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ONTARIO GEOLOGICAL SURVEY

Open File Report 5810

Quaternary Geology of the Shining Tree Area

By

P.W. Alcock

1991

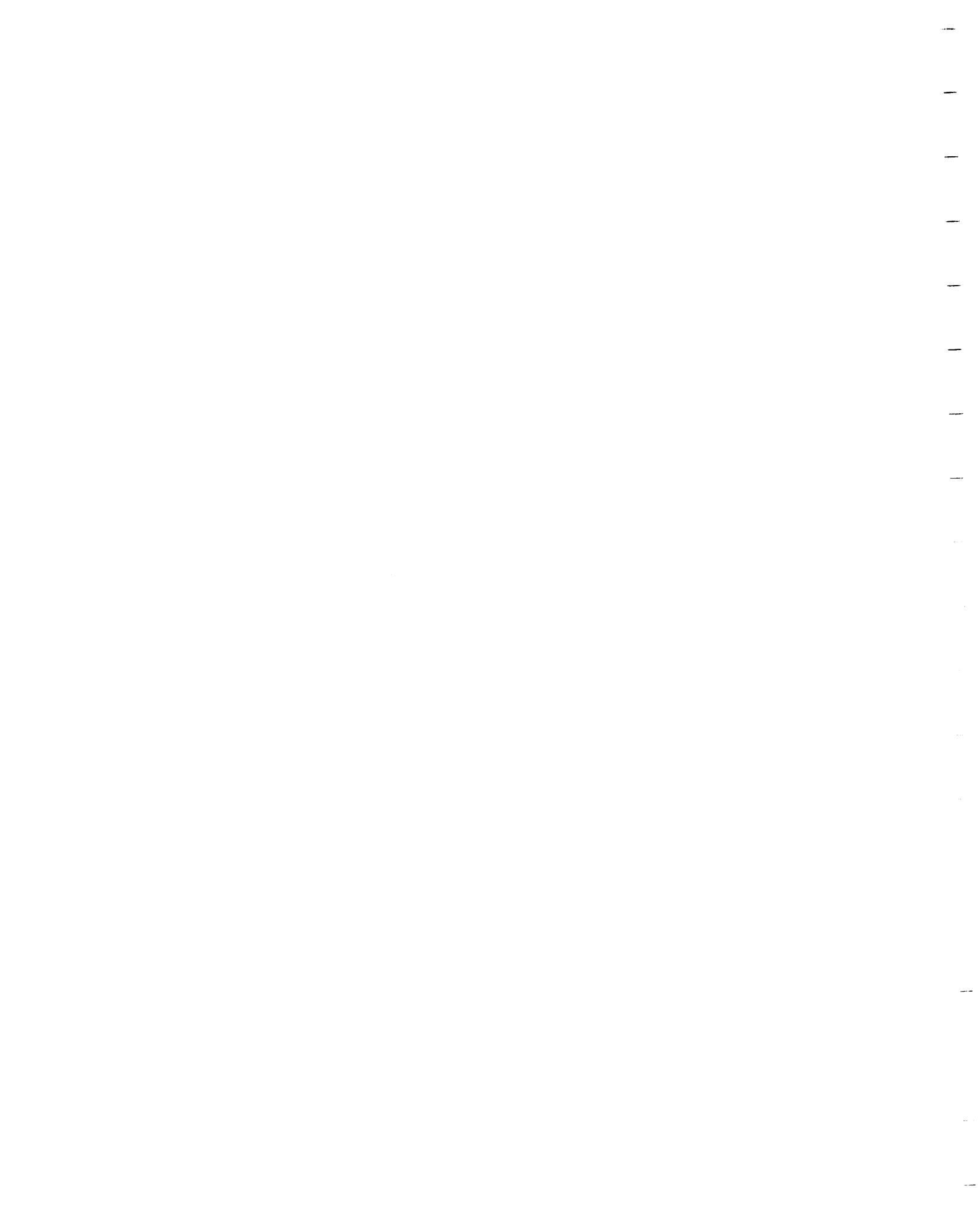
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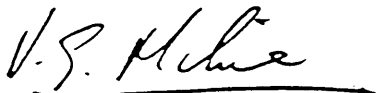
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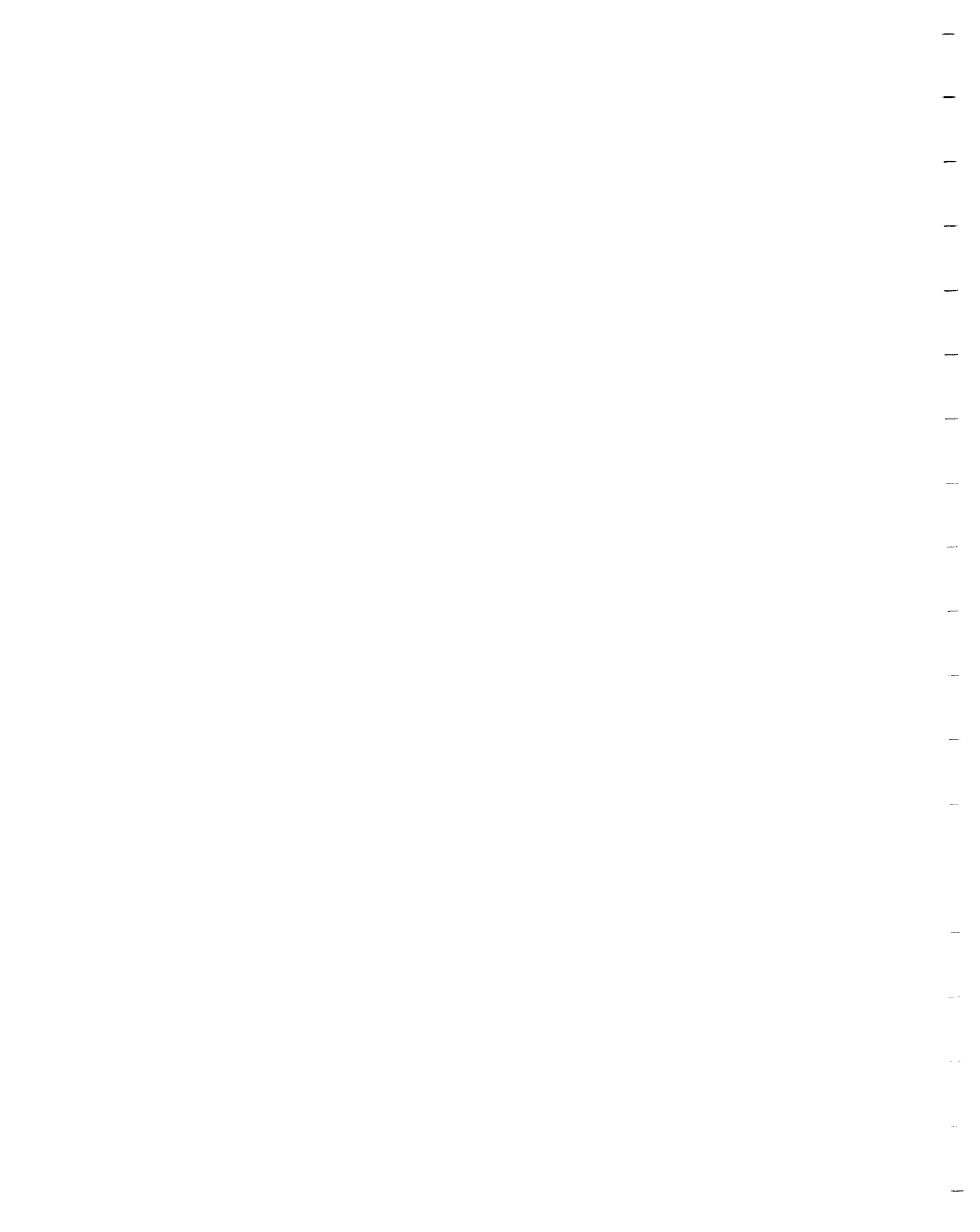
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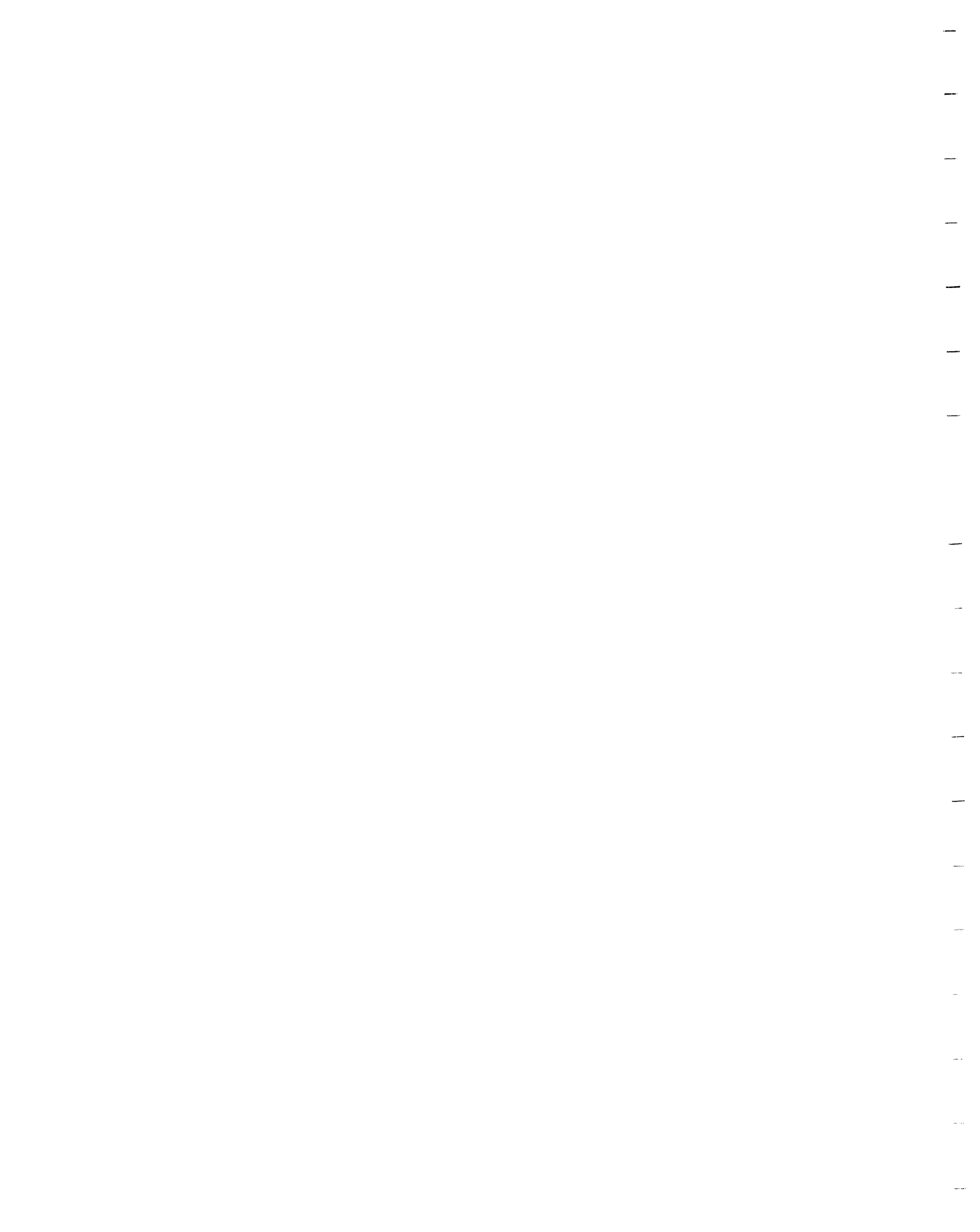


