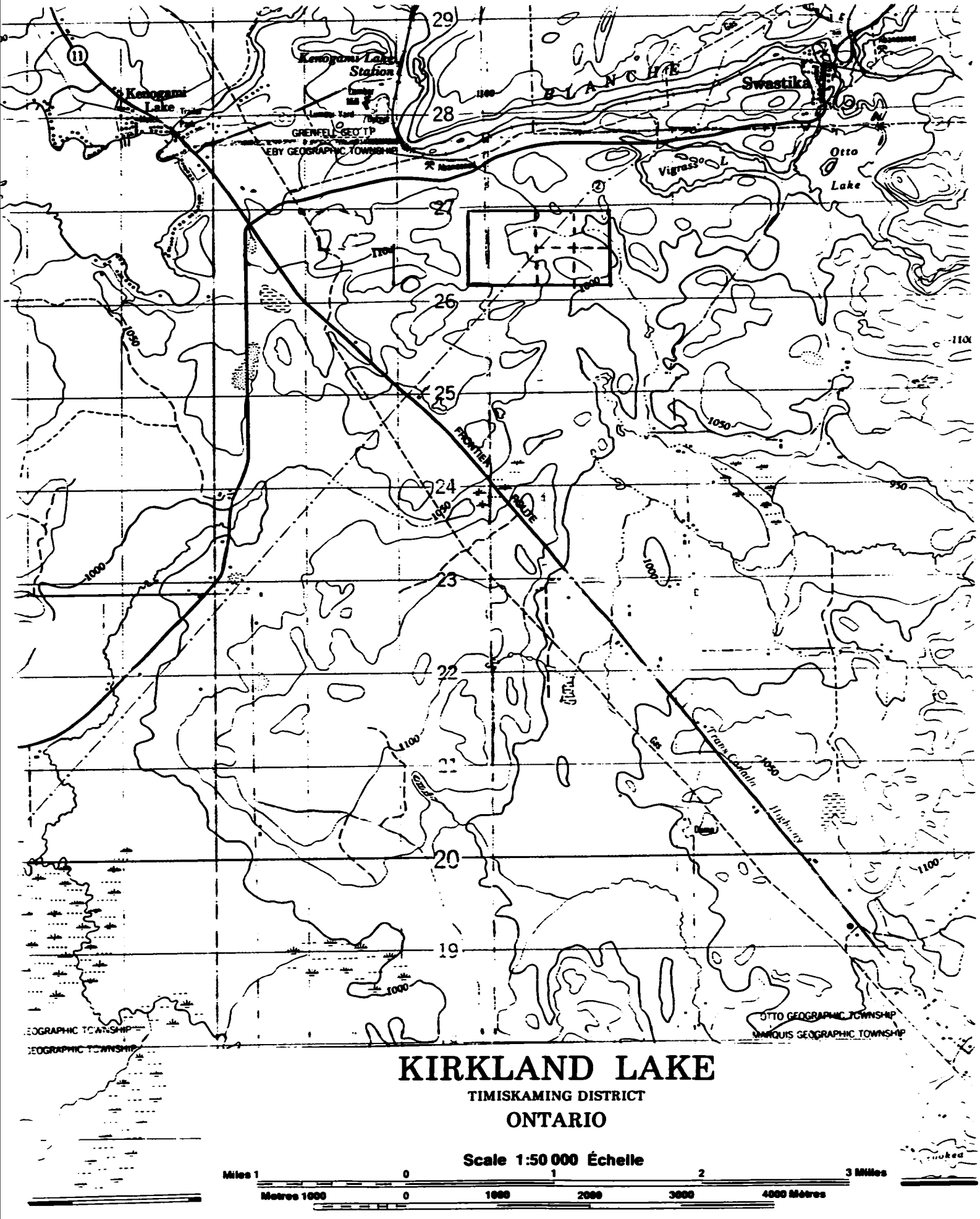


Figure 1. General Location of Claim Groups

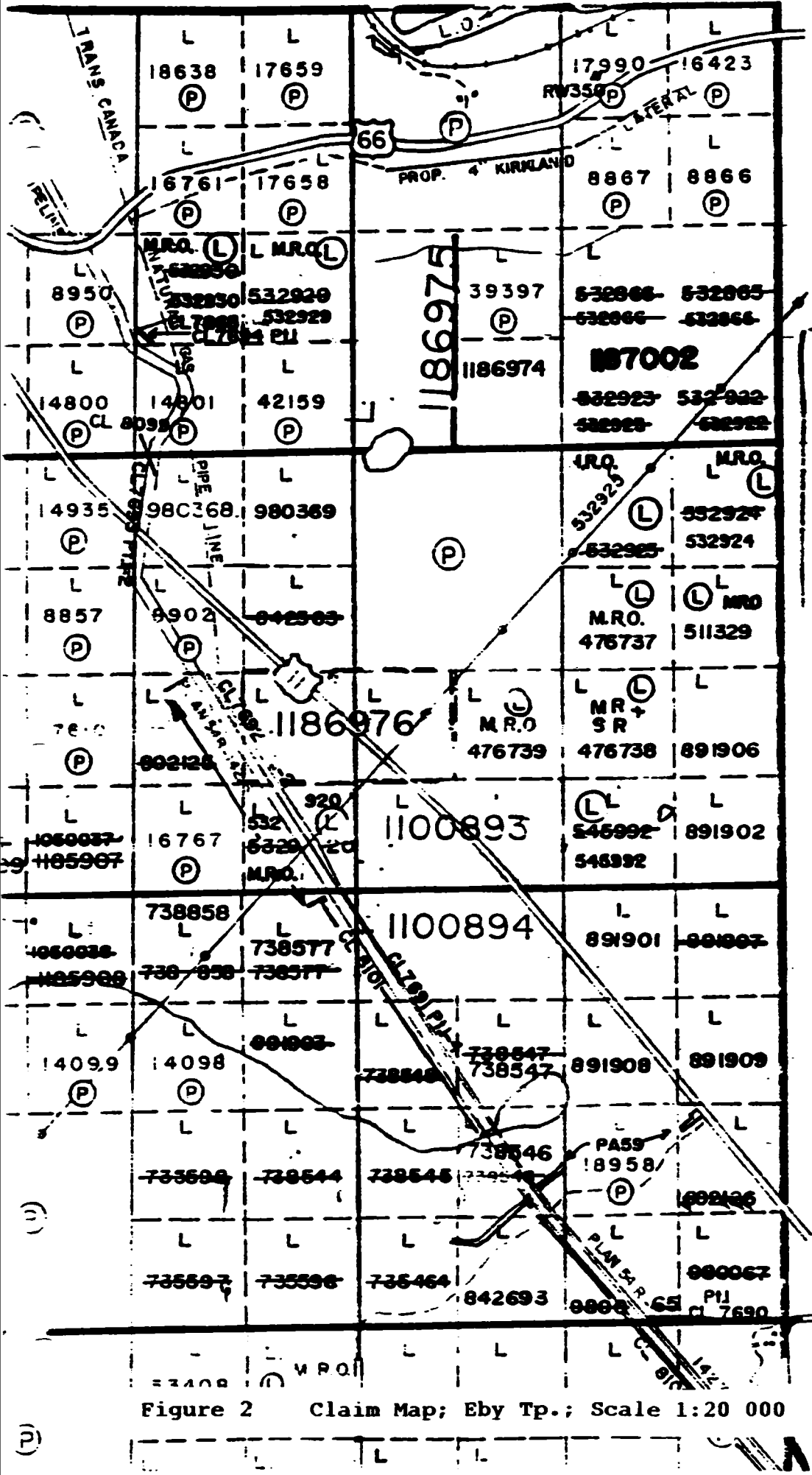


Figure 2 Claim Map; Eby Tp.; Scale 1:20 000

VI

V

IV

DATE OF IS

MAR 15

LARDER LAKE
MINING RECORDER'S

M.379

Eby Twp.

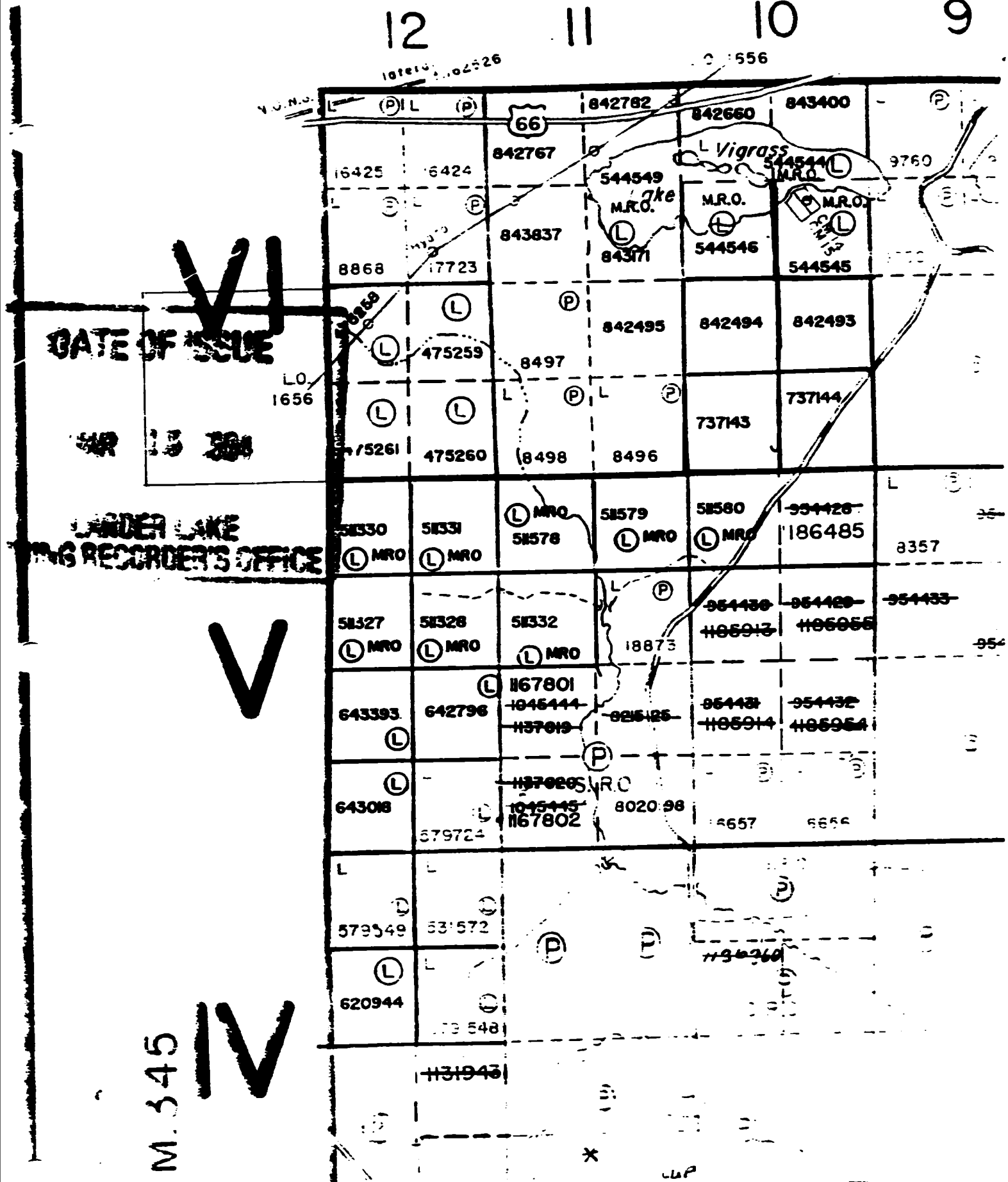


Figure 3. Claim Map; Otto Tp.; Scale 1:20 000

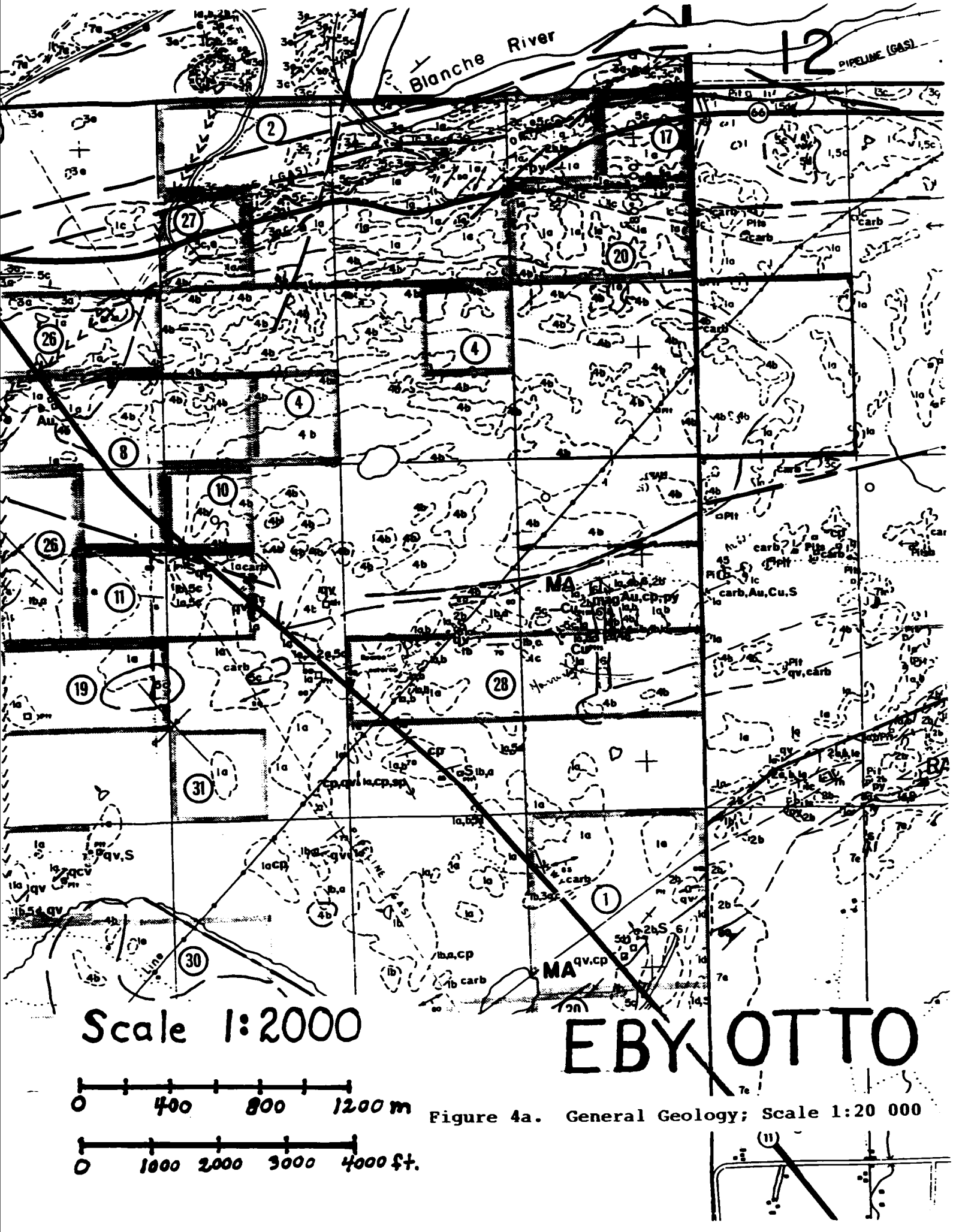


Figure 4a. General Geology; Scale 1:20 000

Map P. 448 - Ontario Department of Mines Preliminary Geological Map No. P. 448; Eby Township.
Scale 1 inch = 1/2 mile

LEGEND

PRECAMBRIAN

PROTEROZOIC

8 MAFIC INTRUSIVE ROCKS

HURONIAN

COBALT GROUP

7 GOWGANDA FORMATION

ARCHEAN

MAFIC INTRUSIVE ROCKS

6 Diabase

FELSIC INTRUSIVE ROCKS (ALGOMAN)

5c Syenite and Syenite Porphyry

5d Mafic syenite, lamprophyre, and hybrid syenite and country rocks

MAFIC AND ULTRAMAFIC INTRUSIVE ROCKS (HAILEYBURIAN, EARLY ALGOMAN, AND SOME KEEWATIN)

4b Gabbro and Diorite

METASEDIMENTS (TIMISKAMING OR KEEWATIN)

3

FELSIC VOLCANIC ROCKS (KEEWATIN)

2a Rhyolite and dacite

MAFIC VOLCANIC ROCKS (KEEWATIN)

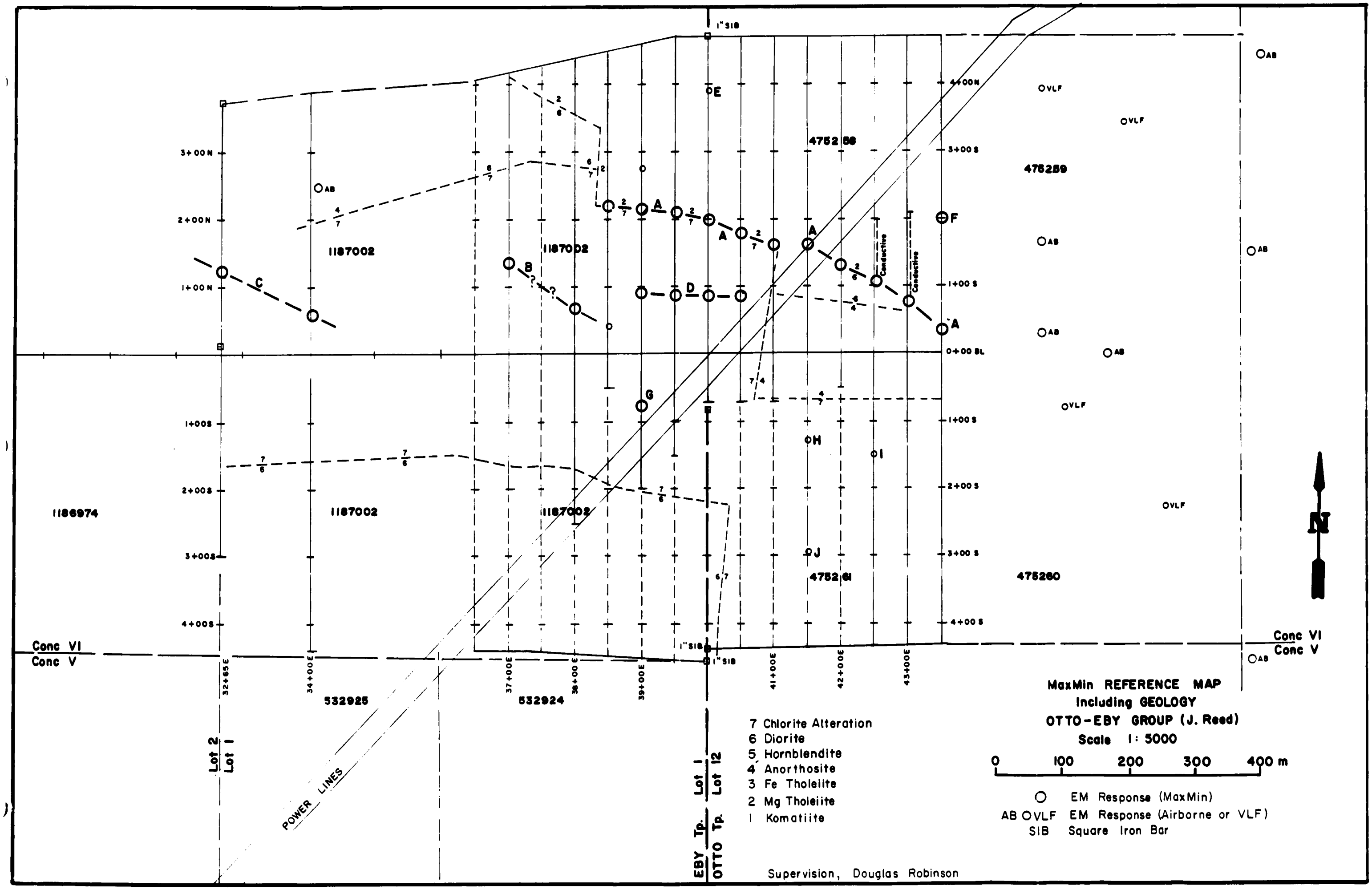
1a Basalt and andesite (pillowed and massive)