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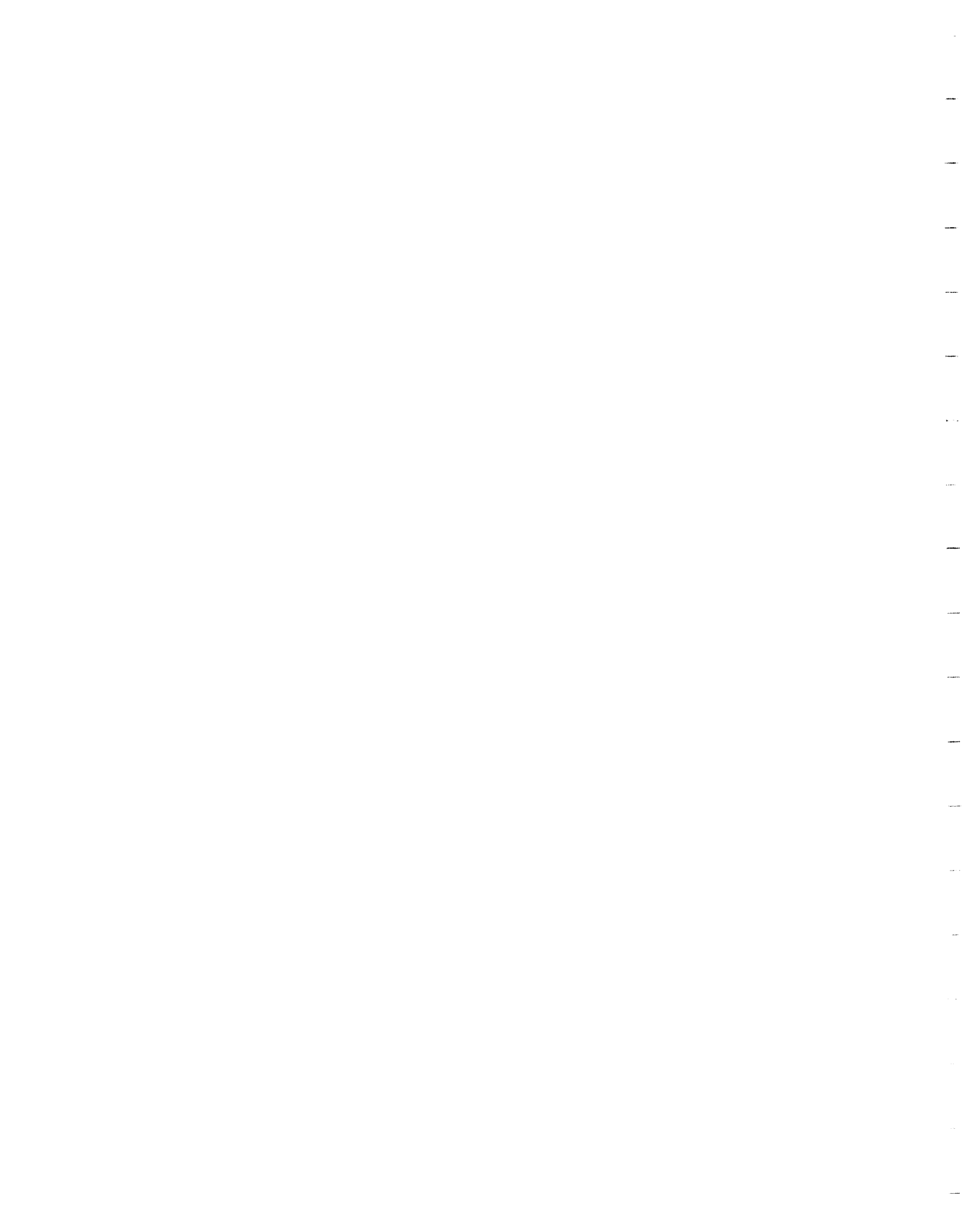
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All at scale 1:50 000



## ABSTRACT

The Quaternary deposits of the Shining Tree Area, located in Northeastern Ontario, are underlain by Archean aged metavolcanic and metasedimentary rocks of the Abitibi Greenstone Belt and Proterozoic aged sedimentary rocks of the Cobalt Group. The bedrock surface strongly controls the physiography of the study area and distribution of the Quaternary deposits.

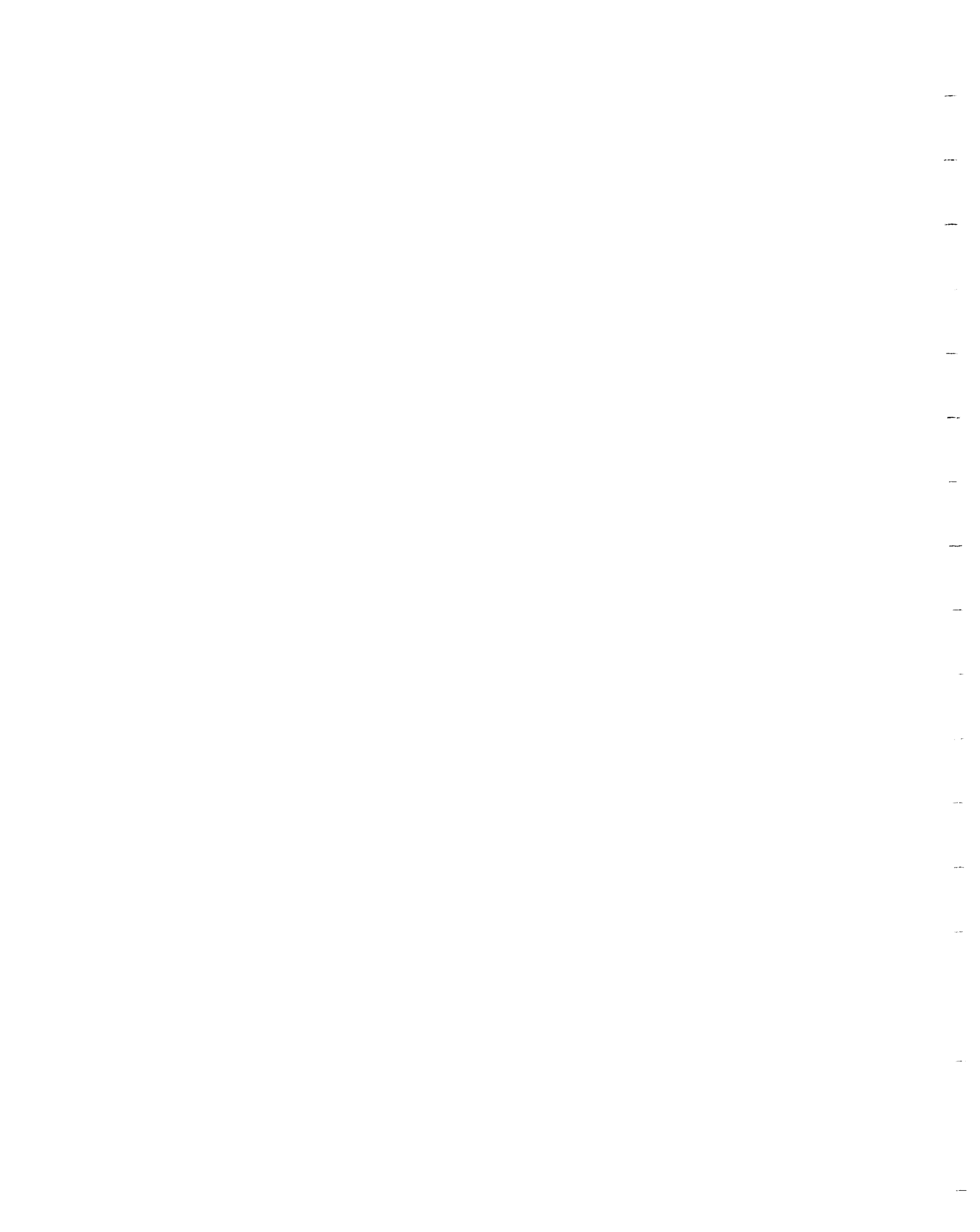
The Pleistocene sediments observed are of Late Wisconsinan age with the oldest unit being a silty sand till deposited by ice advancing southward (180 +30). At a limited number of sites evidence of an earlier southwestward advance was present. Glaciofluvial deposits within the area consist of ice-contact stratified drift, mainly in the form of esker complexes, and outwash. Outwash deposits are the dominant sediment type in valley bottoms achieving widths of several kilometres. Sandy glaciolacustrine material, deposited in short lived proglacial lakes, occupies basins and topographic lows.

Recent deposits within the Shining Tree area include eolian sand dunes and organic and alluvial deposits.

Results of till geochemical sampling within the study area indicate that the drift exploration programs boulder tracing, surface till geochemical analysis and backhoe trenching are effective exploration methods where till is at or near the surface. Both the non-magnetic heavy mineral and silt-clay fraction may be used for unweathered till. In the case of weathered till, the choice of fraction to sample is dependent on the elements being sought.



Aggregate resources in the area, associated with ice-contact stratified drift and outwash, are abundant although no evenly distributed across the area.

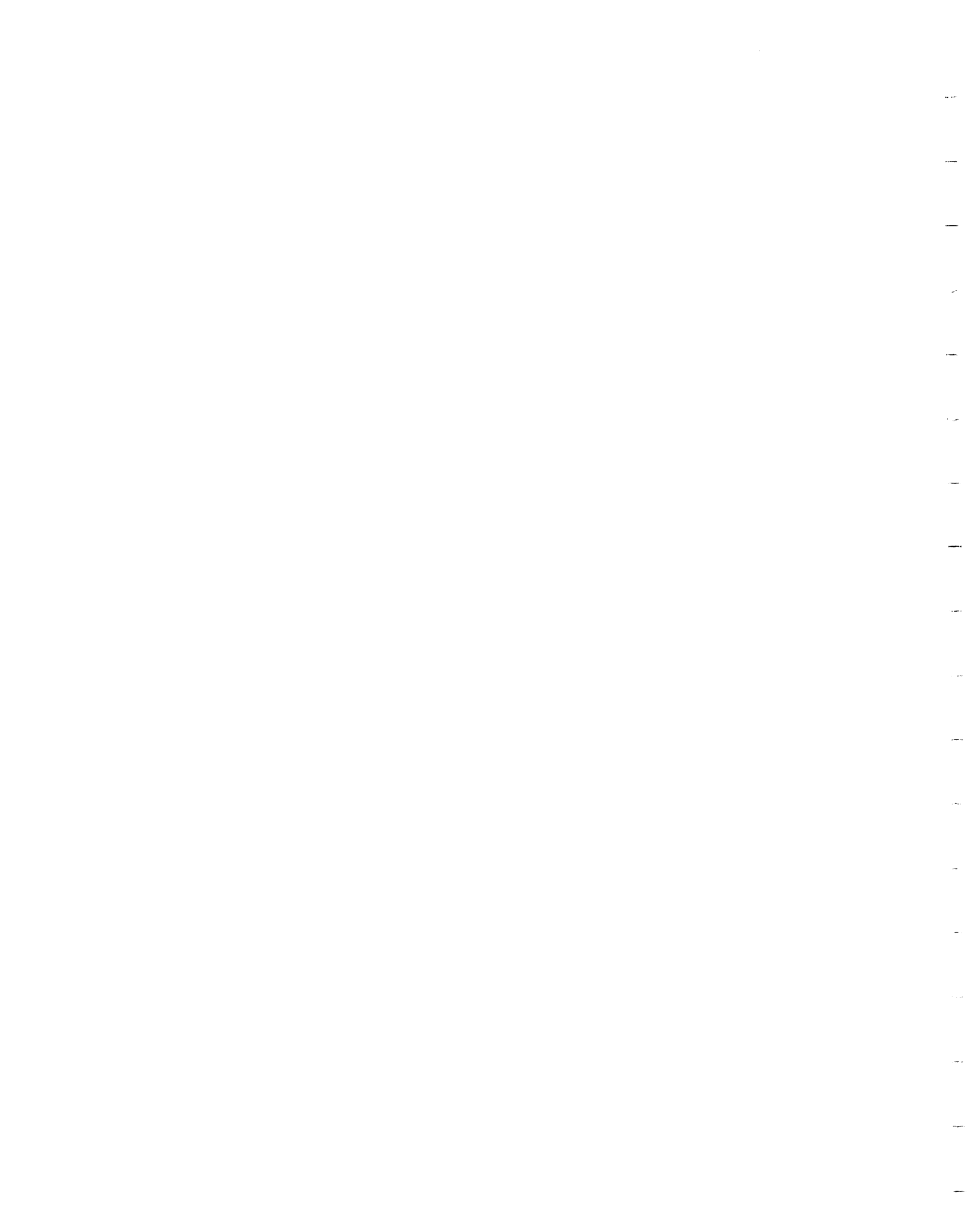


# THE QUATERNARY GEOLOGY OF THE SHINING TREE AREA

by

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Ontario Geological Survey



## **INTRODUCTION**

### **Location and Access**

The Shining Tree project area includes three 1:50,000 N.T.S. map-sheet areas (Shining Tree 41 P/11; Sinclair Lake 41 P/14; and Gowganda 41 P/10) and is located within the Provincial Districts of Sudbury and Timiskaming (Figure 1). The area is located approximately 500 km north of Toronto, 140 km north of Sudbury and 80 km south of Timmins, Ontario. It is an L-shaped area bounded by latitudes 47° 30' and 48° 00' N and longitudes 80° 30' and 81° 30' W and encompasses approximately 3000 km<sup>2</sup> of land.

The settlements within the project area include the villages of Shining Tree and Gowganda. Other communities include Gogama, Matachewan, Elk Lake and a small part of the City of Timmins. The area is served by King's Highways 144, 560 and 566 and several secondary roads including; the Grassy Lake, Bay Lumber, Beauty Lake and Wicks roads. In addition to the public access roads, logging, mining and private secondary roads are present in many parts of the project area.

### **Present Geological Survey**

The objectives of Quaternary mapping in the Shining Tree area are to: 1) determine the distribution and stratigraphy of the Quaternary sediments; and 2) expand the geological database for use in mineral exploration, forestry, and land use planning. This report summarizes information on the sedimentological, structural and geochemical properties of the Quaternary deposits and discusses their distribution, stratigraphy and

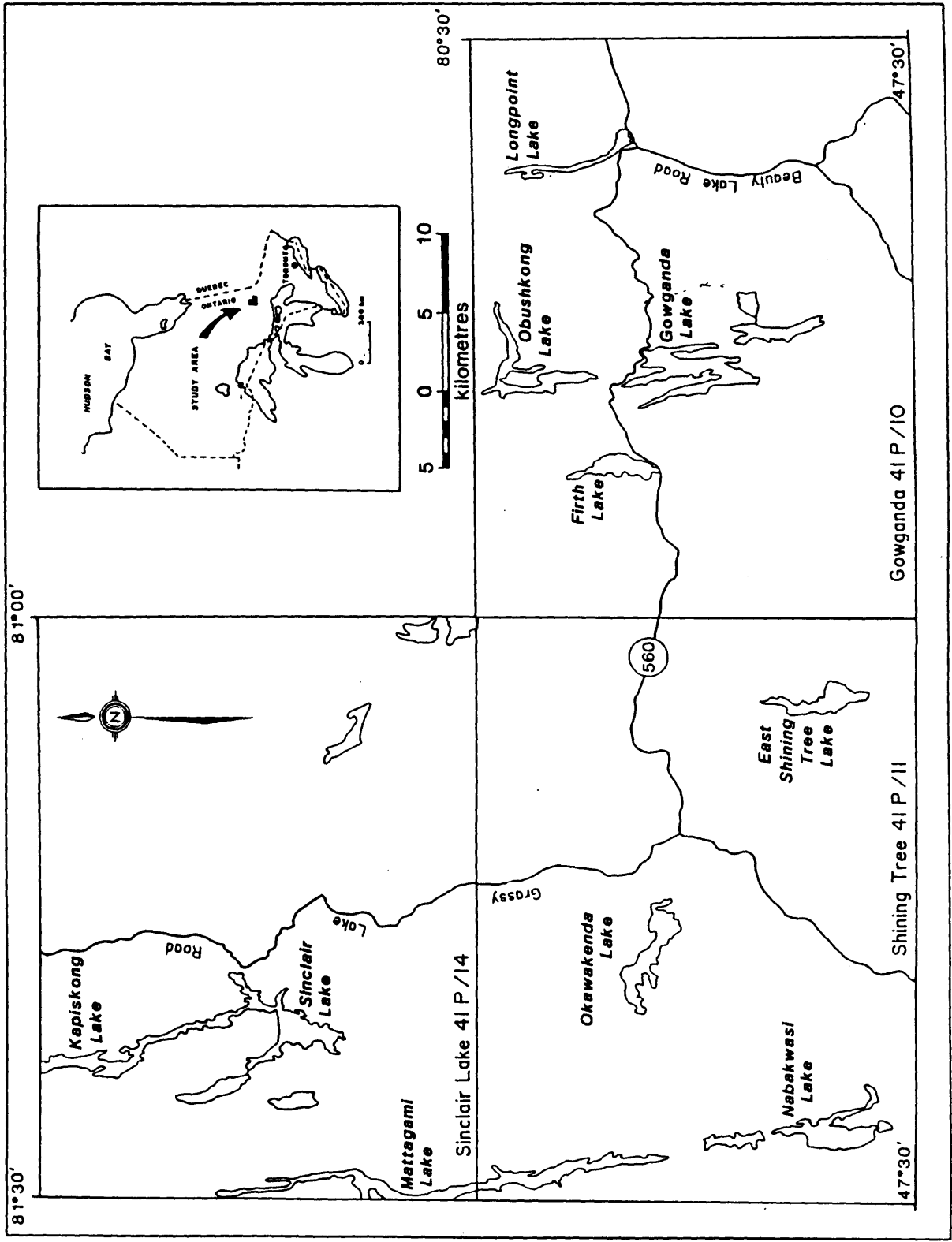


Figure 1. Location map.

depositional history. Three Quaternary geology maps have been prepared at 1:50,000 scale (Alcock and Miller, 1990a, 1990b).

Field work was conducted in the summers of 1986, 1987, 1988 and 1989. Trucks and all terrain vehicles were used to traverse highways, forestry and mining access roads, and power transmission line right-of-ways. Canoes with outboard motors were used for travel along lakes and rivers. Foot traverses were carried out in areas with no access.

The Quaternary deposits were initially examined and interpreted using air photographs at scales 1:15 840, 1:20,000 and 1:63 360 supplied by the Air Photo Library, Ontario Ministry of Natural Resources and the National Air Photo Library, Ministry of Energy, Mines and Resources, Canada. This was followed by examination of natural and man-made exposures along roads, river and lake shores, and in excavations. As much of the area lacked any exposures, hand augering and hand test pitting were used to examine and sample material down to about 1.5 m depth. A total of 32 backhoe trenches were excavated to a depth of about 3 m, in several areas in order to examine and sample deposits, usually thick till. All outcrops along traverses were examined for striations and other ice directional features. Field notes of E. V. Sado and W. A. Clarke were also used (see Sado and Clarke 1974).

The Quaternary deposits were delineated using 1:15,840 and 1:20,000 airphotos, field site observations and bedrock outcrop maps. Deposit morphology, vegetation cover, drainage characteristics, reflectivity of exposed sediments, presence of surface

boulders and bedrock outcrops, and patterns of road and borrow pit development, were used to interpret the Quaternary deposits. In remote areas, using field relationships gained from areas with ground truth were used.

The units delineated on the maps represent areas where the indicated deposit type predominates. They may also include areas of other deposit types too small or too thin (less than 1 m) to map. For example, areas of till veneer over bedrock (Map Unit 2a) may also include areas of thick till (Unit 3) and organic deposits (Unit 8) and occasional thin surface veneers of lacustrine or eolian sediment. Many contacts between map units represent an arbitrary division of the gradual transition from one deposit type to another. Areas of bedrock-drift complex (2, 2a, 2b or 2c) have covers of surficial sediment over bedrock which are often 1 m or less in thickness, with frequent outcrops. All other units represent surficial sediment or organic material at least 1 m thick. Any site specific use of the surficial deposits maps should include an orientation survey to verify the sediment types, thicknesses and distribution locally.

### **Acknowledgements**

Quaternary geological mapping and sampling of the Shining Tree map area (NTS 41 P/11) commenced in 1986 by P. Finamore, J. MacKenzie, A. Chippindale and C. Hibberd. Field mapping between 1987 and 1989 was completed by the author. Assistance in the field was provided by M. Miller, J. Aultman, V. Rammul, M. Schrader and K. O'Keefe.

The administrative and logistical assistance of the staff at the Gogama District Office and the Elk Lake Sub-office, Ontario Ministry of Natural Resources, is gratefully acknowledged. The author would like to thank Gary Naveau and the Mattagami Indian Band for their permission and co-operation in allowing access in 1987 to the Reserve lands (I.R. 71). The author would like to thank the many landowners and claimholders of the Shining Tree area who allowed access to their properties for fieldwork. Valuable discussions regarding the surficial deposits and mapping were held with staff of the Ontario Geological Survey.

### **Physiography and Drainage**

The project area lies within the Abitibi Uplands and Cobalt Plain subdivisions of the James Physiographic Region (Bostock 1970; Shilts et al. 1987). The Abitibi Upland in the project area is underlain by Archean crystalline, metavolcanic and metasedimentary bedrock. The broad, rolling surface of this upland rises southwards at a low gradient. The Cobalt Plain is underlain by generally flat-lying Proterozoic clastic sedimentary rocks with hills formed by gabbroic sills or inliers of Archean crystalline rocks. In the northeastern and eastern parts of the project area, faulting and differential erosion of the beds in the Proterozoic sedimentary rocks have produced north oriented ridges and a stepped appearance to the edge of the large outlier.

The land surface rises generally southward from elevations of less than 335 m (1100 feet) in the north to elevations in excess of 580 m (1900 feet) in the south. The Sinclair Lake map area is generally a low relief lowland area while the Shining Tree map area is of higher local relief and higher elevation. The Gowganda map area has the

highest and most rugged topography, with ridges and hills standing tens to hundreds of metres above the surrounding land surface. Local relief commonly ranges up to 50 m (165 feet) but steep rises in excess of 200 m do occur. Steep bedrock-controlled slopes occur near the boundaries of Proterozoic sedimentary rock areas.

The highest areas include hills in excess of 457 m (1500 feet) near Elephant Head Lake in Miramachi Township, in excess of 492 m (1600 feet) near Upper Grassy Lake in Natal Township and in excess of 580 m (1900 feet) east of Wallis Creek in Roadhouse Township. The topographic highs are generally underlain by Archean metavolcanic and felsic intrusive bedrock and diabase dikes in the Shining Tree and Sinclair Lake map areas, while in the Gowganda map area, the highs are formed of resistant ridges of Nipissing Diabase, Gowganda Formation conglomerate and Lorrain Formation sandstone. Most hills and ridges are glacially streamlined to some extent.

Valleys, which were important drainage route ways during deglaciation, are often underlain by major fault zones. In several locations, fault zones have been preferentially excavated by fluvial and glacial erosion, producing linear depressions. Ice-contact stratified drift deposits form local topographic highs.

The study area straddles the Hudson Bay-Great Lakes drainage divide which passes roughly northward through the Shining Tree map area and through the southeastern corner of the Sinclair Lake map area. The western parts of the Shining Tree and Sinclair Lake map areas drain westward via the Nabakwasi River, Opikinimika River, Claw Creek, Burrows Creek and Hassard Creek, into Mattagami Lake which in

turn drains northward into the Mattagami River. Much of the central and eastern parts of the Sinclair Lake area drain northward by the Grassy River. The central and eastern parts of the Shining Tree area drain southward via the West Montreal River. Drainage in the Gowganda area is mainly northward by the West Montreal and Montreal Rivers and eastward by the Bear River. Most of the creeks and rivers have local base level controlled by bedrock sills. Little incision has occurred, resulting in few natural bank exposures of the Quaternary sediments.

In general, the lowland areas underlain by fine sand and silt of glaciolacustrine and eolian origin have poor drainage while the highland areas, mantled by sandy till, are somewhat better drained.

### **Drift Thickness and Bedrock Topography**

Only in the major valleys and in some of the major areas of ice-contact deposits does the bedrock topography become subdued beneath the cover of Quaternary sediments. Drift thickness commonly ranges from less than 1 m to about 10 m over areas mapped as bedrock–drift complex. Thicknesses of more than 50 m are present in some of the areas of glaciofluvial ice-contact and outwash deposits and along major valleys infilled with glaciolacustrine deposits.