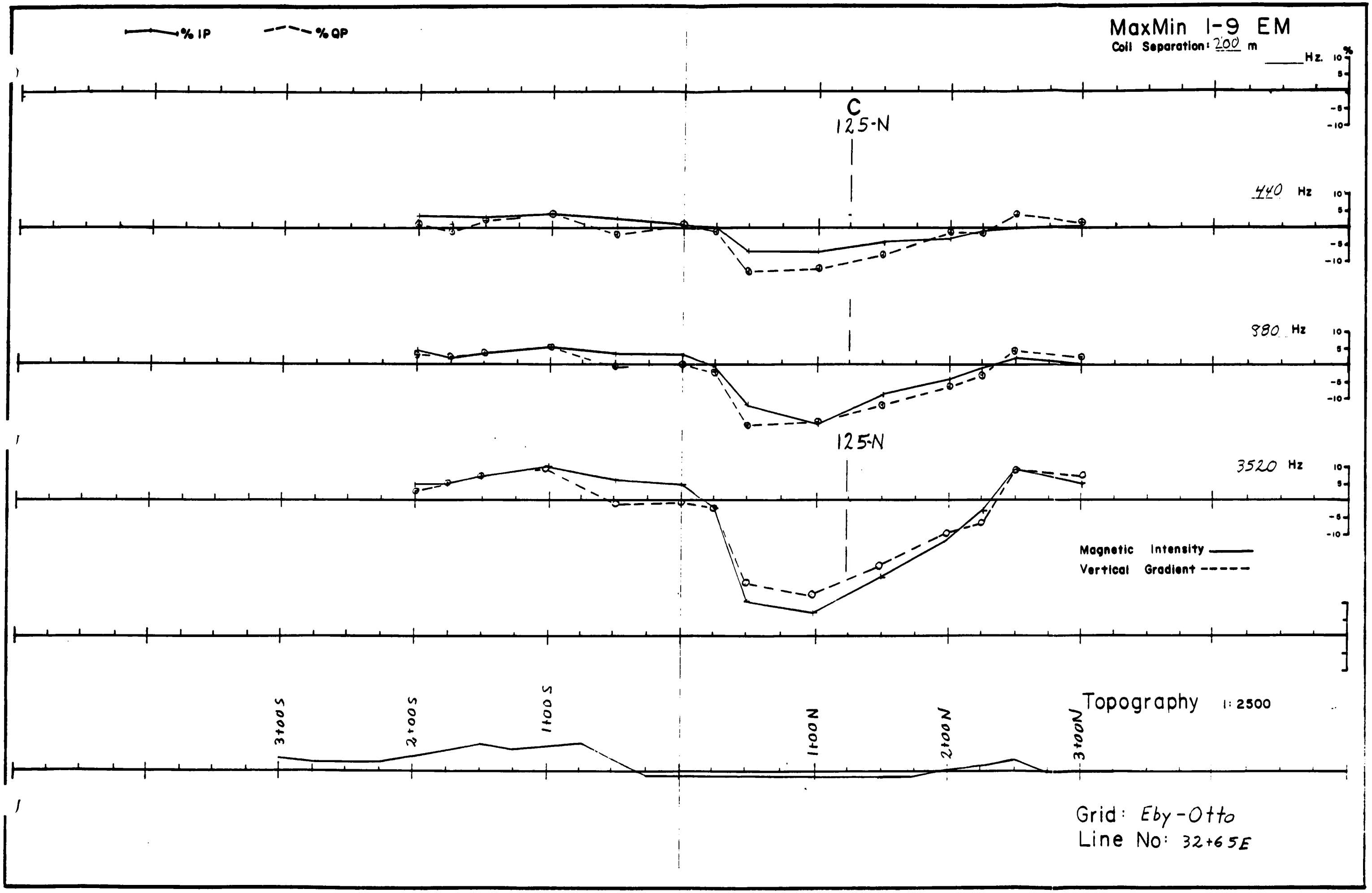
1b Mafic agglomerate and tuff

Figure 4b. General Geology; Legend



Figure 5. Airborne Survey (Map P.2268): Scale 1:20 000


1"SIB
E
F
A
B
C
D
G
H
I
J
4752 58
475259
475260
4752 61
1187002
1186974
532925
532924
Conductive
Conductive
AB
VLF
4+00N
3+00N
2+00N
1+00N
0+00 BL
1+00S
2+00S
3+00S
4+00S
32+65E
34+00E
37+00E
38+00E
39+00E
41+00E
42+00E
43+00E
Conc VI
Conc V
Lot 2
Lot 1
Lot 1
Lot 12
EBY Tp.
OTTO Tp.
POWER LINES
N
7 Chlorite Alteration
6 Diorite
5 Hornblendite
4 Anorthosite
3 Fe Tholeiite
2 Mg Tholeiite
1 Komatiite
MaxMin REFERENCE MAP
Including GEOLOGY
OTTO-EBY GROUP (J. Reed)
Scale 1:5000
0 100 200 300 400 m
EM Response (MaxMin)
AB VLF EM Response (Airborne or VLF)
SIB Square Iron Bar
Supervision, Douglas Robinson


% IP
% QP
MaxMin I-9 EM
Coil Separation: 200 m
Hz.
%
10
5
-5
-10
C
125-N
440 Hz
880 Hz
3520 Hz
Magnetic Intensity
Vertical Gradient
3+00S
2+00S
1+00S
1+00N
2+00N
3+00N
Topography 1:2500
Grid: Eby-Otto
Line No: 32+65E

% IP % QP

MaxMin I-9 EM

Coil Separation: 200 m

Hz. 10 5 -5 -10 %

C

060N

400 Hz 10 5 -5 -10

880 Hz 10 5 -5 -10

3520 Hz 10 5 -5 -10

Magnetic Intensity ——

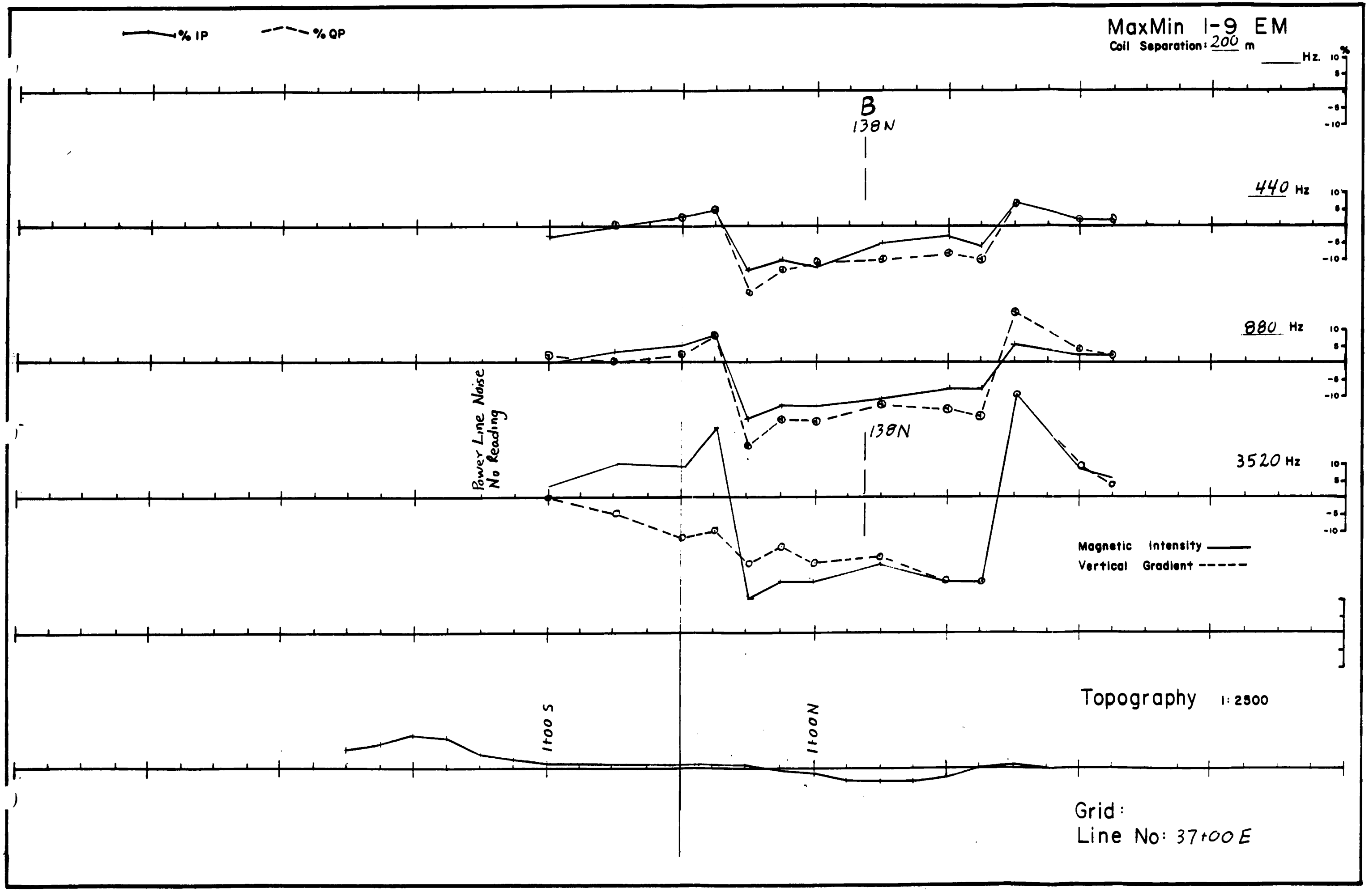
Vertical Gradient - - - -

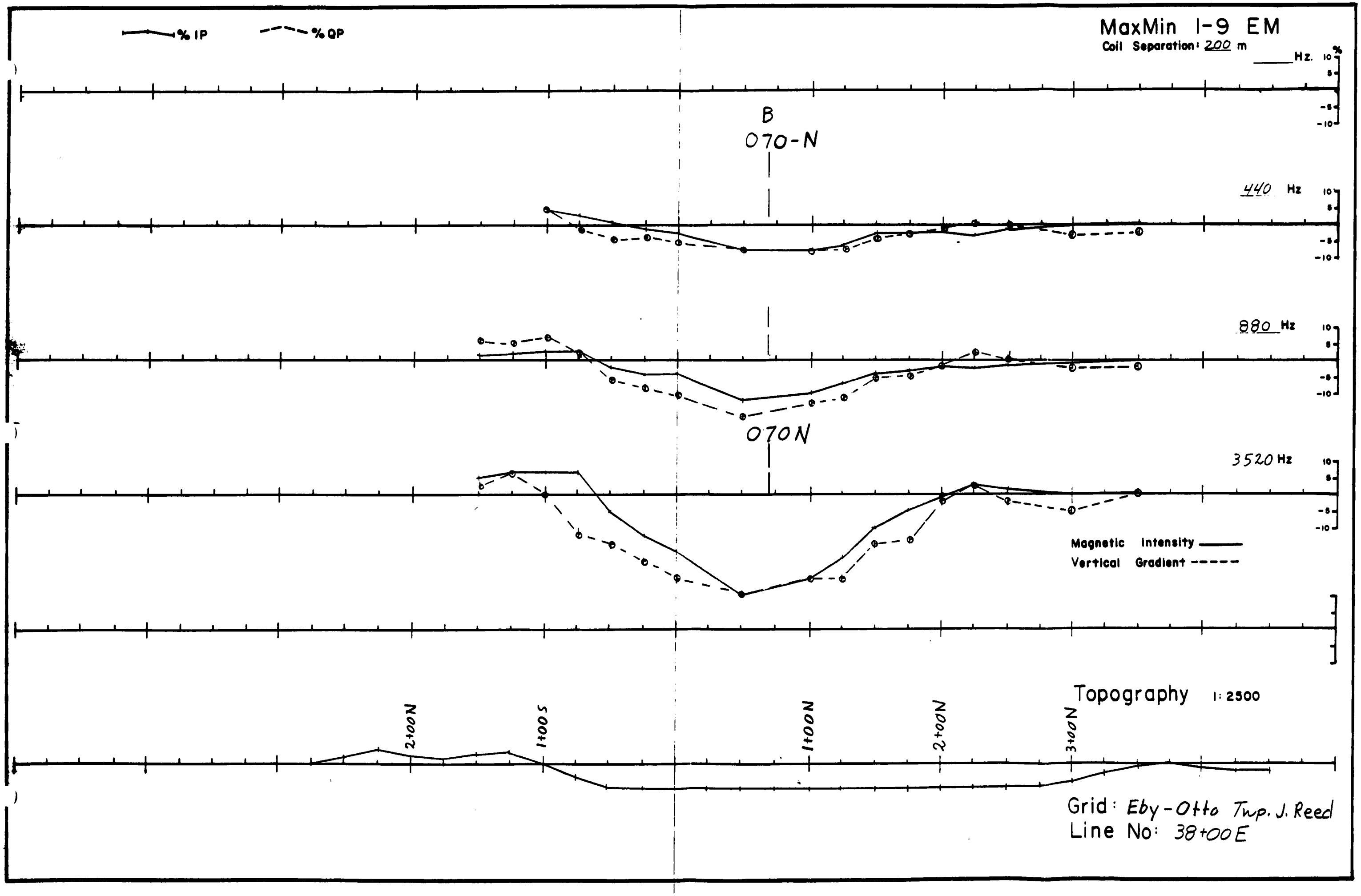
4+00S 3+00S 2+00S 1+00S 1+00N 2+00N 3+00N

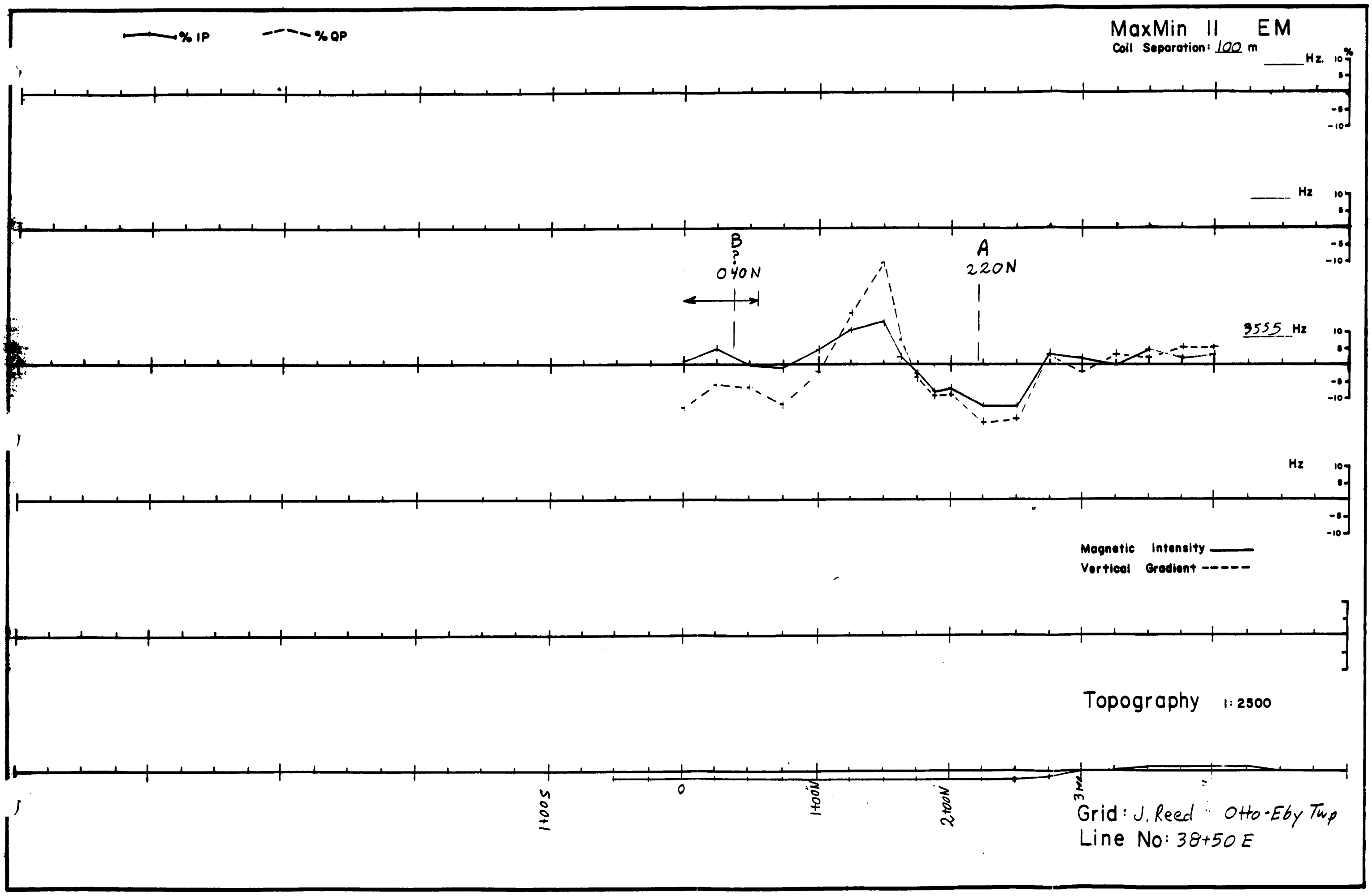
Topography 1:2500

Grid: Otto-Eby

Line No: 34+00E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 200 m
Hz.
B
138N
440 Hz
880 Hz
Power Line Noise
No Reading
138N
3520 Hz
Magnetic Intensity
Vertical Gradient
Topography 1:2500
1100 S
1100N
Grid:
Line No: 37+00E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 200 m
Hz.
%
10
5
-5
-10
B
070-N
440 Hz
880 Hz
070N
3520 Hz
Magnetic Intensity
Vertical Gradient
Topography 1:2500
2+00N
1+00S
1+00N
2+00N
3+00N
Grid: Eby-Otto Twp. J. Reed
Line No: 38+00E


% IP
% QP
MaxMin II EM
Coil Separation: 100 m
Hz.
Hz
9555 Hz
B
?
040N
A
220N
Hz
Magnetic Intensity
Vertical Gradient
Topography 1:2500
1400S
0
1400N
2400N
3mE
Grid: J. Reed Otto-Eby Twp
Line No: 38+50 E