### **Previous Work**

Previous reconnaissance Quaternary geology and engineering and terrain geology studies in the project area were completed by Boissonneau (1965, 1968), Roed (1979) and Roed and Hallett (1979a, 1979b). Quaternary geological mapping of parts of the project

area was carried out by Sado and Clarke (1974). Closs and Sado (1982) undertook detailed bedrock and overburden geochemical investigations in vicinity of base metal occurrences in the Midlothian Lake and Natal Lake areas. Aultman (1988) completed a study of till sedimentology and structure and investigated the nature of gold dispersal down-ice of known gold occurrences in the Shining Tree area. The surficial deposits of the New Liskeard and Englehart areas, east of the project area, were mapped by Morton et al. (1979) and King and Morton (1979) respectively.

## PRECAMBRIAN GEOLOGY

The project area lies within the west-central part of the Abitibi Greenstone Belt and the western part of the Cobalt Plate in the Superior Province of the Canadian Shield (McGlynn 1970). The regional bedrock geology has been compiled by Pyke et al. (1977) and MERQ-OGS (1987). A generalized geology map for the study area is presented as Figure 2.

Halliday, Midlothian, Moher, Semple and Hutt townships in the Sinclair Lake map area have been mapped by Bright (1970, 1984). Carter mapped all of the townships in the Shining Tree map area, with the exception of those included parts of Togo, Brunswick and Londonderry townships (Carter 1989). The bedrock geology of the Gowganda map area has been mapped by several workers. Chown, Lawson, Mickle and Roadhouse townships were mapped by MacKean (1968); Leith, Charters and Corkill townships by McIlwaine (1971); Van Hise, Milner, Haultain and Nichol townships by McIlwaine (1978); and Wallis Township by Card et al. (1973).

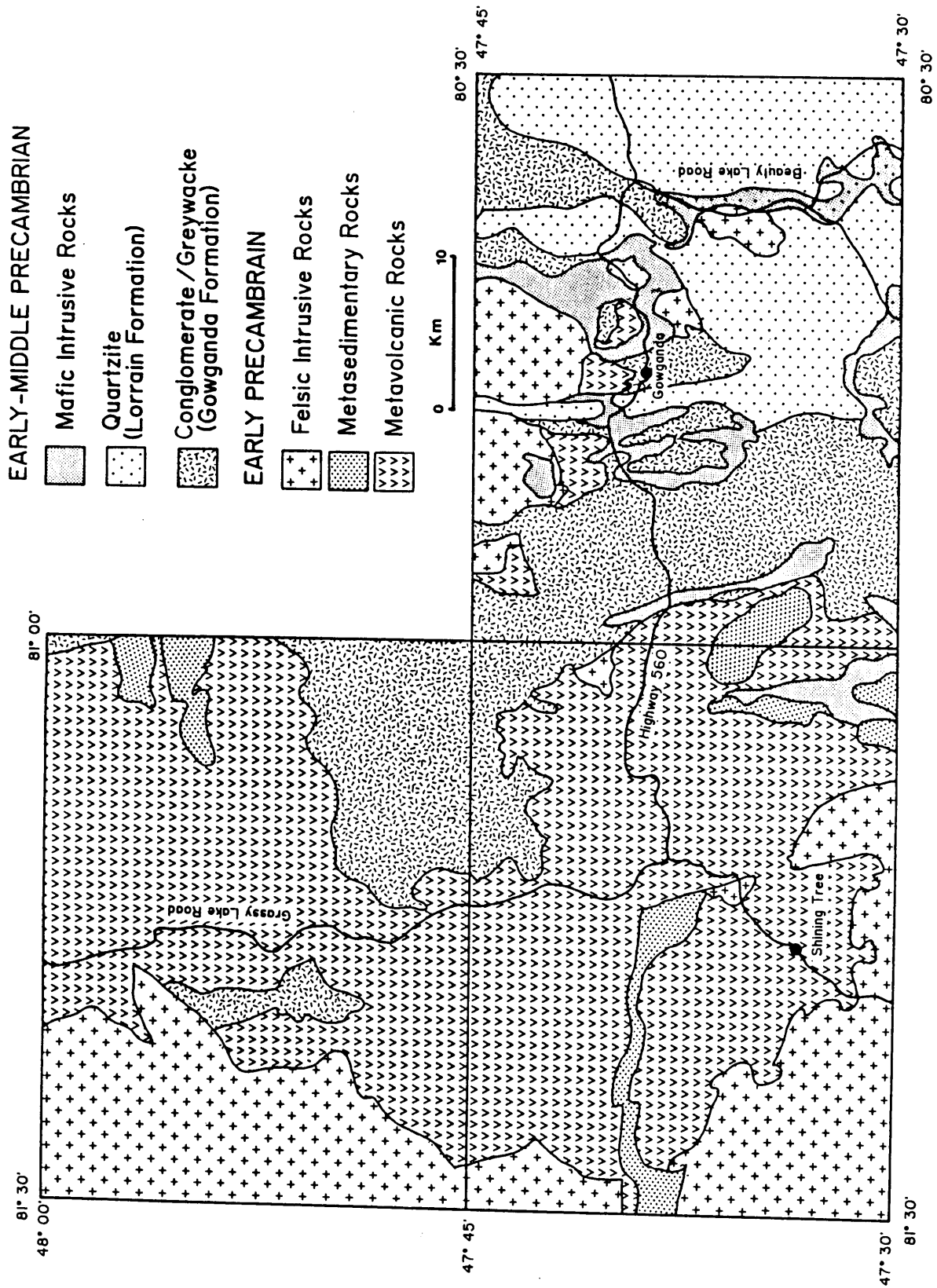


Figure 2. Generalized bedrock geology map.

In the Sinclair Lake map area, Archean rocks consist of a metavolcanic sequence with subordinate units of iron formation and metasedimentary rocks. Mafic and ultramafic sills and sill complexes intrude the metavolcanic sequence. During later regional folding, the northwestern portion of this map area was intruded by a granitic pluton. Late stage porphyritic monzonite, granodiorite and syenite stocks also intruded the metavolcanic rock succession.

In the Shining Tree area, Archean rocks comprise a felsic to mafic metavolcanic and metasedimentary rock sequence which was intruded by mafic and felsic plutonic rocks and diabase dikes.

In the Gowganda area, Archean felsic to mafic metavolcanic and metasedimentary rocks occur as inliers in younger Proterozoic sedimentary and mafic igneous rocks. The metavolcanic rocks were intruded by dunite bodies, felsic intrusive plutons and Matachewan-type diabase dikes.

After a period of erosion and tectonic activity, Cobalt Group sedimentary rocks were deposited over the Archean rocks during Proterozoic time. The basal formation of the Cobalt Group is the Gowganda Formation, consisting of two members, the Coleman Member and overlying Firstbrook Member. The Coleman Member consists of arenites, greywackes and paraconglomerates while the Firstbrook Member consists of laminated argillites. Overlying the Gowganda Formation are feldspathic to quartz arenites of the Lorrain Formation. Both the Gowganda and Lorrain Formations are relatively flat-lying throughout the study area and cover the Archean metavol-

canic-metasedimentary rocks in the eastern portions of the Shining Tree and Sinclair Lake map areas and most of the Gowganda map area.

A number of dikes and sills of Nipissing diabase intruded the earlier metavolcanic and Cobalt Group sedimentary rocks. Northeast (Abitibi) and northwest (Sudbury) trending Proterozoic diabase dike swarms cut the previously emplaced units.

The mineral potential of the area has been evaluated by Springer (1977). The zones of high mineral potential, as determined from the distributions of known deposits, coincide with areas of bedrock-drift complex. Certain zones of medium mineral potential coincide with thicker surficial deposits of glaciofluvial ice-contact and outwash sediments and glaciolacustrine sediments. Areas underlain by Gowganda and Lorrain Formation bedrock are of medium to low mineral potential. Over the area, approximately 10 to 30% of the bedrock is exposed, although the percentage is much lower in areas of metavolcanic and metasedimentary bedrock in the Sinclair Lake map area.

Deposits and occurrences of silver, gold, bismuth, cobalt, copper, iron, molybdenum, nickel, lead, zinc, barite and asbestos occur in the project area (Bright 1970, 1984; Carter 1989; MacKean, 1968; McIlwaine 1971, 1978).

The geology, petrography and whole rock geochemistry of the silver deposits in the Gowganda area were reviewed and studied by Andrews et al. (1986). The paleo-placer gold potential of the Lorrain Formation in the Gowganda area was evaluated by Rice (1986). Geological Data Inventory Folios, published by the Ministry

of Northern Development and Mines, are available for many of the townships in the project area.

## **QUATERNARY GEOLOGY**

### **Glacial Deposits and Features**

The unconsolidated deposits exposed at surface were probably deposited during the Late Wisconsinan and subsequent postglacial period. The surficial deposits and their constituent materials, diagnostic landforms and inferred depositional environments are summarized in Table I and are discussed below in greater detail.

The distribution of deposits is strongly topographically controlled, with till predominating at the highest elevations, glaciofluvial ice-contact and outwash deposits present in valleys oriented northward. Glaciolacustrine and organic deposits occupy many of the topographic lows with restricted drainage.

### **Ice Directional Features**

The last dominant ice movement over the region was towards 180 30 ° as indicated by glacial striations, grooves, roches moutonnées and crag and tail features (Figure 3, Photo 1), till fabrics (Figure 4); and dispersion trends of bedrock and mineral indicators.

The bedrock surface commonly shows evidence of erosion by ice. Stoss sides of bedrock surfaces are usually glacially smoothed and striated; lee sides are smooth to

**Table 1. Surficial deposits**

| Surficial Sediment Unit                              | Map Unit | Material  | Landform  | Depositional Environment  |
|--|----------|---|---|---|
| <b>RECENT</b>  |          |   |   |   |
| Man-emplaced   | 10       | Fine sand and silt, broken rock, municipal and wood waste                     | Taings ponds, rock waste dumps, landfill sites                            | Human activity  |
| Modern Alluvium                                      | 9        | Silt, sand, gravel, minor organics  | Point and channel bars, floodplains                                       | Channels, floodplains   |
| Organic deposits                                     | 8        | Peat, muck and marl   | Surficial blanket   | Wet, poorly drained lows  |
| Eolian   | 7        | Silt and fine to medium sand  | Dunes, surficial blanket  | Subareial, strong winds, no vegetation cover                                |
| <b>PLEISTOCENE</b>                                   |          |   |   |   |
| Glacio-lacustrine (LK)                               | 6        | Massive, laminated silt and clay, fine to coarse sand, pebbly sand and gravel | Low relief plain, offshore bars, beaches, deltas                          | Lake centre and near-shore locations, proglacial ponds, beaches             |
| Glaciofluvial Outwash (GF)                           | 5        | Silty fine sand to boulder gravel   | Undulating blankets, raised kettled terraces, fans                        | Subaerial outwash fans and terraces, minor channel fill                     |
| Ice-contact Stratified Drift (ICSD)                  | 4        | Pebbly to bouldery sand and gravel, minor silt and till                       | Eskers, kames crevasse fillings, moraines, kame terraces, subaqueous fans | Englacial and immediately proglacial, subaqueous and subaerial environments |
| Till (thick: >1 m in thickness on average)           | 3        | sand to silt till with granule to boulder-sized clasts                        | Undulating sheets and hummocks  | Sub-, supra- and proglacial environments                                    |
| Bedrock Drift Complex                                |          |   |   |   |
| a) thin till over bedrock                            | 2a       | As for till   | Patchy venneer, hummocky, bedrock controlled                              | As above, plus possible later water or coluvial reworking                   |
| b) ICSD of GF over bedrock                           | 2b       | As for ICSF or GF   | "   | "   |
| c) Glaciolacustrine or eolian sediments over bedrock | 2c       | As for LK or Eolian   | "   | "   |
| Bedrock  | 1        | Bedrock   | Bare to 50% drift-covered bedrock knobs                                   | Often meltwater or wave-washed  |