% IP % QP

MaxMin I-9 EM

Coil Separation: 100 m

Hz. 10 5 -5 -10 %

No Readings Power Line noise

440 Hz 10 5 -5 -10

G 075-S

D 093N

A 215N

1760 Hz 10 5 -5 -10

093N

275N

7040 Hz 10 5 -5 -10

Magnetic Intensity ——

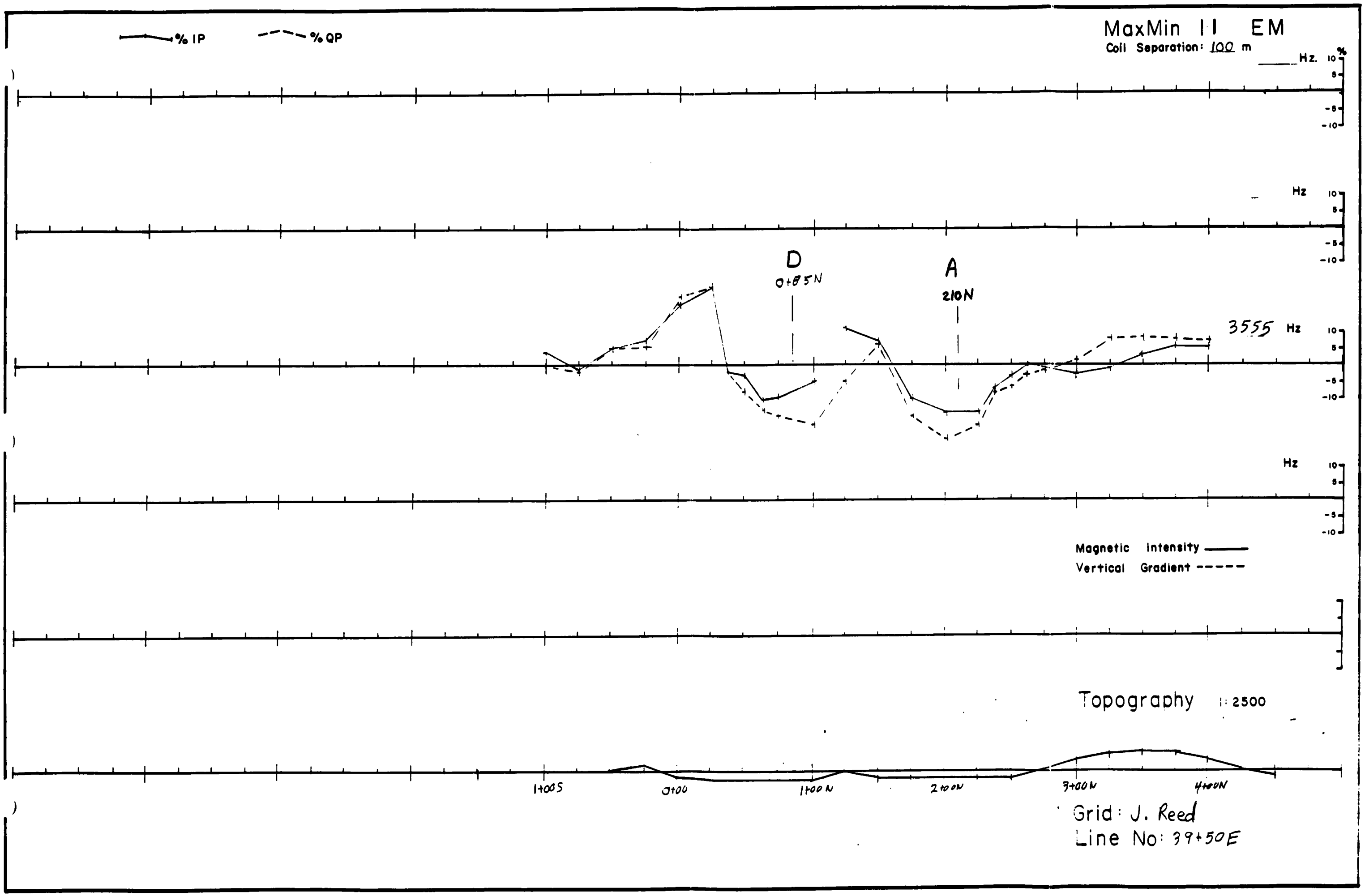
Vertical Gradient - - - -

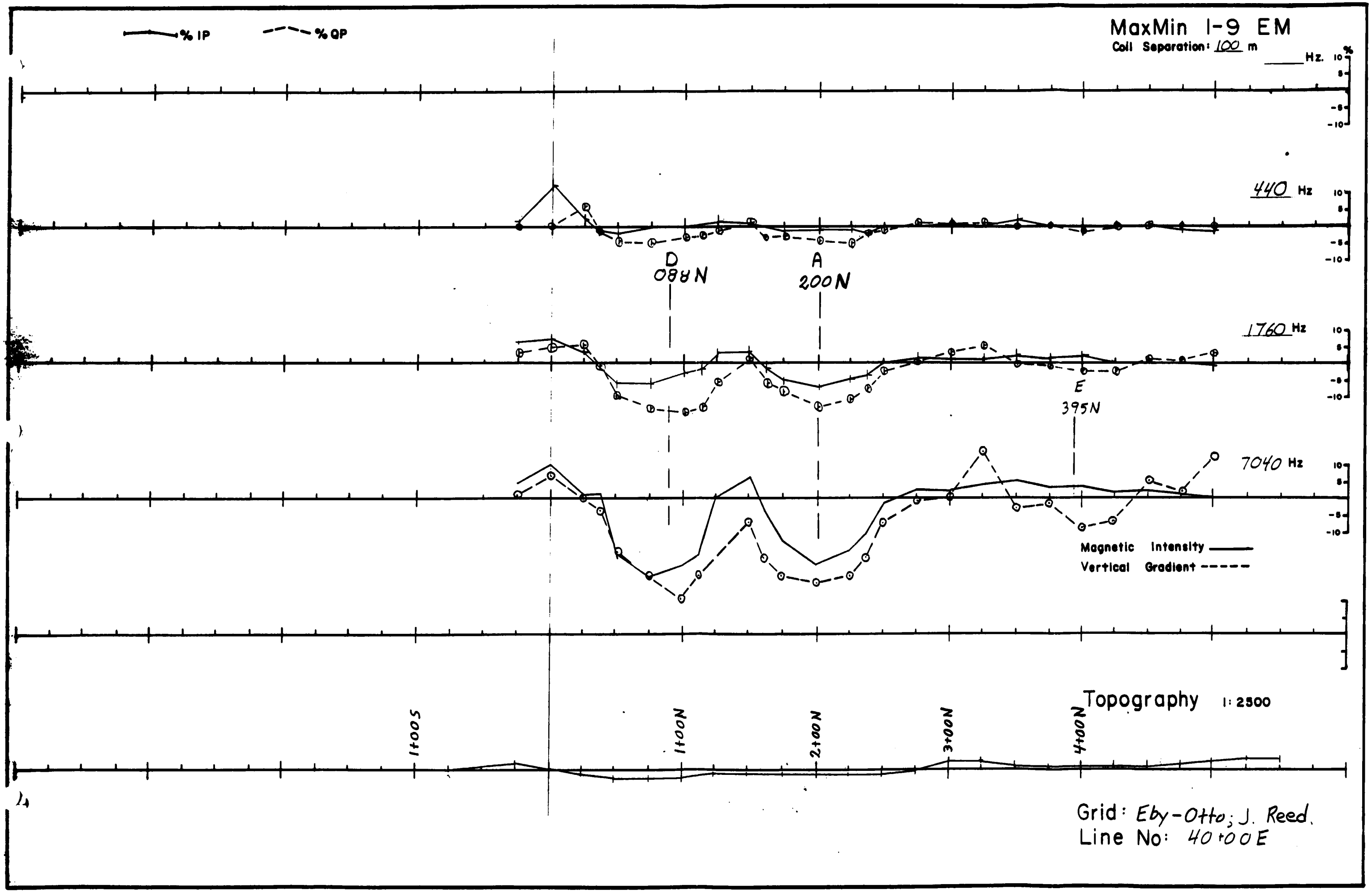
Topography 1:2500

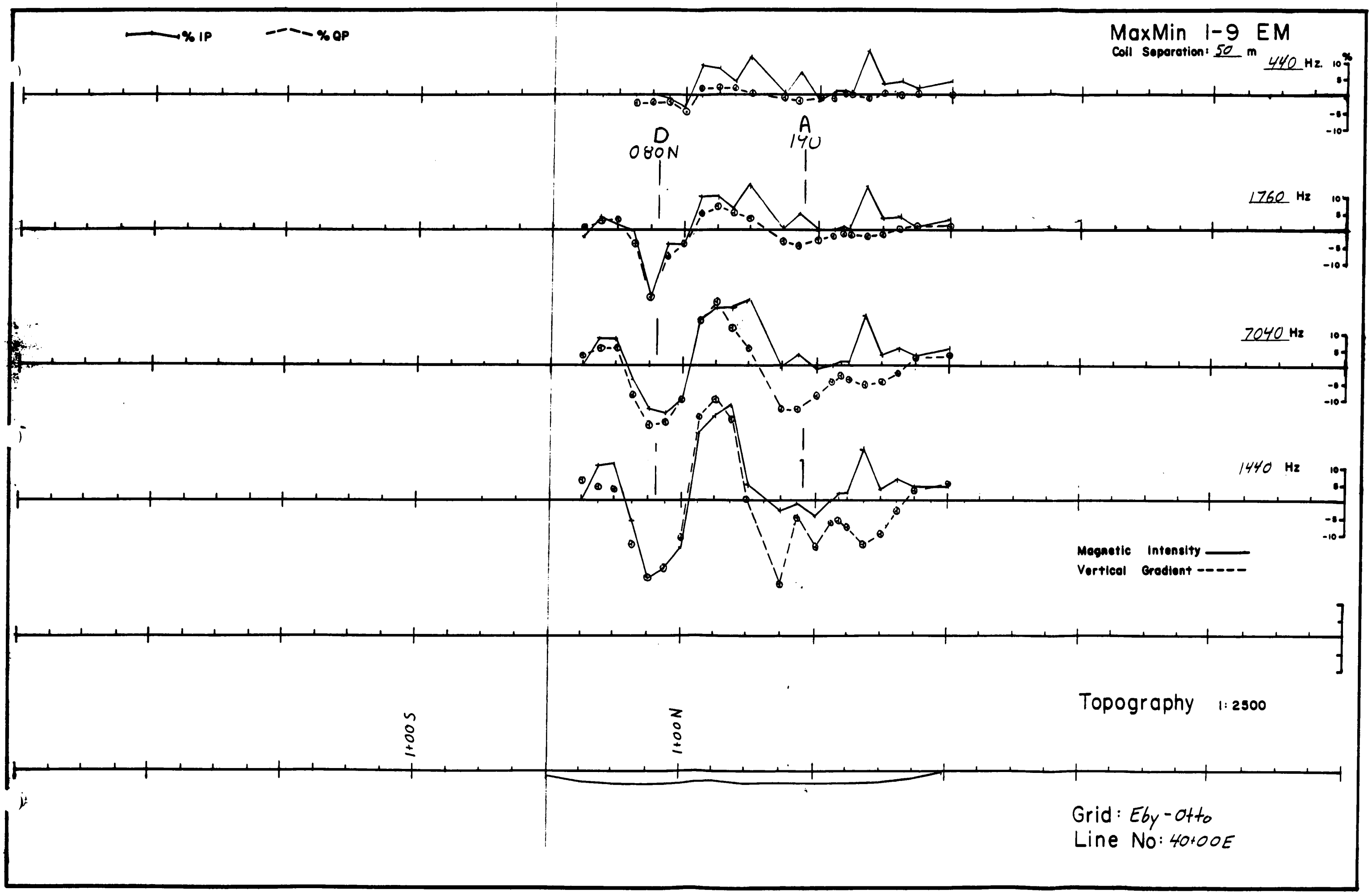
2+00-S 1+00-S 0+00N 1+00N 2+00N 3+00N

Grid: Eby-Otto

Line No: 39+00E


% IP
% QP
MaxMin II EM
Coil Separation: 100 m
Hz.
%
10
5
-5
-10
Hz
D
0+85N
A
210N
3555 Hz
Hz
Magnetic Intensity
Vertical Gradient
Topography 1:2500
1+00S
0+00
1+00N
2+00N
3+00N
4+00N
Grid: J. Reed
Line No: 39+50E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 100 m
Hz.
440 Hz
1760 Hz
7040 Hz
D
088N
A
200N
E
395N
Magnetic Intensity
Vertical Gradient
Topography 1:2500
1+00S
1+00N
2+00N
3+00N
4+00N
Grid: Eby-Otto; J. Reed.
Line No: 40+00E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 50 m
440 Hz.
1760 Hz
7040 Hz
1440 Hz
10
5
-5
-10
%
D
080N
A
140
Magnetic Intensity
Vertical Gradient
1+00S
1+00N
Topography 1:2500
Grid: Eby-Otto
Line No: 40+00E