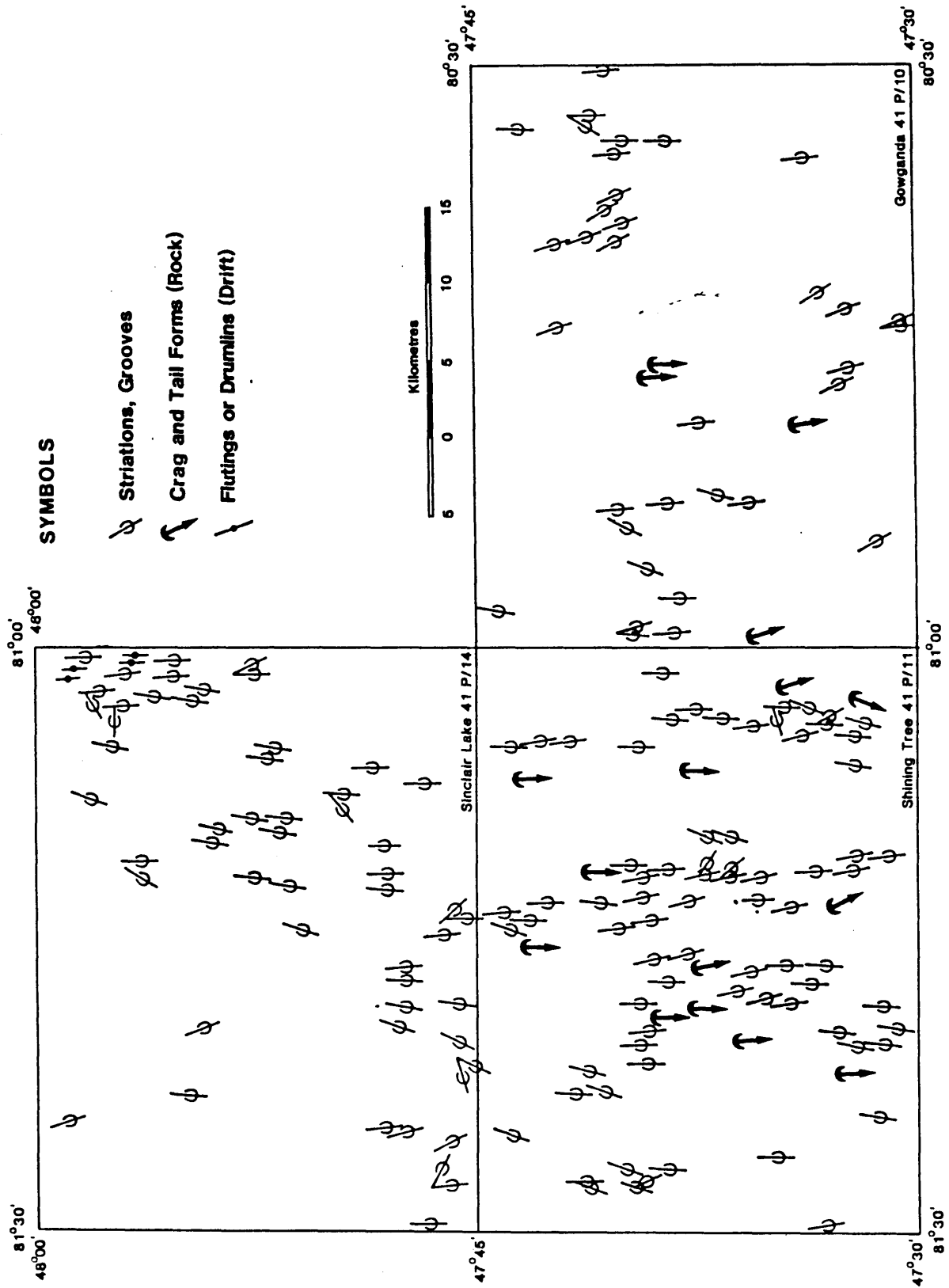
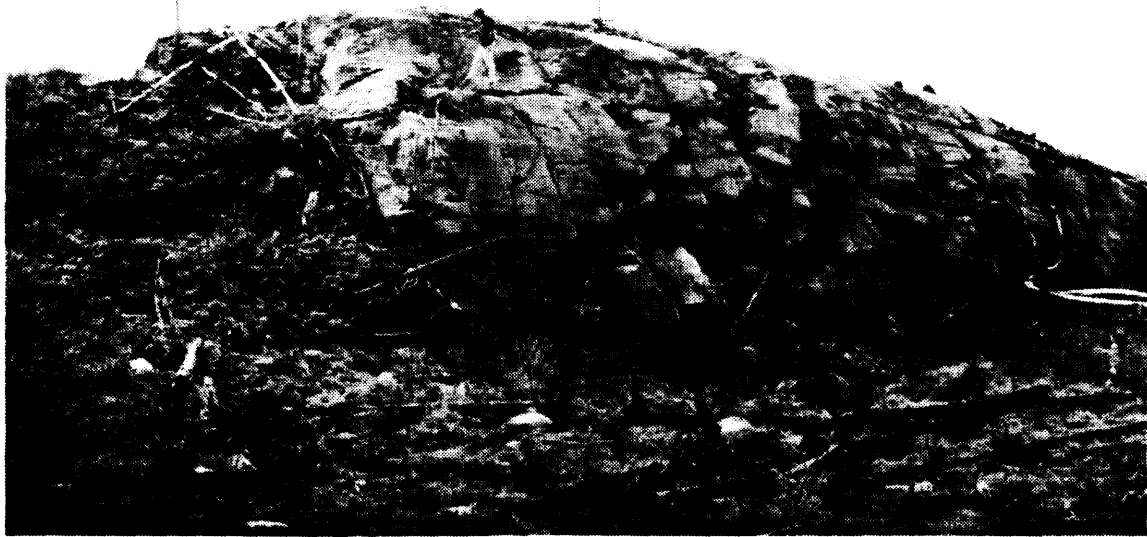


Figure 3. Ice directional indicator map.



**Photo 1.** Roche moutoneé indicating southerly ice-flow.

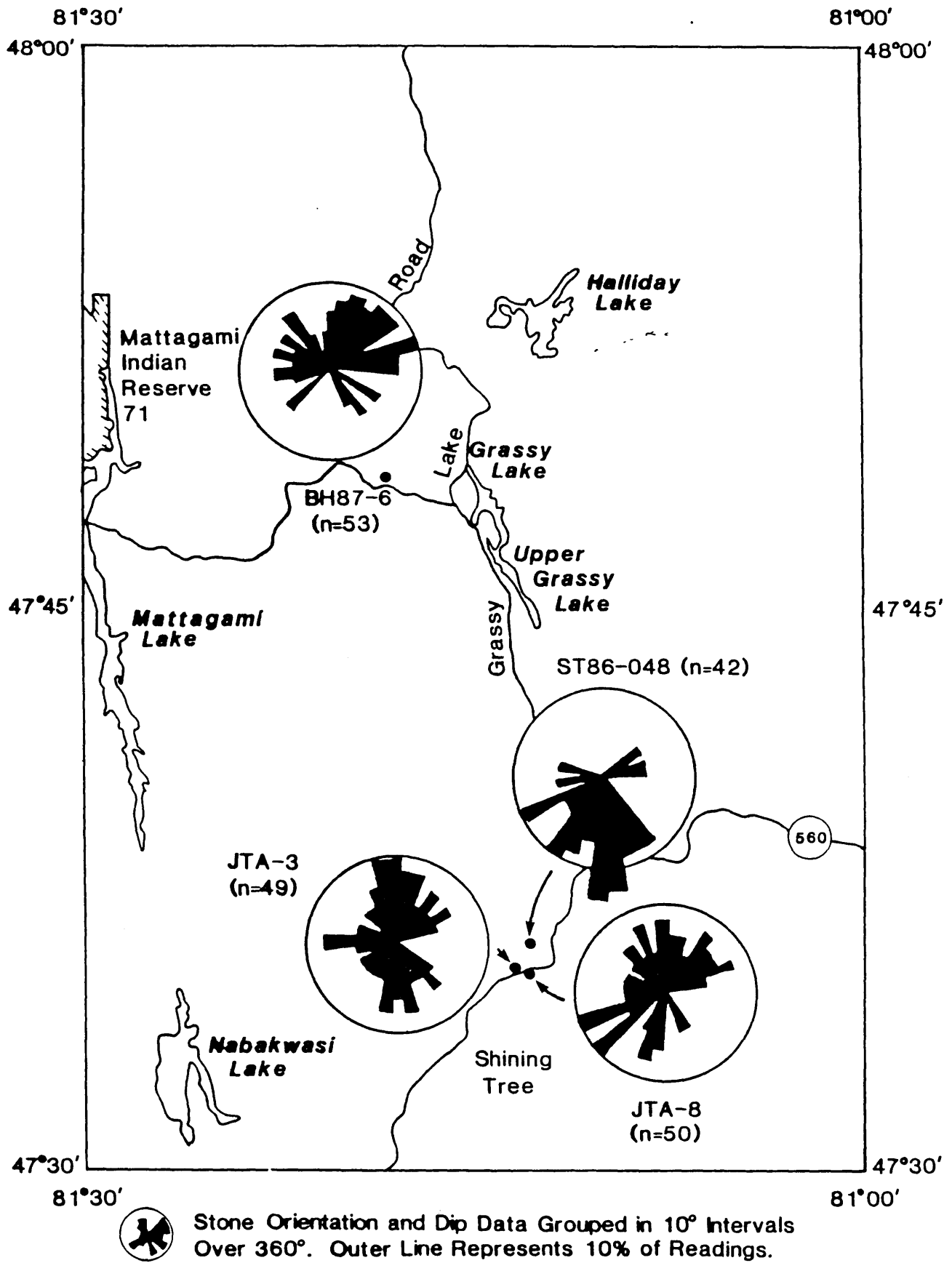


Figure 4. Till fabric diagrams.

jagged. Large exposures of bedrock commonly display whaleback or roche moutonnée forms. Ice flow was influenced by the rugged local bedrock topography.

Minor late-glacial shifts in ice direction due to the bedrock topography are indicated at a few sites, such as along Highway 560 east of Shining Tree, where fine 160° to 180° striations cross-cut an earlier set of well developed 140° to 160° striations. No areally consistent cross-cutting relationships were observed. Sites of cross-cutting glacial striae generally occur on the relatively soft, fine-grained metavolcanic and metasedimentary bedrock in the area (Photo 2). These rock types allow better formation and preservation of striations and grooves than the harder, coarsegrained granitic and gneissic bedrock in the region.

Boissonneau (1968) suggested that the cross-cutting striations found in the Shining Tree area indicated local ice readvances. It is considered here, however, that the presence of such cross-cutting striations is a function of the irregular local bedrock topography, which locally deflected the direction of the thinning ice sheet.

The clast lithological and heavy mineral composition of the till indicate southward ice flow and dispersal of rock debris and minerals. This is discussed in greater detail in the following sections on till composition.

Evidence for an earlier southwestward ice advance was occasionally observed on protected surfaces of large exposures of unweathered bedrock. On several roches moutonnées in the Shining Tree and Sinclair Lake map areas, striations, facets or



**Photo 2.** Striated outcrop with a set of  $182^\circ$  striations (pens at upper left) crosscutting a set of  $147^\circ$  striations (pens at lower right).

remnants of large grooves trending to the southwest are preserved on the lee (southern) sides. Southwesterly-oriented striations or grooves are crossed by southerly-oriented striations on several outcrops (Figure 3). This evidence supports the proposal for an early regional ice advance to the southwest, probably during Wisconsin time, coincident with the advance documented by Veillette (1986a) in the Timmins, Matheson and Lake Timiskaming areas to the north and east of the project area.

No clear evidence of earlier ice flows was found in the Gowganda map area. To the south of the Gowganda map area, however, Card et al. (1973) recorded southwesterly-oriented striations in the area southeast of Lady Evelyn Lake. These are crosscut by later southerly-oriented striations.

Although striations and facets from an earlier ice advance are present, pervasive abrasion and plucking of the bedrock surface by the latest southerly ice advance has removed most evidence of the earlier advance.

### **Bedrock and Bedrock-Drift Complex**

Where less than 50% of the land surface is covered by overburden, the surficial unit has been mapped as bedrock (Map Unit 1). In the Shining Tree and Sinclair Lake map areas, patches of bare bedrock are generally widely dispersed, with larger areas located near Claw Lake and Upper Grassy Lake. At these locations, postglacial lake wave washing has removed the Quaternary sediment cover from the bedrock knobs that were located in the foreshore area. In the Gowganda map area, large tracts of essentially bare bedrock occur on ridges and other topographic highs, near eskers and in meltwater

channels. It is likely here, that subglacial and proglacial meltwaters removed the Quaternary sediment cover along their flow paths. Bedrock cliffs with talus accumulations from the spalling of large rock blocks occur in areas of Cobalt Group sedimentary rock at numerous locations in the eastern part of the project area.

Areas where thin patches of surficial sediment cover more than 50% of the bedrock surface have been defined as bedrock-drift complex deposits (Map Units 2). The bedrock-drift complex areas were delineated through airphoto interpretation on the basis of frequent bedrock outcrops, the presence of a rugged ground surface reflecting the bedrock topography and poor drainage.

The bedrock-drift complex units were separated, where possible, into: till veneers (Unit 2a); sand and gravel veneers (Unit 2b); and sand, silt and clay veneers (Unit 2c). In inaccessible areas, this separation was based mainly on vegetation types and patterns, drainage, relief, and proximity and topographic position with respect to esker and outwash systems and the shorelines of former proglacial lakes. Where the sedimentary nature of the surficial veneer could not be inferred, the unit was designated as undifferentiated drift over bedrock (Unit 2). The veneers of drift are often strongly weathered. The distribution and sedimentary characteristics of the Quaternary sediments forming the veneers are discussed in following sections of this report.

## **Till**

Till is defined as sediment that has been transported and deposited by or from glacial ice with little or no sorting by water (Dreimanis 1982, 1988). It is the most

widespread surficial deposit in the project area and generally occurs as a discontinuous sheet covering bedrock.

The till sheet in the map area represents a single lithostratigraphic unit and is the stratigraphic equivalent of the Matheson Formation (Hughes 1959) defined in the Cochrane, Timmins and Matheson areas. The till sheet may be stratigraphically equivalent to the Adam Till (Skinner 1973) defined in the Moose River Basin in the Hudson Bay Lowland.

The till has varying composition due to: 1) incorporation of numerous bedrock lithologies of different physical characteristics into the ice; 2) deposition by a variety of glacial processes; and 3) postglacial chemical and physical weathering effects. The till was likely derived from both fresh and weathered bedrock and unconsolidated deposits. Some physical and chemical properties of till samples collected in the area are presented in the appendices (A, grainsize and carbonate content; B, heavy mineral concentrate and gold grain counts; C, heavy mineral grain counts; D, rock types of till pebbles; and E, F, G and H, results of geochemical analyses).

No till or other sedimentary units from pre-Late Wisconsinan glacial cycles have been recognized. If present, they are most likely preserved in the deeper valleys or in protected bedrock lows.

Till is commonly found as a veneer over bedrock (generally less than 1 m in thickness: Map Unit 2a) but thicknesses can exceed 4 m or more. Areas with till veneer

have frequent bedrock outcrops and a surface morphology controlled by the underlying bedrock topography. Veneers of till are found over many bedrock hills and uplands and characteristically support a mixed forest of spruce, birch, balsam fir, poplar and pine.

Thicker deposits of till (Map unit 3, greater than 1 m) occur on the larger upland surfaces, in the lee of bedrock highs, and in low areas between bedrock knobs. Very few bedrock outcrops are found within the areas mapped as till. The vegetation pattern is similar to that in till veneer areas except that the stands are more homogeneous because of less variation in topography and surface moisture conditions.

In both the till veneer and till deposit areas, a thin covering of glaciolacustrine, and/or eolian sands and silts and occasionally glaciofluvial sand and gravel or organic deposits can occur.

It is likely that till underlies many deposits of glaciolacustrine and eolian sediment and organic materials mapped as Units 6, 7 or 8. Remnant patches of till are likely to underlie glaciofluvial outwash deposits (Unit 5) where aggradation, not erosion, predominated within meltwater channels. Till is not likely to underlie glaciofluvial ice-contact deposits where subglacial and proglacial meltwater streams were highly active. Valleys and topographic lows in which meltwater flow was restricted and water ponded, may have till deposits preserved at depth.

Facies interpretation of till in areas of coarse-grained bedrock, such as felsic intrusive bedrock or Lorrain Formation arenites, is hampered by its extremely coarse

texture and strong degree of surface weathering. In areas of fine-grained bedrock, such as Archean metavolcanic-metasedimentary rock or Gowganda Formation greywackes, the original sedimentary structures in the till are preserved. Most exposures of till in the map area, are of subglacial till (Photo 3); few exposures of supraglacial till were observed.

### *Subglacial Till*

Subglacially-deposited till is the predominant till type found in the project area. Lodgement, melt-out and flow varieties were identified using sedimentological and structural characteristics (Dreimanis 1982, 1989).

Lodgement till in the project area is commonly stony (10 to 50% clasts by volume), moderately to highly compact with a silty sand matrix. The presence of striated and glacially-faceted clasts, shear structures, fissility and compositional banding, indicate deposition from actively flowing ice. Rare silt and sand stringers and lenses were observed.

Melt-out till in the project area, has a silty sand matrix and is stony (10 to 50% clasts by volume), loose to moderately compact with occasional thin, deformed sand bands and lenses. Meltwater flow generated during the melting of stagnant debris-rich ice produced sand bands and lenses within the till. Meltwater movement around cobbles and boulders during melt-out produced pockets and thin layers of silt or sand surrounding these clasts.



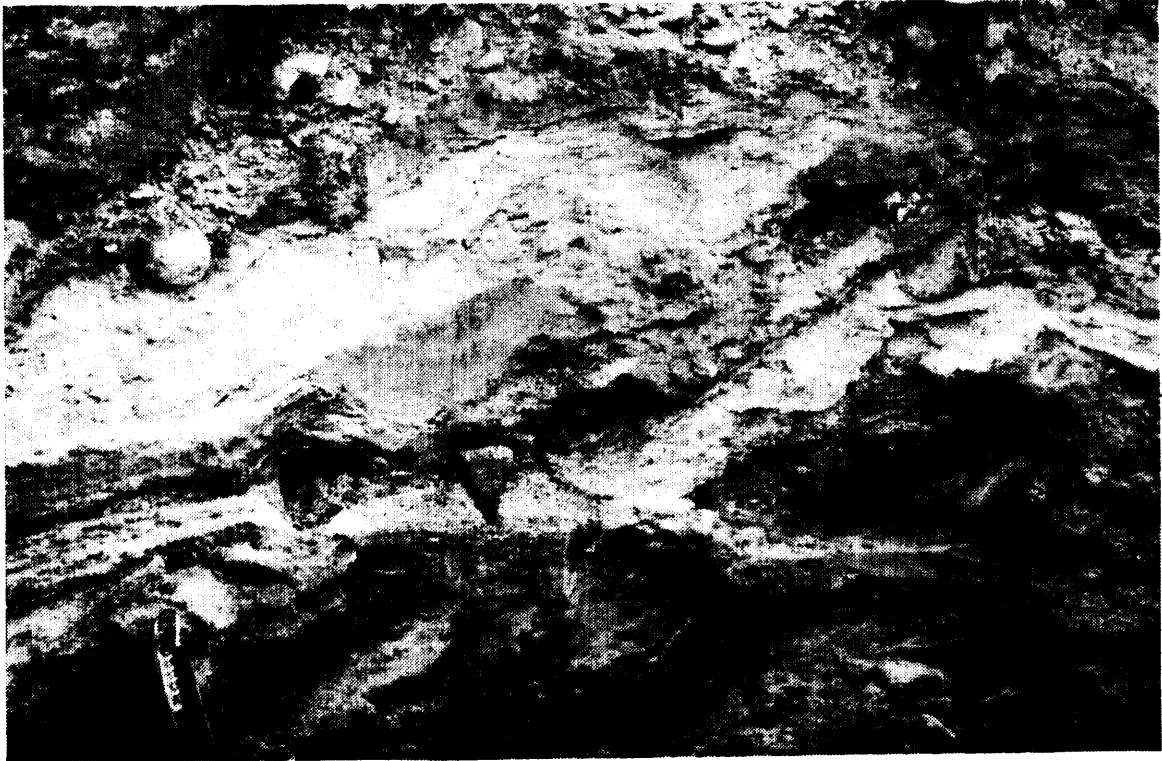
**Photo 3.** Bouldery, silty sand till overlain by eolian sand.

Flow till units are often found as wedge-shaped bodies capping subglacial till on or between bedrock knobs. Deposited subglacially in lee-side cavities, or possibly supraglacially by flowage of former subglacial debris (Photo 4), this till type is commonly stony, moderately to loosely compacted with a sand matrix. Sand stringers and crude layering in flow units are common.

Till matrix colour is a product both of matrix composition and degree of weathering. Weathered subglacial till matrix colours ranged from red (2.5 Y 5/6; Munsell Colour 1973) to yellowish brown (10 YR 6/4) to dark yellowish brown (10 YR 4/4). Unweathered or slightly weathered tills were more gray in colour (10 YR 5/1). Gray or green coloured tills were produced from metavolcanic bedrock, gray to dark gray tills from Gowganda Formation greywackes, and light gray to pinkish gray tills were produced from felsic intrusive bedrock or Lorrain Formation arenites.

The grainsize and carbonate results from 181 samples of subglacial tills are listed in Appendix A and summarized in Table 2. The grainsize composition averages 65% sand, 33% silt and 2% clay and the average median grain size is 0.133 mm (fine sand). The common textural classes are silty sand to sandy silt. The proportions of sand, silt and clay and examples of the range of grainsize distributions present are displayed in Figure 5.

The till matrix (the less than 2 mm fraction of the till) is quite texturally variable, depending upon the source bedrock type and the depositional processes. As in the Kirkland Lake (Baker 1985) and Timmins areas, the sand content varies inversely to the



**Photo 4.** Intercalated flow till and water sorted sand layers.

**Table 2. Summary of till grainsize and carbonate analyses.**

|                    | Matrix Texture |        |        | Md (mm)     | Carbonate Content |                        |
|--------------------|----------------|--------|--------|-------------|-------------------|------------------------|
|                    | % Sand         | % Silt | % Clay |             | Total %           | Calcite/Dolomite Ratio |
| Mean (N=181)       | 65             | 33     | 2      | 0.1333      | 1.54              | 0.89                   |
| Range              | 28-94          | 6-70   | 0-9    | 0.020-0.550 | 0.21-12.77        | 0-6.31                 |
| Standard Deviation | 10.6           | 10.0   | 1.5    | 0.068       | 1.62              | 0.79                   |