% IP % QP

MaxMin I EM

Coil Separation: 100 m

Hz. 10 5 -5 -10 %

Hz 10 5 -5 -10

D 0+87N

A 1+80N

Hz 10 5 -5 -10

Hz 10 5 -5 -10

Magnetic Intensity ——

Vertical Gradient - - - -

Topography 1:2500

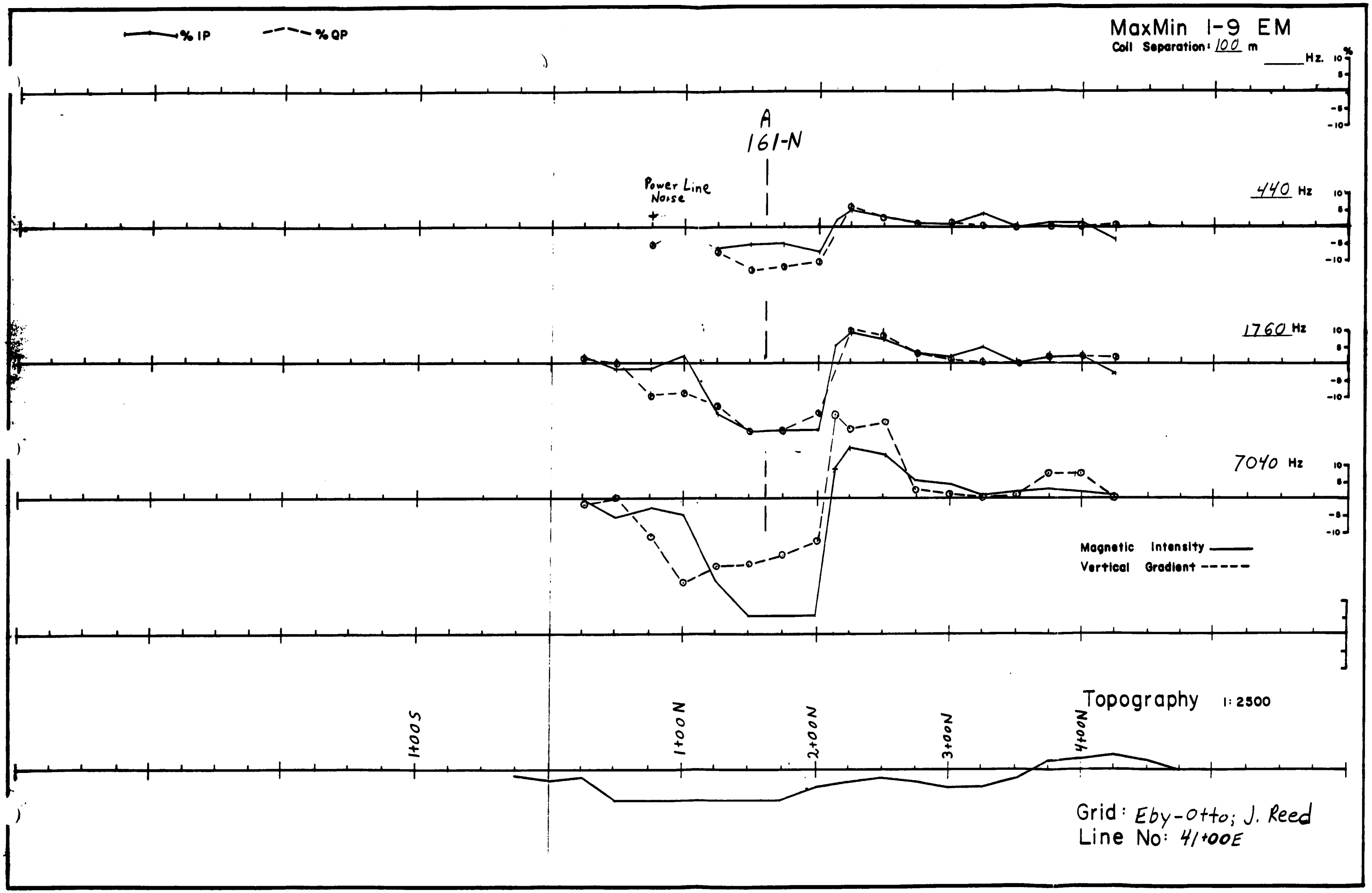
0+00

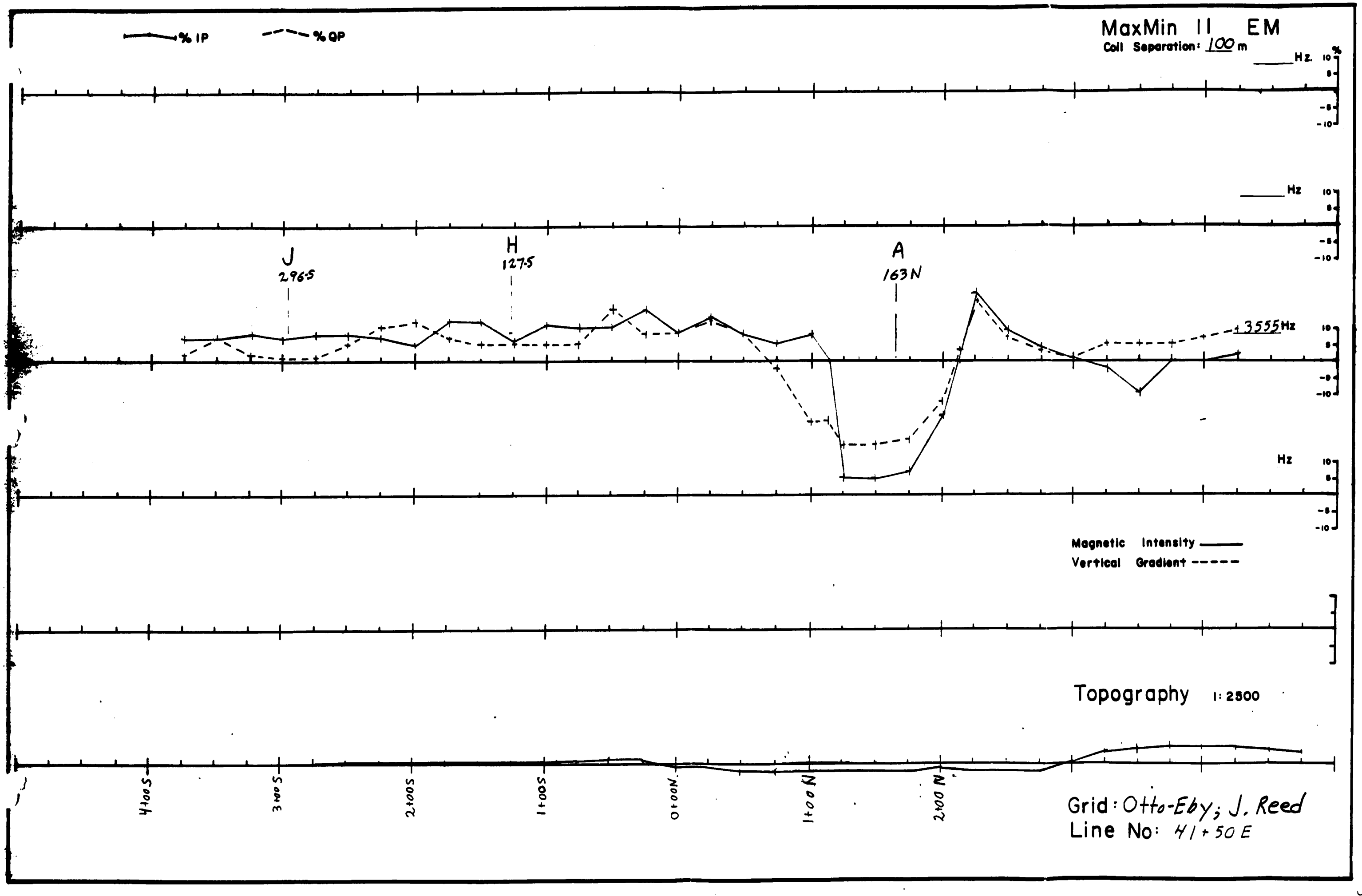
1+00N

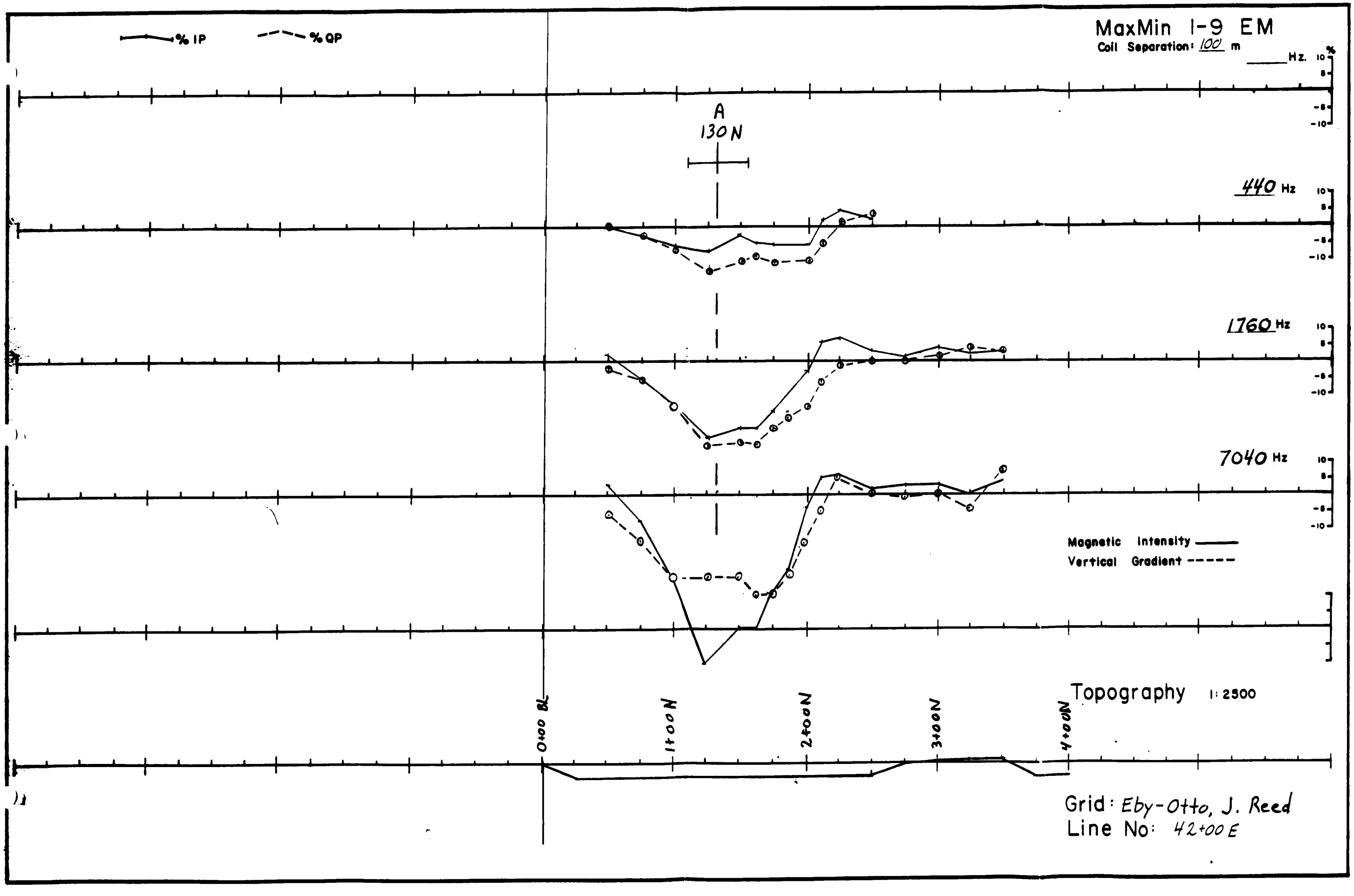
2+00N

Grid: J. Reed, Otto-Eby Twp.

Line No: 40+50N


% IP
% QP
MaxMin I-9 EM
Coil Separation: 100 m
Hz.
A
161-N
Power Line Noise
440 Hz
1760 Hz
7040 Hz
10
5
-5
-10
Magnetic Intensity
Vertical Gradient
Topography 1:2500
1+00S
1+00N
2+00N
3+00N
4+00N
Grid: Eby-Otto; J. Reed
Line No: 41+00E


% IP
% QP
MaxMin II EM
Coil Separation: 100 m
Hz.
Hz
J
296·5
H
127·5
A
163N
3555Hz
Hz
Magnetic Intensity
Vertical Gradient
Topography 1:2500
4100S
3100S
2100S
1100S
0100N
1100N
2100N
Grid: Otto-Eby; J. Reed
Line No: 41+50E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 100 m
Hz.
A
130 N
440 Hz
1760 Hz
7040 Hz
10
8
-8
-10
Magnetic Intensity
Vertical Gradient
Topography 1:2500
0+00 BL
1+00 N
2+00N
3+00N
4+00N
Grid: Eby-Otto, J. Reed
Line No: 42+00 E

% IP % QP

MaxMin I-9 EM

Coil Separation: 100 m

Hz. 10 5 -5 -10 %

A
106 N

440 Hz 10 5 -5 -10

106-N

1760 Hz 10 5 -5 -10

I
150-S

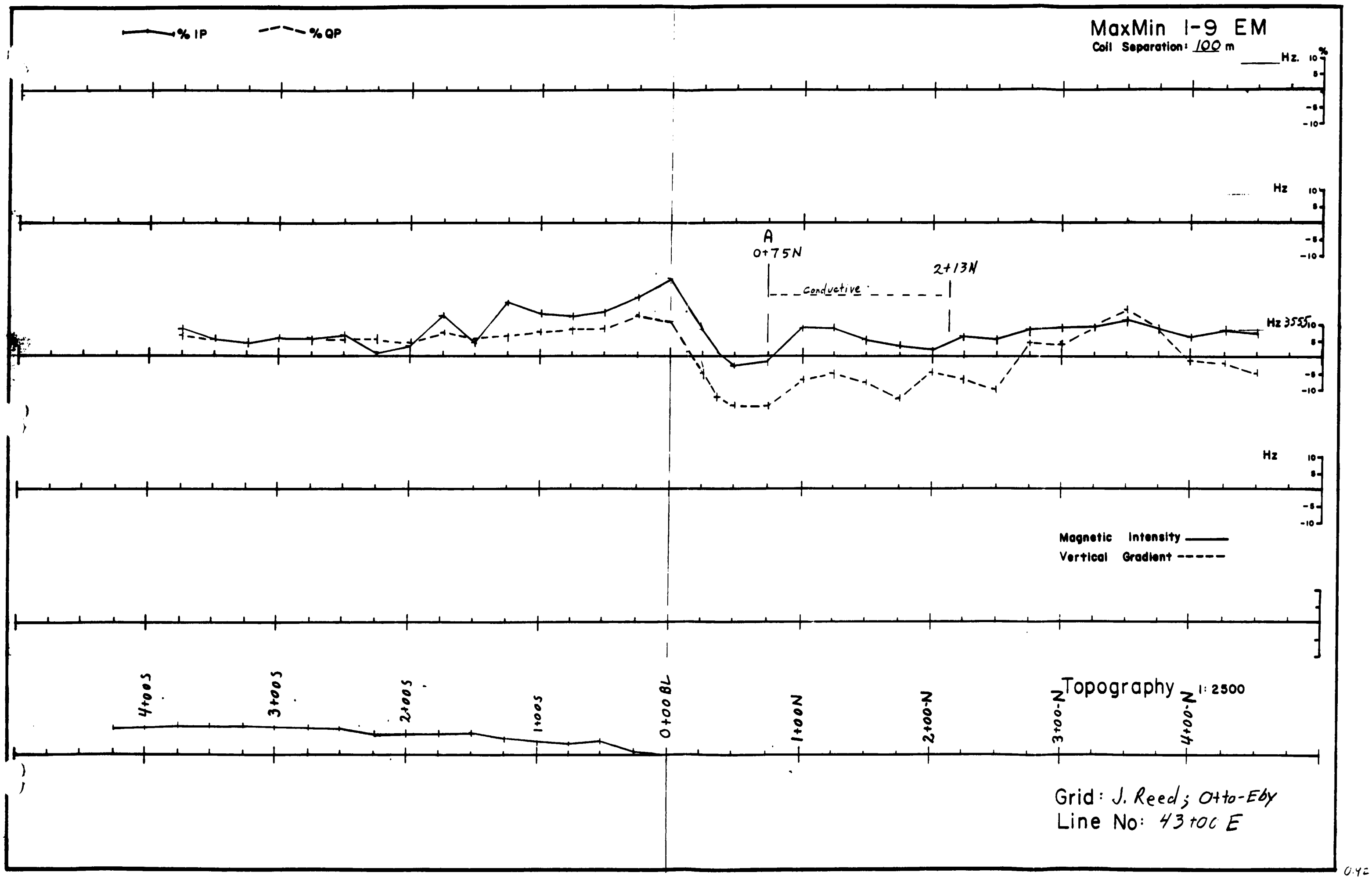
7040 Hz 10 5 -5 -10

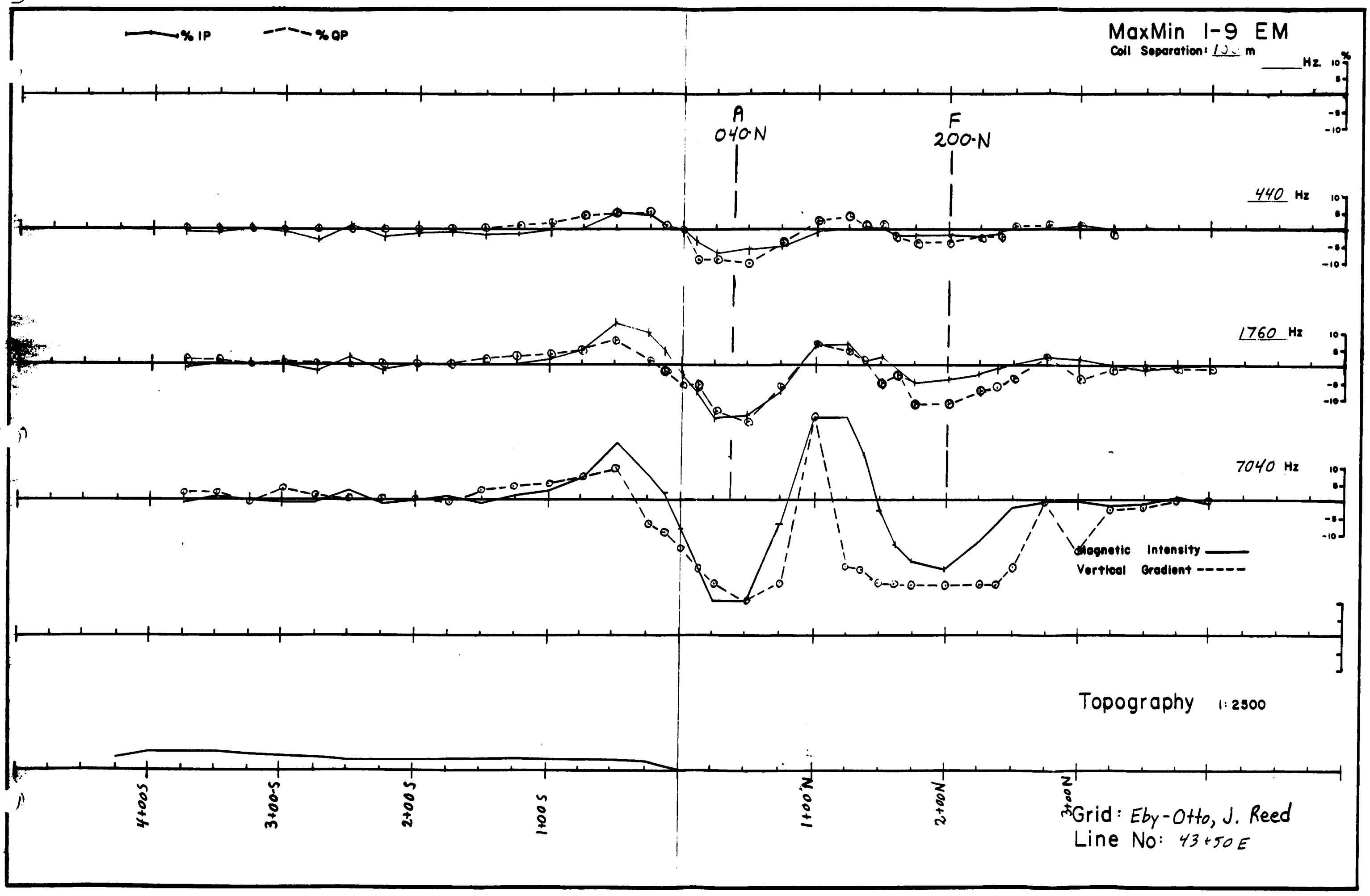
Magnetic Intensity ——
Vertical Gradient - - - -

Topography 1:2500

4+00S 3+00S 2+00S 1+00S 0+00 BL 1+00N 2+00N 3+00N

Grid: Eby-Otto
Line No: 42+50°E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 100 m
Hz.
Hz
Hz 3555
A
0+75N
2+13N
Conductive
Hz
Magnetic Intensity
Vertical Gradient
4+00S
3+00S
2+00S
1+00S
0+00 BL
1+00N
2+00N
3+00N
4+00N
Topography 1: 2500
Grid: J. Reed; Otto-E6y
Line No: 43+00 E


% IP
% QP
MaxMin I-9 EM
Coil Separation: 150 m
Hz
A
040-N
F
200-N
440 Hz
1760 Hz
7040 Hz
Magnetic Intensity
Vertical Gradient
Topography 1:2500
4+00S
3+00S
2+00S
1+00S
1+00N
2+00N
3+00N
Grid: Eby-Otto, J. Reed
Line No: 43+50E

Grid:Eby N Coil Spacing: 200 m.
Line #:32+65 E Receiver S of Transmitter

Slope To Stn		Stn		3520 Hz IP (QP)	880 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
°	%	2+75	N	__._(_._)	__._(_._)	__._(_._)	+ _%
+20°	+35%	2+50	N	__._(_._)	__._(_._)	__._(_._)	+ _%
-10°	+18%	_+25	N	__._(_._)	__._(_._)	__._(_._)	+ _%
-50°	- 9%	2+00	N	5 (7)	0 (2.2)	0.5(1.5)	+ _%
-10°	-19%	_+75	N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+50	N	10 (9)	2 (4)	0 (4)	+ _%
+ 0°	+ 0%	_+25	N	-3 (-7)	-1 (-3)	1 (1.5)	+ _%
+ 0°	+ 0%	1+00	N	-12 (10)	-4.5(-6.5)	-3 (-1)	+ _%
+ 0°	+ 0%	_+75	N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+50	N	-23 (-20)	-9 (-12)	-4 (-8)	+ _%
+ 0°	+ 0%	_+25	N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	0+00	BL	-32 (-28)	-18 (-17)	-7 (-12)	+ _%
+ 0°	+ 0%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+25°	+47%	_+50	S	-30 (-25)	-12 (18)	-7 (-13)	+ 5%
+28°	+53%	_+75	S	-1.5(-2.5)	-0.5(-2.5)	0 (-1)	+10%
- 5°	- 9%	1+00	S	4.5(-0.3)	3 (0)	1 (1)	+10%
- 5°	- 9%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+10°	+19%	_+50	S	6 (-1.2)	3 (-0.5)	2.5(-2)	+10%
-10°	-19%	_+75	S	__._(_._)	__._(_._)	__._(_._)	+ 8%
-10°	-19%	2+00	S	10 (9)	5 (5)	4 (4)	+ _%
-10°	-19%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ 0%
+ 0°	+ 0%	_+50	S	7 (7)	3 (3)	3 (2)	+ 0%
+ 0°	+ 0%	_+75	S	4 (4)	1.5(2)	1 (-1)	- 5%
+ 5°	+ 9%	3+00	S	4.5(2.5)	4 (3)	3.5(1)	+ 0%

Grid:Eby N Coil Spacing: 200 m.

Line #:34+00 E Receiver N of Transmitter

Slope To Stn		Stn		3520 Hz IP (QP)	880 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
°	%	4+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
-15°	-27%	4+00	S	__._(_._)	__._(_._)	__._(_._)	+ _%
-15°	-27%	_+75	S	__._(_._)	__._(_._)	__._(_._)	+ _%
- 5°	- 9%	_+50	S	__._(_._)	__._(_._)	__._(_._)	+ _%
-10°	-17%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	3+00	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+75	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+50	S	4 (-4)	0 (-1)	-0.5(-1.5)	- 5%
+ 0°	+ 0%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 7°	+12%	2+00	S	2 (-2)	1 (0)	0 (1)	- 5%
+ 5°	+ 9%	_+75	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+13°	+23%	_+50	S	3.5(0)	1 (1)	1 (1)	+ 5%
-10°	-18%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
-15°	-26%	1+00	S	5 (4)	2 (0)	0 (1)	+ 0%
+ 0°	+ 0%	_+75	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+50	S	4 (4.5)	2.5(3)	4 (3.5)	+ 0%
+ 0°	+ 0%	_+25	S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	0+00	BL	3 (6)	2 (4)	2 (4)	+ 0%
+ 0°	+ 0%	_+25	N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+50	N	0 (-5)	-2 (-2.5)	-2 (0)	- 5%
+ 0°	+ 0%	_+75	N	-16 (-13)	-9 (-10)	-4 (-7)	+ 0%
+ 0°	+ 0%	1+00	N	-40 (-25)	-17 (-19)	-9 (-14)	+ 0%
+15°	+27%	_+25	N	__._(_._)	__._(_._)	__._(_._)	+ _%
+20°	+37%	_+50	N	-37 (-25)	-16 (-19)	-9 (-14)	+ 8%
+ 5°	+ 9%	_+75	N	__._(_._)	__._(_._)	__._(_._)	+ _%
-15°	-27%	2+00	N	-40 (-21)	-20 (-20)	-14 (-14)	+ 8%
-10°	+18%	_+25	N	-33 (-25)	-12 (-19)	-5 (-13)	+ 0%
+ 0°	+ 0%	_+50	N	-15 (-25)	-2 (-8)	-1.5(-1)	+ 0%
+ 0°	+ 0%	_+75	N	1 (-3.5)	3 (-2)	2 (1)	- 5%
+ 0°	+ 0%	3+00	N	23 (23)	6.5(12)	3 (8)	+ 0%
+ 0°	+ 0%	_+25	N	__._(_._)	__._(_._)	__._(_._)	+ 0%
+ 0°	+ 0%	_+50	N	7 (18)	1 (6)	-0.5(4)	+ 0%
+ 0°	+ 0%	_+75	N	__._(_._)	__._(_._)	__._(_._)	+ 0%
+ 0°	+ 0%	4+00	N	6.5(6)	1 (2.5)	1 (2)	+ 0%

Grid:Eby N Coil Spacing: 200 m.

Line #:37+00 E Receiver S of Transmitter

Slope To Stn		Stn	3520 Hz IP (QP)	880 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
+ °	+ %	4+25 N	__._(_._)	__._(_._)	__._(_._)	+ %
+ 0°	+ 0%	4+00 N	__._(_._)	__._(_._)	__._(_._)	+ %
+ 0°	+ 0%	_+75 N	__._(_._)	__._(_._)	__._(_._)	+ %
+10°	+18%	_+50 N	__._(_._)	__._(_._)	__._(_._)	+ %
-10°	+18%	_+25 N	5 (3)	2 (2)	2 (2)	+ 0%
-15°	-26%	2+00 N	8 (9)	2 (4)	2 (2)	+ 0%
- 5°	+ 0%	_+75 N	__._(_._)	__._(_._)	__._(_._)	+ 0%
+ 0°	+ 0%	_+50 N	30 (30)	5 (15)	7 (7)	+ 0%
+ 0°	+ 0%	_+25 N	-25 (-25)	-8 (-16)	-6 (-10)	+ 0%
+12°	+21%	1+00 N	-25 (-25)	-8 (-14)	-3 (-8)	+ 0%
+ 5°	+ 9%	_+75 N	__._(_._)	__._(_._)	__._(_._)	+ 0%
+10°	+18%	_+50 N	-20 (-18)	-11 (-13)	-5 (-10)	+ 0%
+ 0°	+ 0%	_+25 N	__._(_._)	__._(_._)	__._(_._)	+ 0%
+ 0°	+ 0%	0+00 BL	-25 (-20)	-13 (-20)	-12 (-13)	+ 0%
+ 0°	+ 0%	_+25 S	-25 (-15)	-13 (-17)	-10 (-13)	+ 0%
+ 0°	+ 0%	_+50 S	-30 (-20)	-17 (-25)	-13 (-20)	+ 0%
+ 0°	+ 0%	_+75 S	20 (-10)	8 (8)	5 (5)	+ 0%
+ 0°	+ 0%	1+00 S	9 (-12)	5 (2)	3 (3)	+ 0%
+ 5°	+ 9%	_+25 S	__._(_._)	__._(_._)	__._(_._)	+ 0%
+10°	+18%	_+50 S	10 (-5)	3 (0)	0 (0)	+ 5%
+25°	+47%	_+75 S	__._(_._)	__._(_._)	__._(_._)	+ 0%
+ 5°	+ 9%	2+00 S	3 (0)	0 (2)	-3 (-8)	+10%
-15°	-27%	2+25 S	__._(_._)	__._(_._)	__._(_._)	+ 0%
- 8°	-14%	2+50 S	To noisy to read (power line interference)			

Grid:Eby N Coil Spacing: 200 m.

Line #:38+00 E Receiver N of Transmitter

Slope To Stn		Stn	3520 Hz IP	3520 Hz (QP)	880 Hz IP	880 Hz (QP)	440 Hz IP	440 Hz (QP)	Slope Correction
°	%	2+75 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+12°	+21%	_+50 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+12°	+21%	_+25 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
-10°	-18%	2+00 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
- 5°	- 9%	_+75 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+10°	+18%	_+50 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+ 5°	+ 9%	_+25 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
-15°	-27%	1+00 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
-27°	-51%	_+75 S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
-18°	-33%	_+50 S	5	(3)	1.5	(6)	-5	(-4)	-10%
+ 0°	+ 0%	_+25 S	7	(7)	2	(5)	NR	(NR)	-10%
+ 0°	+ 0%	0+00 BL	7	(0)	3	(7)	5	(5)	-10%
+ 0°	+ 0%	_+25 N	7	(-12)	3	(1)	3	(-1)	-10%
+ 0°	+ 0%	_+50 N	-5	(-15)	-2	(-6)	1	(-4)	-10%
+ 0°	+ 0%	_+75 N	-12	(-20)	-4	(-8)	-1	(-4)	-15%
+ 0°	+ 0%	1+00 N	-17	(-25)	-4	(-10)	-2	(-5)	-10%
+ 0°	+ 0%	_+25 N	__._	(_._)	__._	(_._)	__._	(_._)	+ 0%
+ 0°	+ 0%	_+50 N	-30	(-30)	-12	(-17)	-7	(-7)	+ 0%
+ 0°	+ 0%	_+75 N	__._	(_._)	__._	(_._)	__._	(_._)	+ 0%
+ 0°	+ 0%	2+00 N	-25	(-25)	-10	(-13)	-7	(-7)	+ 0%
+ 0°	+ 0%	_+25 N	-19	(-25)	-7	(-11)	-6	(-7)	+ 0%
+ 0°	+ 0%	_+50 N	-10	(-15)	-4	(-5)	-2	(-4)	+ 0%
+ 0°	+ 0%	_+75 N	-5	(-14)	-3	(-5)	-2	(-3)	+ 0%
+ 5°	+ 9%	3+00 N	-1	(-2)	-2	(-2)	-2	(-1)	+ 0%
+15°	+27%	_+25 N	3	(2)	-2	(2)	-3	(0)	+ 5%
+12°	+21%	_+50 N	2	(-2)	-1	(0)	-1	(0)	+ 5%
+ 3°	+ 5%	_+75 N	__._	(_._)	__._	(_._)	__._	(_._)	+ 0%
- 7°	-12%	4+00 N	0	(-5)	-2	(-1)	-3	(0)	+ 5%
- 3°	+ 0%	_+25 N	__._	(_._)	__._	(_._)	__._	(_._)	+ 5%
+ 0°	+ 0%	4+50 N	0	(0)	-1.5	(0)	-2	(0)	+ 5%

0+50S to 1+50N 440 hz has power line noise

Grid:Eby N Coil Spacing: 100 m. (MaxMin 11)
Line #:38+50 E Receiver S of Transmitter

Slope To Stn		Stn	3555 Hz IP	(QP)	Slope Correction
°	%	4+50 N	__._	(_._)	+ %
+ 7°	+11%	_+25 N	__._	(_._)	+ _%
+ 0°	0%	4+00 N	__._	(_._)	+ %
+ 0°	+ 0%	_+75 N	__._	(_._)	+ _%
+ 0°	+ 0%	_+50 N	3	(5)	+ 0%
- 5°	- 8%	_+25 N	2	(5)	+ 0%
- 0°	+ 0%	3+00 N	4	(2)	+ 0%
- 8°	-13%	_+75 N	0	(3)	+ 0%
- 5°	- 8%	_+50 N	2	(-2)	- 5%
+ 0°	+ 0%	_+25 N	3	(3)	+ 0%
+ 0°	+ 0%	2+00 N	-12	(-16)	+ 0%
+ 0°	+ 0%	_+75 N	-12	(-17)	+ 0%
+ 0°	+ 0%	_+50 N	-7	(-9)	+ 0%
+ 0°	+ 0%	_+25 N	-3	(-3)	+ 0%
+ 0°	+ 0%	1+00 N	12	(30)	+ 0%
+ 0°	+ 0%	_+75 N	10	(15)	+ 0%
+ 0°	+ 0%	_+50 N	4	(-2)	+ 0%
+ 0°	+ 0%	_+25 N	-1	(-12)	+ 0%
+ 0°	+ 0%	0+00 BL	0	(-7)	+ 0%
+ 0°	+ 0%	_+25 S	4	(-6)	+ 0%
+ 0°	+ 0%	_+50 S	1	(-13)	+ 0%
+ °	+ %	1+13 N	2	(7)	+ 0%
+ °	+ %	1+37 N	-8	(-9)	+ 0%

Line terminted at 0+50S due to darkness.

Grid:Eby N Coil Spacing: 100 m.

Line #:39+00 E Receiver N of Transmitter

Slope To Stn	Stn	7040 Hz IP (QP)	1760 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
+ ° + %	4+50 N	__._(_._)	__._(_._)	__._(_._)	+ %
- 4° - 7%	_+50 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 4° + 7%	_+25 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+13° +23%	4+00 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+14° +25%	_+75 N	0 (6)	0 (2)	0 (0)	+12%
+ 0° + 0%	_+50 N	-2 (6)	-2 (2)	-3 (0)	+17%
- 8° -14%	_+25 N	5 (7)	3 (3)	3 (0)	+10%
-24° -45%	3+00 N	7 (9)	4 (3)	3 (1)	-10%
- 9° -16%	_+75 N	-1 (-3)	0 (-1)	0 (0)	-20%
- 9° -16%	_+50 N	-3 (-7)	0 (-2)	0 (0)	-25%
- 4° - 7%	_+25 N	-2 (-15)	2 (-4)	0 (0)	-20%
+ 4° + 7%	2+00 N	-17 (-19)	-2 (-10)	0 (-3)	-15%
+ 5° + 9%	_+75 N	-20 (-25)	-5 (-14)	1 (-5)	+ 0%
+ 0° + 0%	_+50 N	-25 (-20)	-7 (-15)	-1 (-5)	+ 0%
+ 0° + 0%	_+25 N	-19 (-25)	-7 (-12)	-2 (-5)	+ 5%
- 1° - 1%	1+00 N	23 (6)	5 (7)	2 (2)	+ 0%
+ 0° + 0%	_+75 N	2 (-13)	2 (-1)	1 (1)	+ 0%
+ 0° + 0%	_+50 N	-13 (-25)	0 (-10)	2 (-2)	+ 0%
+ 0° + 0%	_+25 N	-11 (-11)	-1 (-8)	1 (-1)	+ 0%
+ 0° + 0%	0+00 BL	-6 (-1)	-1 (-6)	0 (-1)	+ 0%
+ 0° + 0%	_+75 S	19 (15)	6 (10)	3 (4)	+ 0%
+ 0° + 0%	_+50 S	20 (25)	6 (10)	3 (4)	+ 0%
+ 0° + 0%	_+25 S	0 (-3)	0 (0)	0 (3)	+ 0%
+ 0° + 0%	1+00 S	-8 (-12)	-4 (-7)		+ 0%
+ 6° +10%	_+25 S	-8 (-12)	-4 (-7)	Power Line	+ 0%
+ 6° +10%	_+50 S	-4 (-12)	0 (-6)	Noise	+ 5%
+22° +40%	_+75 S	1 (-3)	2 (-2)	No Readings	+15%
+ 0° + 0%	2+00 S	1 (1)	1 (1)		+15%
+ 0° + 0%	1+13 N	-6 (-12)	-2 (-4)	-1 (-1)	+ 0%
+ 0° + 0%	2+13 N	-10 (-17)	-1 (-7)	1 (-2)	+ 0%

Grid:Eby N Coil Spacing: 100 m. (MaxMin 11)
Line #:39+50E Receiver N of Transmitter

Slope To Stn		Stn		3555 Hz IP	(QP)	Slope Correction
+ 0°	+ 0%	_+25	S	__._	(_._)	+ _%
+ 0°	+ 0%	1+00	S	__._	(_._)	+ _%
+ 0°	+ 0%	_+75	S	__._	(_._)	+ _%
+ 0°	+ 0%	_+50	S	4	(0)	+ 0%
+10°	+18%	_+25	S	-1	(-2)	+ 5%
-20°	-36%	0+00	BL	5	(5)	- 5%
- 2°	- 3%	_+25	N	7	(5)	- 5%
- 2°	- 3%	_+50	N	18	(20)	- 5%
+ 0°	+ 0%	_+75	N	23	(23)	-10%
+ 0°	+ 0%	1+00	N	-3	(-8)	+ 0%
+15°	+27%	_+25	N	-10	(-15)	+ 5%
-10°	-18%	_+50	N	-5	(-18)	+ 0%
+ 0°	+ 0%	_+75	N	11	(-5)	+ 0%
+ 0°	+ 0%	2+00	N	7	(6)	+ 0%
+ 0°	+ 0%	_+25	N	-10	(-15)	- 5%
+ 0°	+ 0%	_+50	N	-14	(-22)	+ 0%
+15°	+27%	_+75	N	-14	(-18)	+ 5%
+15°	+27%	3+00	N	-3	(-6)	+15%
+10°	+17%	_+25	N	-1	(-2)	+15%
+ 5°	+ 8%	_+50	N	-3	(1)	+20%
+ 0°	+ 0%	_+75	N	-1	(8)	+15%
-10°	-18%	4+00	N	3	(8)	+ 5%
-15°	-27%	_+25	N	5	(8)	-10%
-10°	-18%	4+50	N	5	(7)	-15%
+ _°	+ _%	3+13	N	0	(-3)	+15%
+ _°	+ _%	2+13	N	-7	(-8)	+ 0%
+ _°	+ _%	0+87	N	-2	(-18)	+ 0%
+ _°	+ _%	1+12	N	-10	(-13)	+ 0%

Grid:Eby N Coil Spacing: 50 m.

Line #:40+00 E Receiver S of Transmitter

Slope To Stn Correction	Stn	14080 Hz IP	14080 Hz (QP)	7040 Hz IP	7040 Hz (QP)	1760 Hz IP	1760 Hz (QP)	440 Hz IP	440 Hz (QP)	Slope
-10° -17%	2+75 N	4	(5)	5	(3)	3	(1)	4	(0)	-10%
+ 0° + 0%		__._	(_._)	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
- 5° - 9%	_+50 N	4	(3)	3	(2)	1	(1)	2	(0)	-15%
+ 0° + 0%		6	(-3)	5	(-2)	4	(0)	4	(0)	-10%
+ 0° + 0%	_+25 N	3	(-10)	3	(-5)	3	(-1)	3	(0)	- 5%
+ 0° + 0%		15	(-13)	15	(-6)	13	(-2)	13	(-1)	+ 0%
+ 0° + 0%	2+00 N	2	(-8)	1	(-4)	0	(-1)	0	(0)	+ 0%
+ 0° + 0%		0	(-7)	0	(-5)	0	(-2)	1	(-1)	+ 0%
+ 0° + 0%	_+75 N	-5	(-14)	-1	(-9)	0	(-3)	11	(-1)	+ 0%
+ 0° + 0%		-1	(-5)	3	(-13)	5	(-5)	7	(-2)	+ 0%
+ 0° + 0%	_+50 N	-3	(-25)	-1	(-13)	0	(-3)	0	(-1)	+ 0%
+ 0° + 0%		__._	(_._)	__._	(_._)	__._	(_._)	__._	(_._)	+ 0%
+ 5° + 9%	_+25 N	5	(0)	19	(5)	13	(3)	11	(0)	+ 5%
+ 0° + 0%		18	(14)	17	(11)	6	(5)	4	(2)	+ 5%
- 5° - 9%	1+00 N	25	(30)	17	(19)	10	(7)	8	(2)	+ 0%
+ 0° + 0%		20	(25)	15	(14)	10	(5)	9	(2)	+ 0%
+ 0° + 0%	_+75 N	-14	(-11)	-10	(-10)	-4	(-4)	-3	(-2)	- 5%
+ 0° + 0%		-20	(-20)	-14	(-17)	-4	(-8)	-1	(-2)	+ 0%
+ 0° + 0%	_+50 N	-23	(-23)	-15	(-18)	-20	(-20)	0	(-2)	+ 0%
+ 0° + 0%		-6	(-13)	-4	(-9)	0	(-4)	0	(-2)	+ 0%
+ 5° + 9%	_+25 N	11	(3)	8	(5)	2	(3)	__._	(_._)	+ 5%
+ 0° + 0%		10	(4)	8	(5)	4	(3)	__._	(_._)	+10%
+10° +18%	0+00 BL	0	(6)	0	(3)	-2	(1)	__._	(_._)	+15%
+ 0° + 0%	1+94 N	2	(-6)	1	(-3)	1	(-1)	1	(0)	+ 0%

Grid:Eby N Coil Spacing: 100 m.
Line #:40+00 E Receiver N of Transmitter

Slope To Stn		Stn	3520 Hz IP (QP)	880 Hz IP (QP)	440 Hz IP (QP)	Slopy Correction
°	%	0+75 S	__._(_._)	__._(_._)	__._(_._)	%
+ 5°	+ 9%	0+50 S	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 5°	+ 9%	_+25 S	__._(_._)	__._(_._)	__._(_._)	+ _%
-10°	-18%	0+00 BL	__._(_._)	__._(_._)	__._(_._)	+ _%
-10°	-18%	_+25 N	5 (1)	6 (3)	2 (0)	- 5%
- 7°	-11%	_+50 N	10 (7)	7 (5)	5 (0)	-10%
+ 0°	+ 0%	_+75 N	1 (0)	3 (5)	2 (6)	-10%
+ 0°	+ 0%	1+00 N	-17 (-16)	-6 (-10)	-2 (-5)	- 7%
+ 8°	+14%	_+25 N	-23 (-23)	-6 (-14)	0 (-5)	+ 0%
+ 0°	+ 0%	_+50 N	-20 (-30)	-3 (-15)	0 (-3)	+ 0%
+ 0°	+ 0%	_+75 N	0 (0)	3 (-6)	1 (-1)	+ 5%
+ 0°	+ 0%	2+00 N	6 (-7)	3 (1)	1 (1)	+ 5%
+ 0°	+ 0%	_+25 N	-13 (-23)	-5 (-9)	-1 (-3)	+ 0%
+ 0°	+ 0%	_+50 N	-20 (-25)	-7 (-13)	-1 (-4)	+ 0%
+ 5°	+ 9%	_+75 N	-16 (-23)	-5 (-11)	-1 (-5)	+ 0%
+15°	+27%	3+00 N	-2 (-8)	0 (-3)	0 (-1)	+10%
+ 0°	+ 0%	_+25 N	2 (-1)	1 (0)	0 (1)	+10%
- 7°	-12%	_+50 N	2 (0)	1 (3)	1 (1)	+ 5%
+ 0°	+ 0%	_+75 N	4 (14)	1 (5)	0 (1)	+ 0%
+ 0°	+ 0%	4+00 N	5 (-3)	2 (0)	2 (0)	+ 0%
+ 0°	+ 0%	_+25 N	3 (-2)	1 (-1)	0 (0)	+ 0%
+ 0°	+ 0%	_+50 N	3 (-9)	2 (-2)	1 (-1)	+ 0%
+ 5°	+ 8%	_+75 N	1 (-7)	0 (-2)	0 (0)	+ 0%
+ 5°	+ 8%	5+00 N	2 (5)	0 (1)	0 (0)	+ 0%
+ 5°	+ 8%	_+25 N	1 (2)	0 (1)	-1 (0)	+ 5%
+ 0°	+ 0%	5+50 N	0 (12)	-1 (3)	-1 (0)	+ 0%
+ 0°	+ 0%	2+88 N	-11 (-17)	-4 (-8)	-2 (-2)	+ 5%
+ 0°	+ 0%	2+13 N	-5 (-18)	-2 (-6)	0 (-3)	+ 0%
+ 0°	+ 0%	1+63 N	-17 (-23)	-2 (-13)	0 (-2)	+ 5%
+ 0°	+ 0%	0+88 N	2 (-4)	0 (-1)	-1 (-1)	- 7%

Grid:Eby N Coil Spacing: 100 m. (MaxMin 11)
Line #:40+50E Receiver S of Transmitter

Slope To Stn		Stn	3555 Hz IP	(QP)	Slope Correction
°	%	_+75 N	__._	(_._)	+ _%
+ 5°	+ 8%	_+50 N	__._	(_._)	+ _%
+ 5°	+ 8%	_+25 N	__._	(_._)	+ _%
- 5°	- 8%	4+00 N	__._	(_._)	+ %
-10°	-18%	_+75 N	3	(12)	- 5%
+ 0°	+ 0%	_+50 N	8	(4)	- 5%
+ 0°	+ 0%	_+25 N	2	(-2)	- 5%
+ 0°	+ 0%	3+00 N	-1	(-5)	- 5%
+ 0°	+ 0%	_+75 N	5	(0)	+ 0%
+12°	+20%	_+50 N	4	(1)	+ 5%
- 6°	-10%	_+25 N	7	(4)	+ 0%
- 6°	-10%	2+00 N	10	(5)	+ 0%
+ 0°	+ 0%	_+75 N	-5	(-9)	+ 0%
+ 0°	+ 0%	_+50 N	-11	(-13)	- 5%
+ 0°	+ 0%	_+25 N	-13	(-14)	+ 0%
+ 0°	+ 0%	1+00 N	- 4	(-7)	+ 0%
+ 0°	+ 0%	_+75 N	7	(-5)	+ 0%
+ 0°	+ 0%	_+50 N	3	(-5)	+ 0%
+ 0°	+ 0%	_+25 N	-3	(-9)	+ 0%
+15°	+27%	0+00 BL	-5	(-10)	+ 5%
+ 5°	+ 8%	_+25 S	12	(12)	+10%
+ 0°	+ 0%	_+50 S	9	(9)	+10%
+ 0°	+ 0%	_+75 S	13	(10)	+10%
+ _°	+ _%	0+87 N	3	(-2)	+ _%
+ _°	+ _%	1+12 N	-10	(-12)	+ _%
+ _°	+ _%	1+66 N	-8	(-12)	+ _%
+ _°	+ _%	1+88 N	7	(4)	+ _%

Grid:Eby N Coil Spacing: 100 m.