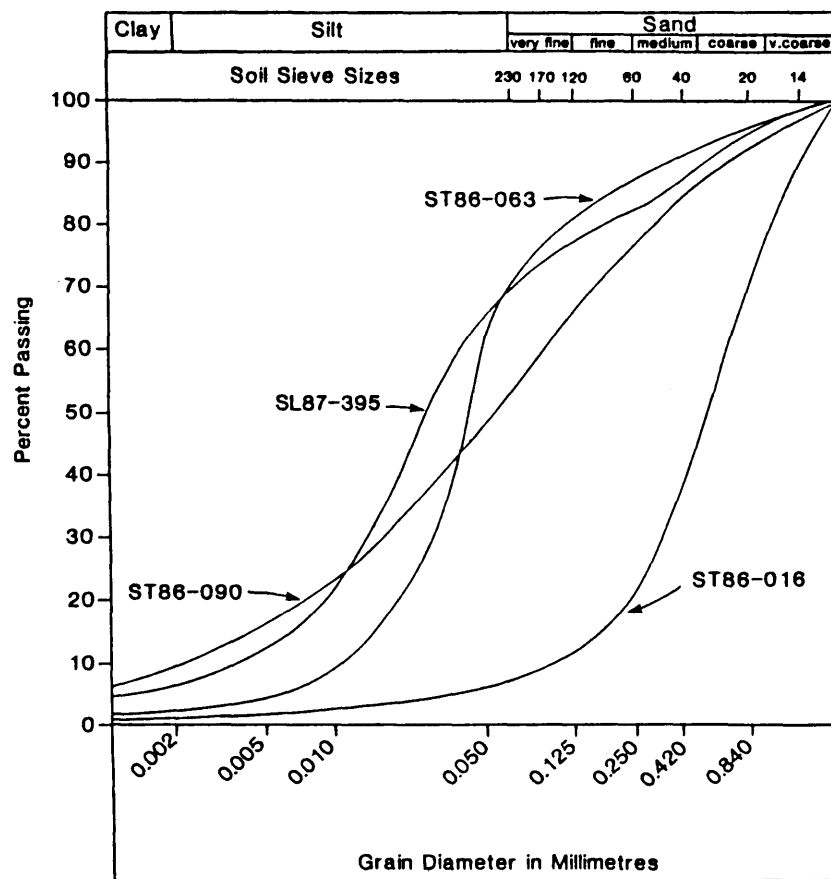
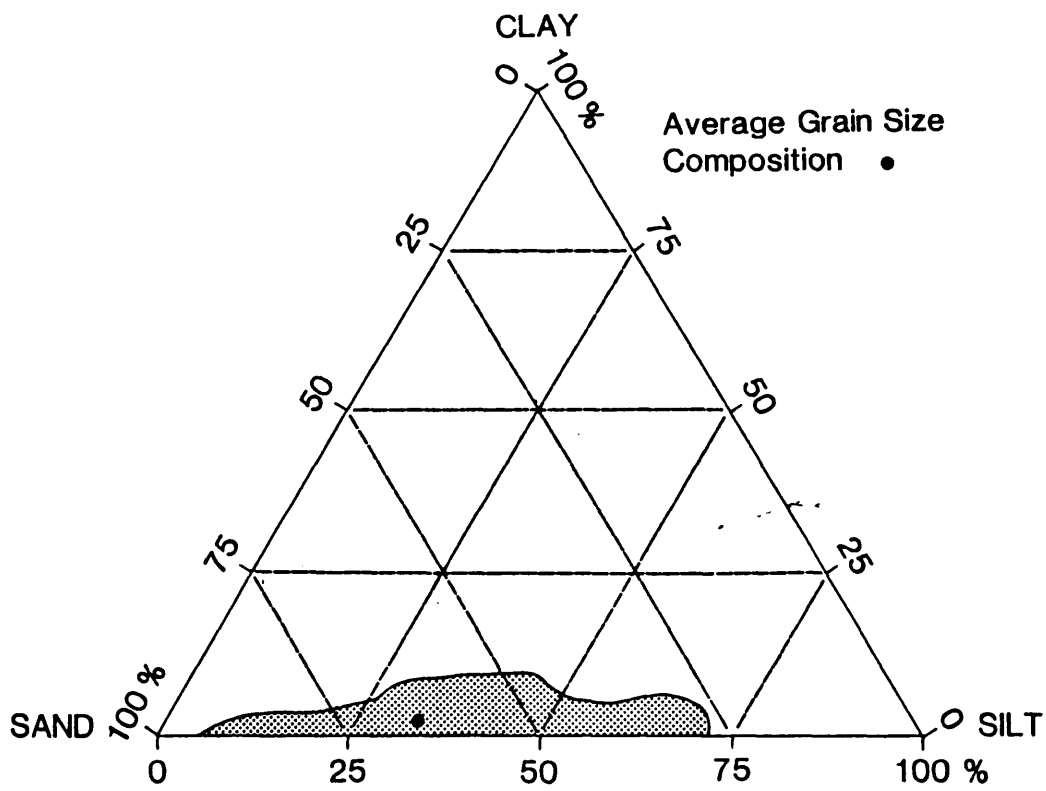


Figure 5. Textural variation in till samples a) proportions of sand, silt and clay, b) grainsize distribution curves.

silt content since the clay contents are consistently low (less than 5%). The grainsize results are similar to the proportions and ranges obtained by Closs and Sado (1982) and Aultman (1988).

The till matrix is commonly low in total carbonates (average 1.5%, range 0.2% - 12.8%) and the calcite/dolomite ratio varies widely, indicating no predominance of either mineral species (Table 2, Appendix A). The total carbonate values reflect, in part, the effects of carbonate leaching in the near surface zone (less than 1 m depth). Backhoe pit samples collected below 1m depth contained total carbonate values ranging from 5 to 12.8%. This suggests that the original carbonate content of the till matrix was higher than indicated by the near surface samples. Precipitation of carbonates has also occurred in till in the weathering zone as indicated by: the presence of total carbonate values up to 11.3% in thin surface tills; cementation of the till matrix in these locations; and the rare presence of calcium carbonate rinds on the underside of till clasts.

Non-magnetic and magnetic heavy mineral concentrates of 143 till samples were separated by a combination of concentration on a shaker table, heavy liquid separation and magnetic separation by the method described by Averill et al. (1986). The results are listed in Appendix B. Eight additional till samples were processed as part of a gold dispersal case study (Aultman 1988; Appendix B).

The weight percentage of sand-sized non-magnetic heavy minerals (S.G. greater than 3.3) averages about 0.3% (n=144) and ranges from 0.08% to 0.8%; similar to the ranges from the Timmins and Matheson areas (Bloom and Steele 1989). These similar

weight percentages of heavy minerals are likely due to the similar mix of bedrock lithologies in the three source areas, which are dominated by metavolcanic and felsic intrusive bedrock.

The weight percentage of magnetic heavy minerals averages 0.1% and ranges from 0.01% to 0.4%. The weight percentage of magnetic heavy minerals in till samples was not obviously higher over, or down-ice of, the thin iron formation bedrock units that occur in the area.

The most common mineral species in 100 point counts under a binocular microscope were: garnet and epidote with lesser amounts of pyroxene, hornblende, illmenite and hematite (see Appendix C). Few sulphide grains were observed.

The subglacial till facies contain variable amounts of clasts (10% to 50%), ranging from granules to boulders. Most are angular to subrounded in shape and often bear striations or facets. Some very large striated boulders (1 to 2 m long axis) were found during trenching and likely occur throughout the till. The hard, metavolcanic bedrock fragments, tend to form elongate, subangular clasts. The Gowganda Formation greywackes and siltstones, form elongate, subrounded clasts. The Lorrain Formation arenites commonly form plate and rectangular-shaped clasts, where the felsic intrusive bedrock fragments form spherical, subrounded clasts.

The tills are generally matrix supported and the clasts generally lie with their long axes oriented to the south or southwest. Till clast fabrics (Andrews 1971) were

completed at four sites (Figure 4). The fabrics were done in backhoe trenches or roadcuts at depths of greater than 1.5 m.

The orientation and dip of clasts with a minimum clast a:b axis ratio of 2:1 were measured to the nearest 5° or better. The data was grouped in 10° intervals and plotted on 360° hemispheric grids for presentation as rose diagrams (Nemec 1988, Figure 4).

The fabrics obtained were of moderate strength with uni- to multi-modal trends and indicate subglacial deposition. The fabric directions support the range of southerly ice flow directions obtained from striations. Even the deflection of the ice flow around a local bedrock high produced a southwestward trending clast fabric similar to nearby 220° striations (Figure 4, site JTA-8; Aultman 1988).

The clast composition of the subglacial tills often strongly reflects the local bedrock lithologies (Appendix D). Clast composition results from samples along a transect in the eastern portion of the Sinclair Lake map area are shown in Figure 6. Metavolcanic or Huronian sedimentary bedrock fragments predominate in the clast lithological assemblage. Even a small outlier of sedimentary rock contributed a large amount of rock debris to the till. Till overlying bedrock in the project area reflects the composition of bedrock lithologies which occur locally and immediately up-ice; within several hundred to a few thousand metres. About 20% of the clasts in the till samples were composed of rock types of more distant derivation, such as durable felsic intrusive bedrock.

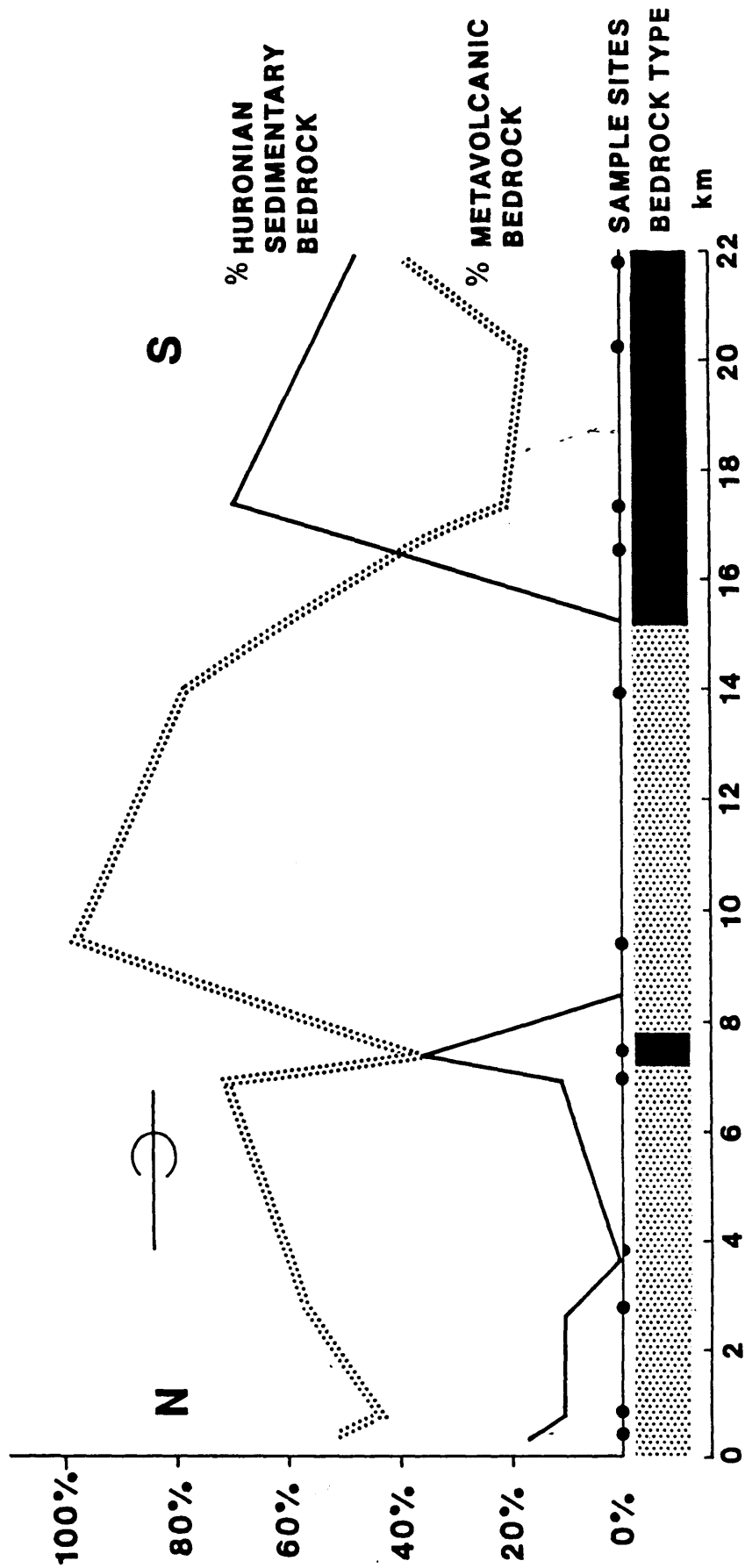


Figure 6. Clast lithological composition in subglacial tills, Sinclair Lake area.

Where clast lithology samples were taken from two levels in the same exposure, or from nearby sample sites, the percentages of rock types were similar, indicating lithological homogeneity, at least, over short distances.

In general, boulders of exotic indicator lithologies are very rare in the project area (see also Sado and Clarke 1974). Rare Paleozoic carbonate clasts, likely derived from the James Bay Lowlands, have been found in till and outwash deposits. The project area is south and east of the limit of carbonate drift as mapped by Karrow and Geddes (1987).

### *Supraglacial Till*

Supraglacial till is usually found overlying subglacial till. It is commonly thin, loose and stony with a sand matrix containing frequent subrounded cobbles and boulders of distant provenance. This till type was deposited by supraglacial melt-out at the upper ice surface or by subsequent flowage of this debris.