Line #:41+00 E Receiver N of Transmitter

Slope To Stn	Stn	7040 Hz IP (QP)	1760 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
+15° +27%	4+75 N	1 (0)	-3 (2)	-3 (0)	-10%
+ 9° +16%	_+50 N	2 (7)	2 (2)	2 (0)	-20%
- 3° - 5%	_+25 N	3 (7)	2 (2)	1 (0)	-20%
- 3° - 5%	4+00 N	2 (1)	0 (0)	0 (0)	-20%
-30° -57%	_+75 N	1 (0)	5 (0)	4 (0)	+15%
-12° -21%	_+50 N	4 (1)	2 (1)	1 (1)	+ 5%
+ 0° + 0%	_+25 N	5 (2)	3 (2)	1 (1)	+ 5%
+11° +19%	3+00 N	13 (22)	7 (8)	3 (3)	+ 0%
+ 7° +13%	_+75 N	15 (20)	9 (10)	5 (6)	-10%
- 7° -12%	_+50 N	-35 (-13)	-20 (-15)	-7 (-10)	-15%
- 8° -14%	_+25 N	-35 (-17)	-20 (-20)	-5 (-12)	-10%
- 7° -12%	2+00 N	-35 (-20)	-20 (-20)	-5 (-12)	-10%
+ 0° + 0%	_+75 N	-25 (-20)	-15 (-13)	-6 (-7)	+ 0%
+ 0° + 0%	_+50 N	-5 (-25)	2 (-9)	P.Line Noise	+15%
+ 0° + 0%	_+25 N	-3 (-12)	-2 (-10)	3 (-5)	+15%
+ 0° + 0%	1+00 N	-6 (0)	-2 (0)	P.Line Noise	+15%
+ 0° + 0%	_+75 N	0 (-2)	2 (1)	P.Line Noise	+15%
+37° +63%	_+50 N	__._(_._)	__._(_._)	__._(_._)	+ _%
- 5° - 9%	_+25 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 8° +14%	0+00 BL	__._(_._)	__._(_._)	__._(_._)	+ _%
°	% 0+25 S	__._(_._)	__._(_._)	__._(_._)	%

+ 0° + 0%	2+62 S	9 (25)	5 (10)	-2 (7)	-10%

Grid:Eby N Coil Spacing: 100 m. (MaxMin 11)
Line #:41+50E Receiver N of Transmitter

Slope To Stn		Stn		3555 Hz IP (QP)		Slope Correction
°	%	4+25	S	__._(_._)		%
+ 0°	+ 0%	4+00	S	__._(_._)		+ %
+ 0°	+ 0%	_+75	S	__._(_._)		+ _%
+ 0°	+ 0%	_+50	S	__._(_._)		+ _%
+ 0°	+ 0%	_+25	S	7	(2)	+ 0%
+ 0°	+ 0%	3+00	S	7	(5)	+ 0%
+ 0°	+ 0%	_+75	S	8	(2)	+ 0%
+ 1°	+ 2%	_+50	S	7	(1)	+ 0%
+ 0°	+ 0%	_+25	S	8	(1)	+ 0%
+ 0°	+ 0%	2+00	S	8	(5)	+ 0%
+ 0°	+ 0%	_+75	S	7	(10)	+ 0%
+ 0°	+ 0%	_+50	S	5	(12)	+ 0%
+ 0°	+ 0%	_+25	S	12	(7)	+ 0%
+ 0°	+ 0%	1+00	S	12	(5)	+ 0%
+ 1°	+ 2%	_+75	S	6	(5)	+ 0%
+ 2°	+ 3%	_+50	S	11	(5)	+ 0%
+ 0°	+ 0%	_+25	S	10	(5)	+ 0%
-12°	-20%	0+00	BL	15	(-5)	- 5%
+ 0°	+ 0%	_+25	N	8	(-5)	- 5%
- 5°	- 8%	_+50	N	8	(-5)	- 5%
- 2°	- 3%	_+75	N	12	(-5)	- 5%
+ 0°	+ 0%	1+00	N	8	(0)	+ 0%
+ 0°	+ 0%	_+25	N	5	(-2)	+ 0%
+ 0°	+ 0%	_+50	N	8	(-18)	+ 0%
+ 0°	+ 0%	_+75	N	-35	(-25)	+ 0%
+ 7°	+12%	2+00	N	-35	(-25)	+ 0%
- 5°	- 8%	_+25	N	-33	(-23)	+ 0%
+ 0°	+ 0%	_+50	N	-16	(-16)	+ 0%
+ 0°	+ 0%	_+75	N	+20	(18)	+ 0%
+15°	+27%	3+00	N	9	(7)	+ 5%
+18°	+32%	_+25	N	4	(3)	+15%
+ 7°	+12%	_+50	N	1	(1)	+15%
+ 4°	+ 7%	_+75	N	-2	(5)	+20%
+ 0°	+ 0%	4+00	N	-10	(5)	+15%
+ 0°	+ 0%	_+25	N	0	(5)	+ 5%
- 5°	- 8%	_+50	N	0	(7)	+ 0%
- 5°	- 8%	4+75	N	2	(9)	- 5%
+ _°	+ _%	2+66	N	3	(4)	+ 0%
+ _°	+ _%	1+66	N	0	(-18_)	+ 0%

Grid:Eby N Coil Spacing: 100 m.

Line #:42+00 E Receiver N of Transmitter

Slope To Stn		Stn	7040 Hz IP (QP)	1760 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
°	0%	0+00 N	__._(_._)	__._(_._)	__._(_._)	%
-26°	-46%	_+25 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	0%	_+50 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	_+75 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0°	+ 0%	1+00 N	3 (- 6)	2 (- 2)	0 (0)	-10%
+ 0°	+ 0%	_+25 N	-8 (-14)	- 5 (-6)	- 2 (- 3)	+ 0%
+ 0°	+ 0%	_+50 N	-25 (-25)	-13 (-13)	- 5 (- 7)	+ 0%
+ 0°	+ 0%	_+75 N	-50 (-25)	-23 (-25)	- 7 (-13)	+ 0%
+ 0°	+ 0%	2+00 N	-40 (-25)	-20 (-25)	- 2 (-10)	+ 0%
+ 0°	+ 0%	_+25 N	-30 (-30)	-15 (-20)	- 5 (-10)	+ 0%
+ 0°	+ 0%	_+50 N	- 4 (-15)	- 3 (-14)	- 5 (- 5)	+ 0%
+18°	+33%	_+75 N	6 (5)	7 (- 0)	5 (1)	+ 0%
+ 5°	+ 9%	3+00 N	2 (0)	3 (0)	2 (4)	+10%
+ 2°	+ 3%	_+25 N	3 (- 1)	1 (0)		+10%
+ 0°	+ 0%	_+50 N	3 (0)	4 (2)		+10%
-26°	-46%	_+75 N	0 (5)	2 (4)		+ 0%
+ 0°	+ 0%	4+00 N	4 (7	3 (3)		+ 0%
+ 0°	+ 0%	2+62 N	5 (5)	6 (6)	2.5(-5)	+ _%
+ 0°	+ 0%	2+38 N	-23 (-24)	-15 (-17_)	__._(_._)	+ _%
+ 0°	+ 0%	2+12 N	-40 (-30)	-20 (-25)	-5 (-9)	+ _%

Grid:Eby N Coil Spacing: 100 m.
Line #:42+50 E Receiver N of Transmitter

Slope To Stn		Stn		7040 Hz IP	7040 Hz (QP)	1760 Hz IP	1760 Hz (QP)	440 Hz IP	440 Hz (QP)	Slope Correction
°	%	4+00	S	__._	(_._)	__._	(_._)	__._	(_._)	%
+ 5°	+ 9%	4+00	S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+ 3°	+ 5%	3+75	S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+10°	+18%	3+50	S	__._	(_._)	__._	(_._)	__._	(_._)	+ _%
+ 0°	+ 0%	3+25	S	-2	(2)	-2	(1)	-2	(0)	+ 8%
+ 0°	+ 0%	3+00	S	0	(3)	-1	(1)	-2	(0)	+ 5%
+ 0°	+ 0%	2+75	S	0	(3)	-1	(1)	-1	(0)	+ 5%
-10°	-18%	2+50	S	5	(3)	4	(1)	4	(0)	- 5%
+ 0°	+ 0%	2+25	S	0	(0)	1	(1)	0	(0)	- 5%
+ 0°	+ 0%	2+00	S	3	(1)	2	(0)	3	(0)	- 5%
+ 0°	+ 0%	1+75	S	3	(3)	2	(1)	2	(1)	- 5%
+ 0°	+ 0%	1+50	S	0	(1)	-0.5	(0.5)	-1	(0)	+ 0%
+ 0°	+ 0%	1+25	S	-1	(2)	-2	(1)	-2	(0)	+ 0%
+ 0°	+ 0%	1+00	S	-1	(7)	-1.5	(2)	-2	(1)	+ 0%
-12°	-21%	0+75	S	1	(-1)	0	(2)	-1	(1)	- 5%
- 5°	- 9%	0+50	S	3	(2)	3	(1)	1	(1)	- 8%
- 7°	-12%	0+25	S	6	(2)	4	(1)	3	(1)	-10%
- 5°	- 9%	0+00	BL	5	(2)	3	(2)	0	(2)	-12%
+ 0°	+ 0%	0+25	N	5	(-1)	3	(2)	0	(2)	-12%
+ 0°	+ 0%	0+38	N	5	(0)	3	(3)	-1	(3)	-12%
+ 0°	+ 0%	0+50	N	9	(-4)	6	(2)	-3	(2)	-12%
+ 0°	+ 0%	0+87	N	3	(-20)	2	(-5)	3	(-2)	+ 0%
+ 0°	+ 0%	1+00	N	-4	(-25)	-2	(-7)	0	(-5)	+ 0%
+ 0°	+ 0%	1+12	N	-12	(-25)	-5	(-10)	0	(-7)	+ 0%
+ 0°	+ 0%	1+25	N	-18	(-25)	-9	(-12)	3	(-7)	+ 0%
+ 0°	+ 0%	1+37	N	-20	(-30)	-9	(-12)	0	(-7)	+ 0%
+ 0°	+ 0%	1+87	N	-17	(-23)	-8	(-12)	0	(-4)	+ 0%
+ 0°	+ 0%	2+00	N	-16	(-19)	-9	(-12)	Noisy		+ 0%
+ 0°	+ 0%	2+13	N	-5	(-15)	-4	(-9)	__._	(_._)	+ 0%
+ 0°	+ 0%	2+25	N	1	(-14)	0	(-15)	0	(-10)	+ 0%
+ 0°	+ 0%	2+38	N	-3	(-25)	-2	(-18)	__._	(_._)	+ 0%
+ 0°	+ 0%	2+50	N	0	(-25)	0	(-20)	__._	(_._)	+ 0%
+ 5°	+ 9%	2+75	N	4	(-12)	4	(-10)	__._	(_._)	+ 0%
+ 3°	+ 5%	3+00	N	0	(-7)	0	(-4)	__._	(_._)	+ 0%
+ 3°	+ 5%	3+25	N	2	(0)	1	(1)	__._	(_._)	+ 5%
+ 5°	+ 9%	3+50	N	2	(12)	0	(4)	__._	(_._)	+ 7%
+ 0°	+ 0%	3+75	N	2	(7)	0	(3)	__._	(_._)	+ 5%
+ 0°	+ 0%	4+00	N	-1	(8)	-2	(2)	__._	(_._)	+ 0%
-10°	-18%	4+25	N	0	(7)	-1	(2)	__._	(_._)	+ 0%
+ 0°	+ 0%	4+50	N	1	(-1)	1	(0)	__._	(_._)	- 5%

Grid:Eby N Coil Spacing: 100 m.
Line #:43+00E Receiver S of Transmitter

Slope To Stn		Stn		3555 Hz IP	(QP)	Slope Correction
°	%	5+00	N	__._	(_._)	+ %
+ 0°	+ 0%	_+75	N	__._	(_._)	+ _%
+ 0°	+ 0%	_+50	N	__._	(_._)	+ _%
+ 0°	+ 0%	_+25	N	__._	(_._)	+ _%
+ 0°	+ 0%	4+00	N	7	(-5)	+ 0%
+ 0°	+ 0%	_+75	N	8	(-2)	+ 0%
+ 0°	+ 0%	_+50	N	6	(-1)	+ 0%
+ 0°	+ 0%	_+25	N	9	(8)	+ 0%
+ 0°	+ 0%	3+00	N	11	(14)	+ 0%
+ 0°	+ 0%	_+75	N	9	(9)	+ 0%
+ 0°	+ 0%	_+50	N	9	(4)	+ 0%
+ 0°	+ 0%	_+25	N	8	(4)	+ 0%
+ 0°	0%	2+00	N	5	(-10)	+ 0%
+ 0°	+ 0%	_+75	N	6	(-7)	+ 0%
+ 0°	+ 0%	_+50	N	2	(-5)	+ 0%
+ 0°	+ 0%	_+25	N	3	(-13)	+ 0%
+ 0°	+ 0%	1+00	N	5	(-8)	+ 0%
+ 0°	+ 0%	_+75	N	8	(-5)	+ 0%
+ 0°	+ 0%	_+50	N	8	(-7)	+ 0%
+ 0°	+ 0%	_+25	N	-2	(-15)	+ 0%
+ 0°	+ 0%	0+00	BL	-3	(-15)	+ 0%
+ 5°	+ 8%	_+25	S	8	(-5)	+ 2%
+17°	+30%	_+50	S	23	(10)	+10%
- 5°	- 8%	_+75	S	18	(12)	+ 5%
+ 5°	+ 8%	1+00	S	13	(8)	+ 5%
+ 5°	+ 8%	_+25	S	12	(8)	+ 5%
+10°	+17%	_+50	S	13	(7)	+ 5%
+ 0°	+ 0%	_+75	S	16	(6)	+ 5%
+ 0°	+ 0%	2+00	S	4	(5)	+10%
+ 0°	+ 0%	_+25	S	12	(7)	+ 5%
+10°	+17%	_+50	S	3	(4)	+ 5%
+ 2°	+ 3%	_+75	S	1	(5)	+ 5%
+ 2°	+ 3%	3+00	S	6	(5)	+ 5%
+ 2°	+ 3%	_+25	S	5	(5)	+ 5%
+ 0°	+ 0%	_+50	S	5	(5)	+ 0%
+ 0°	+ 0%	_+75	S	4	(4)	+ 0%
- 2°	- 3%	4+00	S	5	(5)	+ 0%
- 2°	- 3%	4+25	S	8	(6)	+ 0%
+ _°	+ _%	0+37	S	1	(-12)	+ _%

Grid:Eby N Coil Spacing: 100 m.
Line #:43+50 E Receiver S of Transmitter

Slope To Stn	Stn	7040 Hz IP (QP)	1760 Hz IP (QP)	440 Hz IP (QP)	Slope Correction
+ 0° + 0%	_+50 N	__._(__._)	__._(__._)	__._(__._)	+ _%
+ 0° + 0%	_+25 N	__._(__._)	__._(__._)	__._(_._)	+ _%
+ 0° + 0%	4+00 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0° + 0%	_+75 N	__._(_._)	__._(_._)	__._(_._)	+ _%
+ 0° + 0%	_+50 N	-1 (0)	0 (1)	Noisy	+ 0%
+ 0° + 0%	_+25 N	1 (0)	-1 (-1)	Noisy	+ 0%
+ 0° + 0%	3+00 N	-1 (-2)	-2 (-1)	Noisy	+ 0%
+ 0° + 0%	_+75 N	-1 (-3)	0 (-1)	0 (-1)	+ 0%
+ 0° + 0%	_+50 N	0 (-15)	1 (-4)	1 (1)	+ 0%
+ 0° + 0%	_+25 N	0 (0)	2 (2)	0 (1)	+ 0%
+ 0° + 0%	2+00 N	-2 (-20)	0 (-4)	0 (1)	+ 0%
+ 0° + 0%	_+75 N	-12 (-25)	-3 (-8)	-2 (-2)	+ 0%
+ 0° + 0%	_+50 N	-20 (-25)	-4 (-12)	-1 (-4)	+ 0%
+ 0° + 0%	_+25 N	-18 (-25)	-5 (-12)	-2 (-4)	+ 0%
+ 0° + 0%	1+00 N	-3 (-2.5)	2 (-5)	0 (2)	+ 0%
+ 0° + 0%	_+75 N	25 (-20)	6 (4)	0 (4)	+ 0%
+ 0° + 0%	_+50 N	25 (25)	5 (6)	-1 (2)	+ 0%
+ 0° + 0%	_+25 N	-7 (-25)	-8 (-7)	-5 (-4)	+ 0%
+ 2° + 3%	0+00 BL	-30 (-30)	-15 (-17)	-6 (-10)	+ 8%
+15° +27%	_+25 S	-30 (-25)	-16 (-14)	-7 (-9)	+ 0%
+ 5° + 9%	_+50 S	-9 (-14)	-3 (-6)	0 (0)	+10%
+ 0° + 0%	_+75 S	7 (-7)	9 (1)	4 (5)	+10%
+ 0° + 0%	1+00 S	17 (9)	12 (7)	5 (5)	+ 0%
+ 1° + 2%	_+25 S	6 (7)	4 (4)	0 (4)	+ 0%
+ 0° + 0%	_+50 S	3 (5)	1 (3)	0 (2)	+ 0%
+ 0° + 0%	_+75 S	1 (4)	0 (2)	-1 (1)	+ 0%
+ 0° + 0%	2+00 S	-1 (3)	0 (2)	-2 (0)	+ 0%
+ 0° + 0%	_+25 S	1 (-1)	0 (0)	-1 (0)	+ 0%
+ 0° + 0%	_+50 S	0 (0)	0 (0)	-1 (0)	+ 0%
+15° +27%	_+75 S	-1 (0)	-2 (0)	-2 (0)	+ 8%
+15° +27%	3+00 S	3 (0)	2 (0)	1 (0)	+15%
+15° +27%	_+25 S	-1 (1)	-2 (1)	-3 (0)	+20%
+ 0° + 0%	_+50 S	-1 (3)	0 (1)	-1 (0)	+20%
-15° -27%	_+75 S	0 (-1)	0 (0)	0 (0)	+ 8%
- 5° - 9%	4+00 S	1 (2)	0 (1)	-1 (0)	+ 5%
- 5° - 9%	_+25 S	-1 (2)	-1 (1)	-1 (0)	+ 0%
+ 0° + 0%	0+63 S	2 (-10)	4 (-2)	1 (2)	+ _%
+ 0° + 0%	0+37 S	-20 (-20)	-8 (-10)	-3 (-6)	+ _%
+ 0° + 0%	0+87 N	13 (-25)	1 (0)	1 (0)	+ _%
+ 0° + 0%	1+13 N	-13 (-25)	-3 (-9)	-2 (-2)	+ _%
+ 0° + 0%	1+87 N	-7 (-25)	-1 (-7)	-1 (-2)	+ _%

INVOICE FOR MaxMin EM SURVEY OF JAMES REED CLAIM GROUP IN OTTO AND EBY TOWNSHIPS

Dates of Survey August 10, 11, 12, 1994
December 31, 1994
January 1, 1995
Dates of report preparation January 6, 7, 8, 1994

LINE	COIL SEPARATION (m)	TRAVERSE LENGTH(m)	MEASURED TOPOGRAPHY	
32+65	200	700	700	(440,880,3520 Hz)
34+00	200	850	850	(440,880,3520 Hz)
37+00	200	625	625	(440,880,3520 Hz)
38+00	200	700	700	(440,880,3520 Hz)
38+50	100	500	500	(3555 Hz)
39+00	100	675	675	(440,1760, 7040 Hz)
39+50	100	600	600	(3555 Hz)
40+00	100	625	625	(440,1760, 7040 Hz)
40+00	50	325	325	(440,1760, 7040 Hz)
40+50	100	550	550	(3555 Hz)
41+00	100	500	500	(440,1760, 7040 Hz)
41+50	100	900	900	(3555 Hz)
42+00	100	400	400	(440,1760, 7040 Hz)
42+50	100	875	875	(440,1760, 7040 Hz)
43+00	100	925	925	(3555 Hz)
43+50	100	875	875	(440,1760, 7040 Hz)
Total		10625	106250	

First frequency 10.625 km @ $200/km =	$2125.00
2 additional frequencies: each at @ $25/km	
2 X $25/km X 7.15 km =	$ 357.00
Totography measurement	
$25 X 10.625 km =	$ 265.00
TOTAL BALANCE OWING	$2747.00

Douglas Robinson

Douglas Robinson, P. Eng.
January 8, 1998

MAX-VIN ... SPECIFICATIONS:

... frequencies:	110, 220, 440, 880, 1760, 3520, 7040 and 14080 Hz, plus 50/60 Hz powerline frequency (receiver only).
... modes:	MAX 1: Horizontal loop mode (Transmitter and receiver coil planes horizontal and coplanar). MAX 2: Vertical coplanar loop mode (Transmitter and receiver coil planes vertical and coplanar). MAX 3: Vertical coaxial loop mode (Transmitter and receiver coil planes vertical and coaxial). MIN 1: Perpendicular loop mode 1 (Transmitter coil plane horizontal and receiver coil plane vertical). MIN 2: Perpendicular loop mode 2 (Transmitter coil plane vertical and receiver coil plane horizontal).
... ranges:	12.5, 25, 50, 75, 100, 125, 150, 200, 250, 300, & 400 metres (standard). 10, 20, 40, 60, 80, 100, 120, 160, 200, 240 & 320 metres (selected with grid switch inside of receiver). 50, 100, 200, 300, 400, 500, 600, 800, 1000, 1200 & 1600 feet (selected with grid switch inside of receiver).
... measurements:	In-Phase and quadrature components of the secondary magnetic field, in % of primary (transmitted) field. Field amplitude and/or tilt of 50/60 Hz powerline field.
... readouts:	Analog direct readouts on edgewise panel meters for in-phase, quadrature and tilt, and for 50/60Hz amplitude. (Additional digital readouts when using the DAC, for which interfacing and controls are provided for plug-in).
... scales:	Analog in-phase and quadrature scales: 0±4%, 0±20%, 0±100%, switch activated. Analog tilt scale: 0±75% grade. (Digital in-phase and quad. 0±102.4%).
... resolution:	Analog in-phase and quadrature 0.05% to 0.5%, analog tilt 1% grade. (Digital in-phase and quadrature 0.1%).
... repeatability:	±0.05% to ±1% normally, depending on frequency, coil separation & conditions.
Powerline filtering:	Powerline comb filter, continuous spherics noise clipping, autoadjusting time constant and other filtering.
... lights:	Receiver signal and reference warning lights to indicate potential errors.
... depth:	From surface down to 1.5 times coil separation used.
... scale:	110 Hz: 220 Atm² 1760 Hz: 160 Atm² 220 Hz: 215 Atm² 3520 Hz: 80 Atm² 440 Hz: 210 Atm² 7040 Hz: 40 Atm² 880 Hz: 200 Atm² 14080 Hz: 20 Atm²
Reference cable:	Light weight unshielded 4/2 conductor teflon cable for maximum temperature range and for minimum friction. Please specify cable lengths required.
Intercom:	Voice communication link provided for operators via the reference cable.
... power supply:	Four standard 9V batteries (0.5Ah, alkaline). Life 30 hrs continuous duty, less in cold weather. Rechargeable battery and charger option available.
Transmitter power supply:	Rechargeable sealed gel type lead acid 12V-13Ah batteries [4x6V-6½Ah] in canvas belt. Optional 12V-8Ah light duty belt pack available.
Transmitter battery ...	For 110-120/220-240VAC, 50/60/400 Hz and 12-15VDC supply operation, automatic float charge mode, three charge status indicator lights. Output 14.4V-1.25A nominal.
... temperature:	−40 to + 60 degrees Celsius.
... weight:	8 kg, including the two integral ferrite cored antennas (9 kg with data acq. computer).
... weight:	16 kg with standard 12V-13Ah battery pack. 14 kg with light duty 12V-8Ah pack.
Shipping weight:	60 kg plus weight of reference cables at 2.8 kg per 100 metres plus other optional items if any.
Spare parts:	One spare transmitter battery pack, one spare transmitter battery charger, two spare transmitter retractile connecting cords, one spare set receiver batteries.

Specifications subject to change without notification.

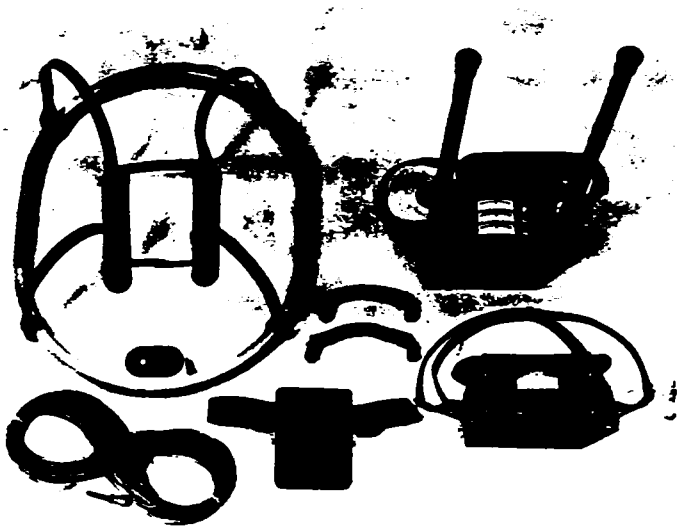
... PARAMETRICS LIMITED

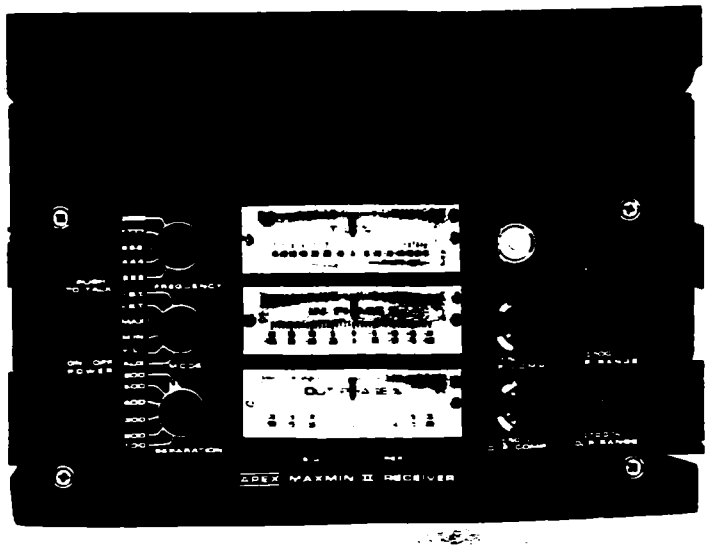
P.O. Box 818, Uxbridge
Ontario, Canada L0C 1K0

Telephones: 416-640-6102
416-852-5875

Fax: 416-852-9688

Telex: 06-966625 APEXPARA UXB
Cables: APEXPARA TORONTO





SPECIFICATIONS :

Frequencies: 222, 444, 888, 1777 and 3555 Hz.

Modes of Operation:
- MAX: Transmitter coil plane and receiver coil plane horizontal (Max-coupled; Horizontal-loop mode). Used with refer. cable.
- MIN: Transmitter coil plane horizontal and receiver coil plane vertical (Min-coupled mode). Used with reference cable.
- V.L. : Transmitter coil plane vertical and receiver coil plane horizontal (Vertical-loop mode). Used without reference cable, in parallel lines.

Coil Separations: 25, 50, 100, 150, 200 & 250 m (MMII) or 100, 200, 300, 400, 600 and 800 ft. (MMIIF).
Coil separations in V.L. mode not restricted to fixed values.

Parameters Read:
- In-Phase and Quadrature components of the secondary field in MAX and MIN modes.
- Tilt-angle of the total field in V.L. mode.

Readouts:
- Automatic, direct readout on 90 mm (3.5") edgewise meters in MAX and MIN modes. No nulling or compensation necessary.
- Tilt angle and null in 90 mm edgewise meters in V.L. mode.

Scale Ranges:
- In-Phase: ±20%, ±100% by push-button switch.
- Quadrature: ±20%, ±100% by push-button switch.
- Tilt: ±75% slope.
- Null (V.L.): Sensitivity adjustable by separation switch.

Readability: In-Phase and Quadrature: 0.25 % to 0.5 % ; Tilt: 1 %.

Repeatability: ±0.25% to ±1% normally, depending on conditions, frequencies and coil separation used.

Transmitter Output:
- 222 Hz : 220 Atm^2
- 444 Hz : 200 Atm^2
- 888 Hz : 120 Atm^2
- 1777 Hz : 60 Atm^2
- 3555 Hz : 30 Atm^2

Receiver Batteries: 9V trans. radio type batteries (4). Life: approx. 35 hrs. continuous duty (alkaline, 0.5 Ah), less in cold weather.

Transmitter Batteries: 12V 6 Ah Gel-type rechargeable battery. (Charger supplied).

Reference Cable: Light weight 2-conductor teflon cable for minimum friction. Unshielded. All reference cables optional at extra cost. Please specify.

Voice Link: Built-in intercom system for voice communication between receiver and transmitter operators in MAX and MIN modes, via reference cable.

Indicator Lights: Built-in signal and reference warning lights to indicate erroneous readings.

Temperature Range: -40°C to +60°C (-40°F to +140°F).

Receiver Weight: 6kg (13 lbs.)

Transmitter Weight: 13kg (29 lbs.)

Shipping Weight: Typically 60kg (135 lbs.), depending on quantities of reference cable and batteries included. Shipped in two field/shipping cases.

Specifications subject to change without notification.

APEX PARAMETRICS LIMITED
BOX 818, R.R. NO.1, UXBRIDGE, ONTARIO, CANADA L0C 1K0

Phone: (416) 640-6102 852-5875 Cables: APEXPARA TORONTO Telex: 06-966625 APEXPARA UXB

LINECUTTING EXPENCES

Linecutting Jim Reed

Date		Hr
May	13	8
	14	6
	18	7
	21	8
	24	8
	25	8
	26	8
	27	7
	28	8
	30	8
June	2	8
	3	8
	8	8
	9	8
	10	8
	11	5
	15	8
	17	7
	18	5
	20	4
	21	7
	22	7
	23	8
	24	7
	25	8
	27	7
	28	8
	30	3
July	1	4
	2	4
	6	8
	7	4
	8	8
	9	6
	10	7
	11	6
	12	6
	13	6
	14	6

continued

	15	6
	22	4
	25	8
	26	8
	29	6
Total	297 hr = 37.10 day = $3710.00	
	265 hr = 33.10 day = $3310.00 linecutting	
	32 hr = 4 days = $ 400.00 prosecting	

Linecutting Jean Reed

Date	Hr
June 3	8
10	8
22	7
Total	23 Hr 2.875 day @ 100.00/day = $287.50

Linecutting Ruth Reed

Date	Hr
June 3	8
10	8
22	7
Total	23 Hr 2.875 day @ 100.00/day = $287.50

Nat Reed

Date	Hr
July 2	4
July 8	4
Total	8 hr = 1 day @ $100/day = $100.00

Linecutting Expences

Jim Reed	265 hr =	33.1	day @ $100/day =	$3310.00
Jean Reed	23 hr =	2.875	day @ $100/day =	$ 287.50
Ruth Reed	23 hr =	2.875	day @ $100/day =	$ 287.50
Nat Reed	8 hr =	1	day @ $100/day =	$ 100.00
TOTAL				$3985.00

Prospecting Expences

Jim Reed	32 hr =	4 days	@ $100/day =	$ 400.00

INVOICE FOR MaxMin EM SURVEY OF JAMES REED CLAIM GROUP IN OTTO AND EBY TOWNSHIPS

Dates of Survey August 10, 11, 12, 1994
December 31, 1994
January 1, 1995
Dates of report preparation January 6, 7, 8, 1994

LINE	COIL SEPARATION (m)	TRAVERSE LENGTH(m)	MEASURED TOPOGRAPHY	
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37+00	200	625	625	(440,880,3520 Hz)
38+00	200	700	700	(440,880,3520 Hz)
38+50	100	500	500	(3555 Hz)
39+00	100	675	675	(440,1760, 7040 Hz)
39+50	100	600	600	(3555 Hz)
40+00	100	625	625	(440,1760, 7040 Hz)
40+00	50	325	325	(440,1760, 7040 Hz)
40+50	100	550	550	(3555 Hz)
41+00	100	500	500	(440,1760, 7040 Hz)
41+50	100	900	900	(3555 Hz)
42+00	100	400	400	(440,1760, 7040 Hz)
42+50	100	875	875	(440,1760, 7040 Hz)
43+00	100	925	925	(3555 Hz)
43+50	100	875	875	(440,1760, 7040 Hz)
Total		10625	106250	

First frequency 10.625 km @ $200/km = $2125.00
2 additional frequencies: each at @ $25/km
2 X $25/km X 7.15 km = $ 357.00
Totography measurement
$25 X 10.625 km = $ 265.00
TOTAL BALANCE OWING $2747.00

Douglas Robinson

Douglas Robinson, P. Eng.
January 8, 1998

Ministry of Northern Development and Mines

Ontario

GAO

Report of Work C
After Recording C

Mining Act

42A01SE0028 2.15784 EBY

900

Personal information collected on this form is obtained under the authority of the Mining Act. This information will be used for correspondence. Questions about this collection should be directed to the Provincial Manager, Mining Lands, Ministry of Northern Development and Mines, Fourth Floor, 159 Cedar Street, Sudbury, Ontario, P3E 6A5, telephone (705) 670-7284.

2.15784

Instructions:
- Please type or print and submit in duplicate.
- Refer to the Mining Act and Regulations for requirements of filing assessment work or consult the Mining Recorder.
- A separate copy of this form must be completed for each Work Group.
- Technical reports and maps must accompany this form in duplicate.
- A sketch, showing the claims the work is assigned to, must accompany this form.

~~Address Attached~~

Recorded Holder(s) *	Client No. *
James D. Reed, ~~E.L.Reed, N. E.Reed, C.L. Reed~~	186441
Address	**Telephone No.**
RR#3, Site 3, Box 2, Swastika, Ontario P0K-1T0	705-642-3573
Mining Division / **Township/Area**	**M or G Plan No.**
Larder Lake / Eby, & Otto	M345, M379
Dates Work Performed From: May 13, 1994 To: January 8, 1995	

Work Performed (Check One Work Group Only)

	Work Group	Type
	Geotechnical Survey	linecutting, Max Min EM{3 Frequency} Terrain Measurement
	Physical Work, Including Drilling	
	Rehabilitation	
	Other Authorized Work	
	Assays	
	Assignment from Reserve	

RECEIVED
JAN 12 1995
MINING LANDS BRANCH

Total Assessment Work Claimed on the Attached Statement of Costs $ 5774

Note: The Minister may reject for assessment work credit all or part of the assessment work submitted if the recorded holder cannot verify expenditures claimed in the statement of costs within 30 days of a request for verification.

Persons and Survey Company Who Performed the Work (Give Name and Address of Author of Report)

Name	Address
James D. Reed (Linecutting)	RR#3 site 3, Box 2, Swastika, ONT, P0K-1T0
Report Douglas Robinson, P.Eng	Box 218 Swastika, Ontario P0K-1T0
Survey EM & Terrain Measurement Douglas Robinson, P.Eng.	Box 218 Swastika, Ontario P0K-1T0

(attach a schedule if necessary)

Certification of Beneficial Interest * See Note No. 1 on reverse side

I certify that at the time the work was performed, the claims covered in this work report were recorded in the current holder's name or held under a beneficial interest by the current recorded holder.	Date	Recorded Holder or Agent (Signature)
	January 19, 1995	Douglas Robinson

Certification of Work Report

I certify that I have a personal knowledge of the facts set forth in this Work report, having performed the work or witnessed same during and/or after its completion and annexed report is true.

Name and Address of Person Certifying

Douglas Robinson Box 218 Swastika, ONT P0K-1T0

Telephone No.	Date	Certified By (Signature)
705-642-9153	January 19, 1995	Douglas Robinson

For Office Use Only

Total Value Cr. Recorded	Date Recorded	Mining Recorder	Received Stamp
$5774.	Jan 10/95		
	Deemed Approval Date: Apr 11/95	Date Approved	
	Date Notice for Amendments Sent		

Work Report Number for Applying Reserve	Claim Number (see Note 2)	Number of Claim Units	Value of Assessment Work Done on this Claim	Value Applied to this Claim	Value Assigned from this Claim	Reserve: Work to be Claimed at a Future Date
	1187002	4	3200	5774	0	0
Lease # 106732	475258	4	2574	0	2574	0
"	475259					
"	475260					
"	475261					
Anniversary Date June 1, 1991						
64.717	HA					
This Lease Recorded in Names of	25% 27, James D. Reed	25%+25%				
	Emmalene L. Reed					
	Nathanael E Reed					
	Charles E Reed.					
	See list of co-holders included					
	Total Number of Claims		Total Value Work Done	Total Value Work Applied	Total Assigned From	Total Reserve

41 (03/91)

Credits you are claiming in this report may be cut back. In order to minimize the adverse effects of such deletions, please indicate from which claims you wish to priorize the deletion of credits. Please mark (✓) one of the following:

1. ☐ Credits are to be cut back starting with the claim listed last, working backwards.
2. ☐ Credits are to be cut back equally over all claims contained in this report of work.
3. ☐ Credits are to be cut back as priorized on the attached appendix.

In the event that you have not specified your choice of priority, option one will be implemented.

Note 1: Examples of beneficial interest are unrecorded transfers, option agreements, memorandum of agreements, etc., with respect to the mining claims.

Note 2: If work has been performed on patented or leased land, please complete the following:

I certify that the recorded holder had a beneficial interest in the patented or leased land at the time the work was performed.

Signature: Douglas Ostrum

Date: Jan 16, 1995

Ministry of Northern Development and Mines

Ontario

Ministère du Développement du Nord et des mines

Statement of Costs for Assessment Credit

État des coûts aux fins du crédit d'évaluation

Mining Act/Loi sur les mines

DOCUMENT No. 00006

Transaction No./N° de transaction W 9850

Personal information collected on this form is obtained under the authority of the Mining Act. This information will be used to maintain a record and ongoing status of the mining claim(s). Questions about this collection should be directed to the Provincial Manager, Minings Lands, Ministry of Northern Development and Mines, 4th Floor, 159 Cedar Street, Sudbury, Ontario P3E 6A5, telephone (705) 670-7264.

Les renseignements personnels contenus dans la présente formule sont recueillis en vertu de la Loi sur les mines et serviront à tenir à jour un registre des concessions minières. Adresser toute quesiton sur la collece de ces renseignements au chef provincial des terrains miniers, ministère du Développement du Nord et des Mines, 159, rue Cedar, 4e étage, Sudbury (Ontario) P3E 6A5, téléphone (705) 670-7264.

1. Direct Costs/Coûts directs

Type	Description	Amount Montant	Totals Total global
Wages Salaires	Labour Linecutting	3027	
	Field Supervision Supervision sur le terrain		3027
Contractor's and Consultant's Fees Droits de l'entrepreneur et de l'expert-conseil	Type 3 Frequency		
	EM (Maxmin)	2747	
	Terrain Measurement		2747
Supplies Used Fournitures utilisées	Type		
Equipment Rental Location de matériel	Type		
	Total Direct Costs Total des coûts directs		5774

2. Indirect Costs/Coûts indirects

** Note: When claiming Rehabilitation work Indirect costs are not allowable as assessment work.
Pour le remboursement des travaux de réhabilitation, les coûts indirects ne sont pas admissibles en tant que travaux d'évaluation.

Type	Description	Amount Montant	Totals Total global
Transportation Transport	Type		
Food and Lodging Nourriture et hébergement			
Mobilization and Demobilization Mobilisation et démobilisation			
	Sub Total of Indirect Costs Total partiel des coûts indirects		
	Amount Allowable (not greater than 20% of Direct Costs) Montant admissible (n'excédant pas 20 % des coûts directs)		
	Total Value of Assessment Credit (Total of Direct and Allowable Indirect costs) / Valeur totale du crédit d'évaluation (Total des coûts directs et indirects admissibles)		

Note: The recorded holder will be required to verify expenditures claimed in this statement of costs within 30 days of a request for verification. If verification is not made, the Minister may reject for assessment work all or part of the assessment work submitted.

Note : Le titulaire enregistré sera tenu de vérifier les dépenses demandées dans le présent état des coûts dans les 30 jours suivant une demande à cet effet. Si la vérification n'est pas effectuée, le ministre peut rejeter tout ou une partie des travaux d'évaluation présentés.

Filing Discounts

1. Work filed within two years of completion is claimed at 100% of the above Total Value of Assessment Credit.

2. Work filed three, four or five years after completion is claimed at 50% of the above Total Value of Assessment Credit. See calculations below:

Total Value of Assessment Credit	Total Assessment Claimed
x 0.50 =	

Remises pour dépôt

1. Les travaux déposés dans les deux ans suivant leur achèvement sont remboursés à 100 % de la valeur totale susmentionnée du crédit d'évaluation.

2. Les travaux déposés trois, quatre ou cinq ans après leur achèvement sont remboursés à 50 % de la valeur totale du crédit d'évaluation susmentionné. Voir les calculs ci-dessous.

Valeur totale du crédit d'évaluation	Évaluation totale demandée
x 0,50 =	

Certification Verifying Statement of Costs

I hereby certify:
That the amounts shown are as accurate as possible and these costs were incurred while conducting assessment work on the lands shown on the accompanying Report of Work form.

That as Douglas Robinson I am authorized
(Recorded Holder, Agent, Position in Company)

To make this certification

Attestation de l'état des coûts

J'atteste par la présente :
que les montants indiqués sont le plus exact possible et que ces dépenses ont été engagées pour effectuer les travaux d'évaluation sur les terrains indiqués dans la formule de rapport de travail ci-joint.

Et qu'à titre de _____ je suis autorisé
(titulaire enregistré, représentant, poste occupé dans la compagnie)

à faire cette attestation.

Signature	Date
Douglas Robinson	January 10, 1997

212 (04/91)

Nota : Dans cette formule, lorsqu'il désigne des personnes, le masculin est utilisé au sens neutre

Ontario

Ministry of Northern Development and Mines

Ministère du Développement du Nord et des Mines

Geoscience Approvals Office
933 Ramsey Lake Road
6th Floor
Sudbury, Ontario
P3E 6B5

Telephone: (705) 670-5853
Fax: (705) 670-5863

Our File: 2.15784
Transaction #W9580.00006

February 24, 1995

Mining Recorder
Ministry of Northern Development
and Mines
4 Government Road East
Kirkland Lake, Ontario
P2N 1A2

Dear Mr. Spooner:

RE: APPROVAL OF ASSESSMENT WORK ON MINING CLAIM 1187002 ET AL IN EBY TOWNSHIP.

The assessment credits for Geophysics (EM), subsection 14, of the Mining Act Regulations, as listed on the original Report of Work, have been approved as of **February 23, 1995.**

Please indicate this approval on the claim record sheets.

If you have any questions concerning this correspondence please contact Bruce Gates at 670-5856.

ORIGINAL SIGNED BY:

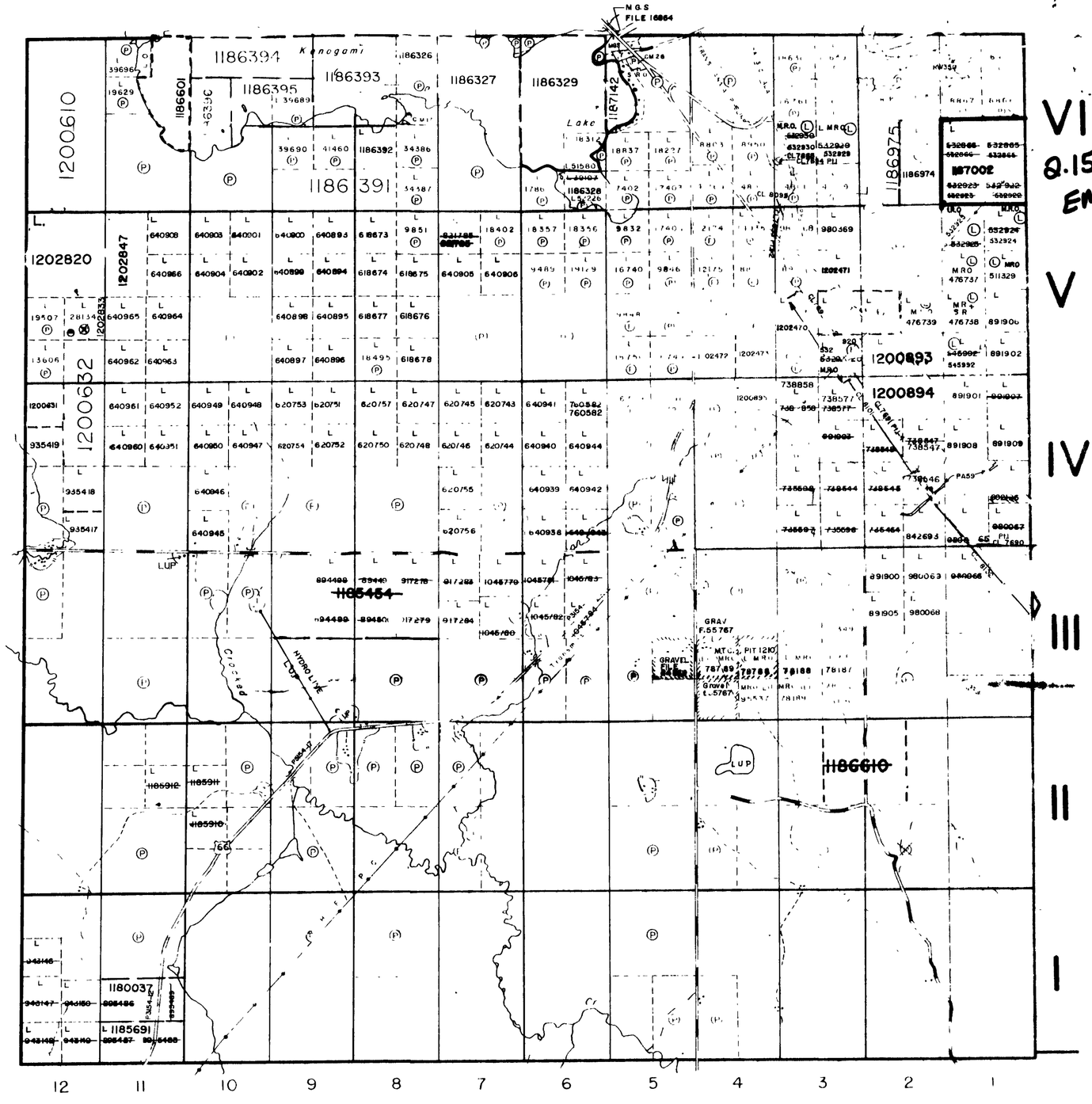
Ron C. Gashinski
Senior Manager, Mining Lands Section
Mining and Land Management Branch
Mines and Minerals Division

BIG/jl
Enclosures:

cc: Assessment Files Office
Sudbury, Ontario

Resident Geologist
Kirkland Lake, Ontario

Grenfell Twp. M.351



THE TOWNSHIP OF EBY

DISTRICT OF TIMISKAMING

LARDER LAKE MINING DIVISION

SCALE 1-INCH=40 CHAINS

VI
Q.15784
EM

LEGEND

PATENTED LAND	(P)
CROWN LAND SALE	C.S.
LEASES	(L)
LOCATED LAND	Loc.
LICENSE OF OCCUPATION	LO
MINING RIGHTS ONLY	MRO
SURFACE RIGHTS ONLY	S OR SRO
ROADS	
IMPROVED ROADS	
KINGS HIGHWAYS	
RAILWAYS	
POWER LINES	
MARSH OR MUSKEG	
MINES	
CANCELLED	

NOTES

... rivers and rivers

AREAS WITHDRAWN FROM STAKING

Surface Rights Withdrawn under Sec 36
The Mining Act R.S.O. 980, ORDER NO W-01/91/ONT
Trans Canada Pipeline Right of Way and Buffer
Zone particularly 40.25 meters or 132 ft on
either side of centre line o. right of way/

THE INFORMATION THAT APPEARS ON THIS MAP HAS BEEN COMPILED FROM VARIOUS SOURCES, AND ACCURACY IS NOT GUARANTEED THOSE WISHING TO STAKE MINING CLAIMS SHOULD CONSULT WITH THE MINING RECORDER, MINISTRY OF NORTHERN DEVELOPMENT AND MINES, FOR ADDITIONAL INFORMATION ON THE STATUS OF THE LANDS SHOWN HEREON

DATE OF ISSUE

PLAN NO. M-345

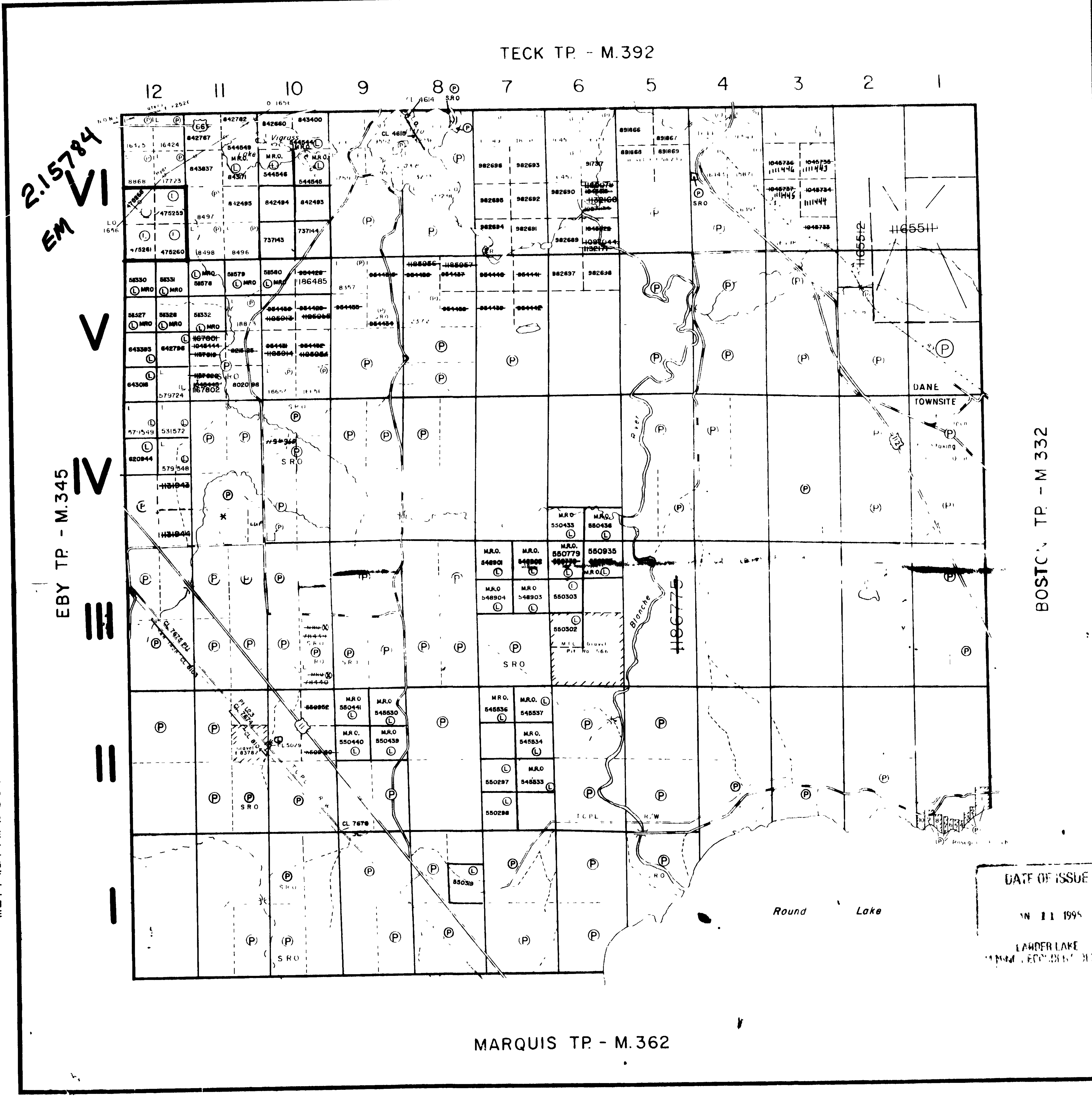
MINISTRY OF NORTHERN DEVELOPMENT AND MINES

Rec'd Jan. 25/89

TRIM LINE

42A01SE0028 2 15784 EBY

200



THE TOWNSHIP OF OTTO

DISTRICT OF TIMISKAMING

LARDER LAKE MINING DIVISION

SCALE: 1-INCH=40 CHAINS

LEGEND

PATENTED LAND	● or Ⓟ
CROWN LAND SALE	C.S.
LEASES	Ⓛ
LOCATED LAND	Loc
LICENSE OF OCCUPATION	L.O.
MINING RIGHTS ONLY	M.R.O.
SURFACE RIGHTS ONLY	S.R.O.
ROADS	
IMPROVED ROADS	
KING'S HIGHWAYS	
RAILWAYS	
POWER LINES	
MARSH OR MUSKEG	
MINES	
CANCELLED	

NOTES

400' surface rights reservation along the shores of all lakes and rivers

Ⓗ SURFACE AND MINING RIGHTS WITHDRAWN FROM STAKING SEC 36/80, W.9/86, JAN. 24, 1986 O-L26-90 NR OPENS W9/86 DEC 14, 1990

✱ APPLICATION UNDER THE PUBLIC LANDS ACT SEC. 31 (b) OF THE MINING ACT

CL 5029 DISPOSITION OF CROWN LAND

Surface Rights Withdrawn under Sec 36. The Mining Act R.S.O. 1980, ORDER NO W-O1/91/ONT (Trans Canada Pipeline Right of Way and Buffer Zone particularly 40.25 meters or 132 ft on either side of centre line of right of way)

NOTICE OF FORESTRY ACTIVITY

THIS TOWNSHIP / AREA FALLS WITHIN THE TIMISKAMING MANAGEMENT UNIT

AND MAY BE SUBJECT TO FORESTRY OPERATIONS. THE MNR UNIT FORESTER FOR THIS AREA CAN BE CONTACTED AT: P.O. BOX 129 SWASTIKA, ONT P0K 1T0 705-642-3222

DATE OF ISSUE

JAN 11 1995

LARDER LAKE MINING RECORDER'S OFFICE

PLAN NO. M-379

MINISTRY OF NORTHERN DEVELOPMENT AND MINES

CIRCULATED NOV.3/88

THE INFORMATION THAT APPEARS ON THIS MAP HAS BEEN COMPILED FROM VARIOUS SOURCES, AND ACCURACY IS NOT GUARANTEED. THOSE WISHING TO STAKE MINING CLAIMS SHOULD CONSULT WITH THE MINING RECORDER, MINISTRY OF NORTHERN DEVELOPMENT AND MINES, FOR ADDITIONAL INFORMATION ON THE STATUS OF THE LANDS SHOWN HEREON.

M.379

TWP OTTO

42A01SE0028 2.15784 EBY

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