Commonly, soil-forming processes have affected the entire thickness of the supraglacial till. Due to its restricted occurrence, limited thickness and highly weathered nature, supraglacial till was not sampled for grain size or carbonate analyses. In addition, as this type of till is not usually composed of locally-derived rock debris, it was not sampled for mineralogical or geochemical analyses.

Supraglacial flow tills occurs as thin, stony, silty sandy units often intercalated with esker or kame sediments (Photo 4). These flow till layers were deposited concurrently with waterlain sediments.

The composition of the supraglacial till usually reflects the local bedrock lithologies poorly. They are commonly derived from material carried long distances in the ice sheet in an englacial or supraglacial position.

### **Glaciofluvial Deposits and Features**

Glaciofluvial deposits were separated into ice-contact (Unit 4) or outwash deposits (Unit 5) on the basis of internal structure, bedding and sedimentology, where sections were available. More commonly, however, deposit morphology, as observed on air photos, was used. Ice-contact stratified drift deposits are usually hummocky, have steep slopes related to deposition against ice walls and are commonly kettled. Ice-contact stratified drift deposits have a wide variety of sediment sizes (clay and silt to boulders) that were laid down in a range of ice-marginal fluvial, glaciolacustrine and colluvial environments.

Glaciofluvial outwash deposits commonly have gently sloping upper surfaces, some kettles and are composed of sorted, generally tabular beds of sand and gravel. Outwash deposits are formed in rivers and streams emanating from the glacier margin.

Hummocky, well- to variably-drained ice-contact deposits commonly support a mixed forest of white spruce, jackpine and poplar. The low relief, well drained outwash deposits commonly support very homogeneous stands of jackpine, with some white spruce and birch.

Few exposures were available in ice-contact or outwash deposits to determine detailed depositional environment or paleoflow direction. However, in eskers, ripples and cross beds indicated southward meltwater flow, against the regional topographic gradient. The flow direction of the eskers is the result of the hydraulic gradient within the ice during deposition.

Meltwater flow beyond the ice margin followed major valley systems and topographic lows. Paleoflow directions were generally southward away from the glacier margin.

The distribution of ice-contact and outwash deposits show no clear organization into belts or zones representing former ice-marginal positions in the map area. However, the Sultan Scarp, a major easterly trending ice-contact feature, occurs immediately south of the Shining Tree map area and along the southern edge of the Gowganda map area.

#### *Ice-Contact Stratified Drift Deposits*

Glaciofluvial ice-contact deposits (Unit 4) are laid down beneath, adjacent and on top of stagnant glacier ice, mainly by glaciofluvial and glaciolacustrine processes. Subsequent melting of the ice removes lateral and underlying support and causes faulting and disturbance of bedding. Dewatering and failure during and after rapid sedimentation may also caused disturbance of sedimentary structures. Ice-contact stratified drift deposits occur in eskers, kames, subaqueous fans, crevasse fillings and stagnant ice features. The deposits consist of pebbly to bouldery sand and sandy gravel.

Occasional blocks of ripped-up sediment, and some pods or layers of flow till may be present in ice-contact stratified drift deposits.

### Esker Complexes

Several esker systems are present in the study area. They are parts of much longer systems which extend beyond the project area (Boissónneau 1965; Sado and Carswell 1987). The distribution of the eskers indicate a well-integrated drainage network existed in the ice sheet. The spacing, orientation, and distribution of eskers are strongly controlled by bedrock elevation and topography.

Large, discontinuous and occasionally compound or braided eskers, up to several hundred metres wide and 90 m high, occur along the sides of the main valleys and in topographic lows. These eskers commonly have a segmented or beaded form, especially near the large lakes, such as Kapiskong, Sinclair and Marne Lakes. They commonly consist of coalescing esker ridges and kames.

Small eskers, often continuous, single ridges, trend generally southward across higher elevation areas (Photo 5). The esker ridges range up to a few hundred metres across and up to 30 m high. These eskers display cores of cobbly to bouldery gravel which are overlain and flanked by beds of sand commonly contain small faults. The form and internal composition of these eskers indicates a change in depositional environment from closed conduit flow to open channel flow.

Some small eskers are remarkably straight where they follow fault-controlled bedrock valleys, such as north of Houston Lake in Macmurchy Township. In other locations, the orientation of small eskers is quite variable, especially where they connect lake basins or other topographic lows.

### Ice Re-entrant Infillings

Several areas of hummocky and kettled ice-contact stratified drift occur in Connaught-Miramichi, Macmurchy-Fawcett, Fawcett-Leonard, Burrows-Cabot, and Sothman Townships. They form roughly inverted "V"-shaped deposits in plan view that are up to 7 km wide. These deposits probably formed in re-entrants along the ice margin which possibly formed due to the collapse of subglacial conduit roofs or preferential melting by meltwater streams focussed at the re-entrant.

The subglacial and proglacial meltwater streams deposited sediment around and on top of stagnant ice blocks. Upon melting of the supporting ice masses and buried ice blocks, steep ice-contact slopes and kettles were formed.

Although, the re-entrant infillings appear aligned along latitudinal belts, no definite ice-marginal positions have been distinguished. Similar deposits have been described in the Pamour map area (NTS 42 A/11) northeast of Timmins by Richard (1983).



**Photo 5.** Clast supported bouldery to cobbly gravel in a small esker.

## Kames, Kettles and Minor Morainic Ridges

Large, isolated, well drained kames up to a few hundred metres across, are associated with the eskers of the area. They are thought to be deposited in crevasses or moulins in the ice by meltwater streams or by colluviation during ice wastage. Locally, small kames less than several tens of metres across are found in valleys among drift-veneered bedrock knobs. Many are too small to be differentiated and mapped at 1:50 000 scale.

The internal composition of these kames is highly variable and suggests deposition in a wide variety of low and high energy environments. In Asquith Township, 2 km north of the village of Shining Tree, a kame consisting of gravelly sands with contorted bedding was probably deposited in a low to medium energy fluvial environment. Along the Grassy Lake Road in northern Kemp Township, kames are made up of clast to matrix supported cobble and boulder gravels interlayered with coarse sand and were probably deposited in a high energy fluvial environment.

Kettles are common in ice-contact deposits and occur in a variety of forms and shapes. Some kettles are partially infilled with glaciolacustrine or eolian sediments or organic material. Many of the large, lowland lakes surrounded by ice-contact deposits, such as: Waonga, Ketchiwaboose, Fawcett, South Sandstrum, Cabot, Caribou, Marne, Sinclair, Beauty and Headwater lakes are likely coalesced kettle lakes. This suggests that very large ice blocks up to several hundred metres in diameter were left stranded in valleys upon deglaciation.

Minor morainic ridges were identified in Fawcett, Connaught and Corkill townships. They probably consist of glaciofluvial ice-contact sediment or till deposited at or near the ice edge. These ridges are linear features and given their well-drained appearance, likely do not contain much till.

### *Glaciofluvial Outwash Deposits*

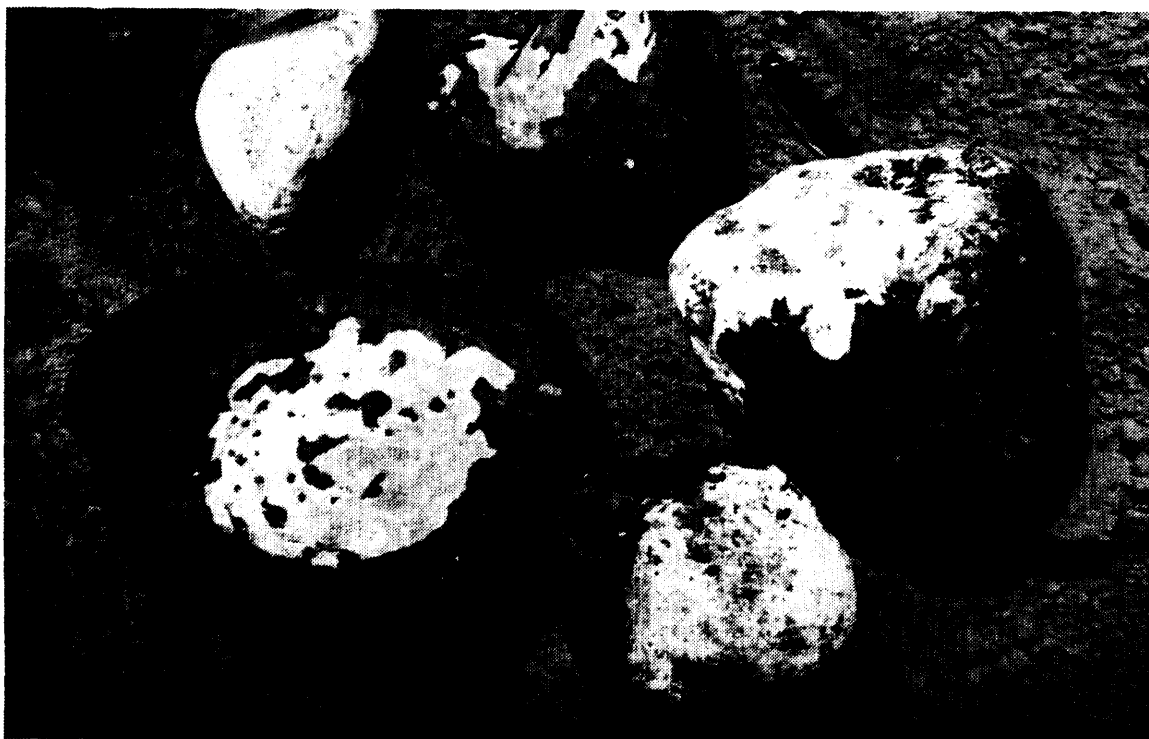
Glaciofluvial outwash deposits (Unit 5), were laid down in braided meltwater rivers beside and beyond the ice margin. These deposits consist of near horizontal beds of pebbly to gravelly sand and often flank eskers (Photo 6). Clasts are often imbricated and generally well rounded. Some beds are clast supported, with coarse sand and granules filling the interstices. Carbonate precipitation is common on the undersides of cobbles (Photo 7), forming rinds 1 to 3 mm thick. A few large boulders are found in these deposits, usually at the base of beds which fine upwards, and may represent major flood events.

The glaciofluvial outwash deposits are up to several kilometres in width and in places over 30 m thick. Large volumes of sediment were transported from the glacier and deposited in the meltwater streams of the area. Occasionally, outwash fans formed at the downstream ends of eskers. Many areas of outwash sediments probably had ice or proglacial lakes as the local base level control.

Extensive tracts of kettled and occasionally terraced outwash occupy large areas in: the southwestern, western and northwestern portions of the Shining Tree map area; the north, central and southeastern parts of the Sinclair Lake map area; and the southern



**Photo 6.** Bedded sands and gravels in a kettled outwash terrace.



**Photo 7.** Carbonate accumulations on cobbles.

parts of the Gowganda map area. The frequency of kettles in the outwash deposits indicates that large numbers of ice blocks were left stranded in the proglacial zone.

Veneers of glaciofluvial ice-contact and outwash sediments on bedrock (Unit 2b) are associated with both eskers and outwash systems. They generally occur on the saddles between topographic lows in areas of high relief, such as the areas underlain by Huronian sedimentary rock.

The sedimentary characteristics of two deep and laterally extensive glaciofluvial outwash sand deposits, just southeast of the project area in Westbrook and Garvey townships, have been investigated by Guillet (1983).

#### *Glaciofluvial Meltwater Channels*

Several of the major rivers in the area, such as the West Montreal, Grassy and Bear rivers, and Shining Tree Creek, occupy enlarged channels which were meltwater routes during deglaciation.

Meltwater channels were cut into drift between lake basins and between kettle holes in ice-contact and outwash deposits. Most of these meltwater channels are short, poorly developed and appear related to meltwater outflow from conduits at the ice edge. Boulder lag deposits on the floors of meltwater channels were noted in several locations (Photo 8). A distributary pattern of meltwater channels occurs on the outwash fan at the south end of Nabakwasi Lake.



**Photo 8.** Boulder lag accumulation in a meltwater channel.

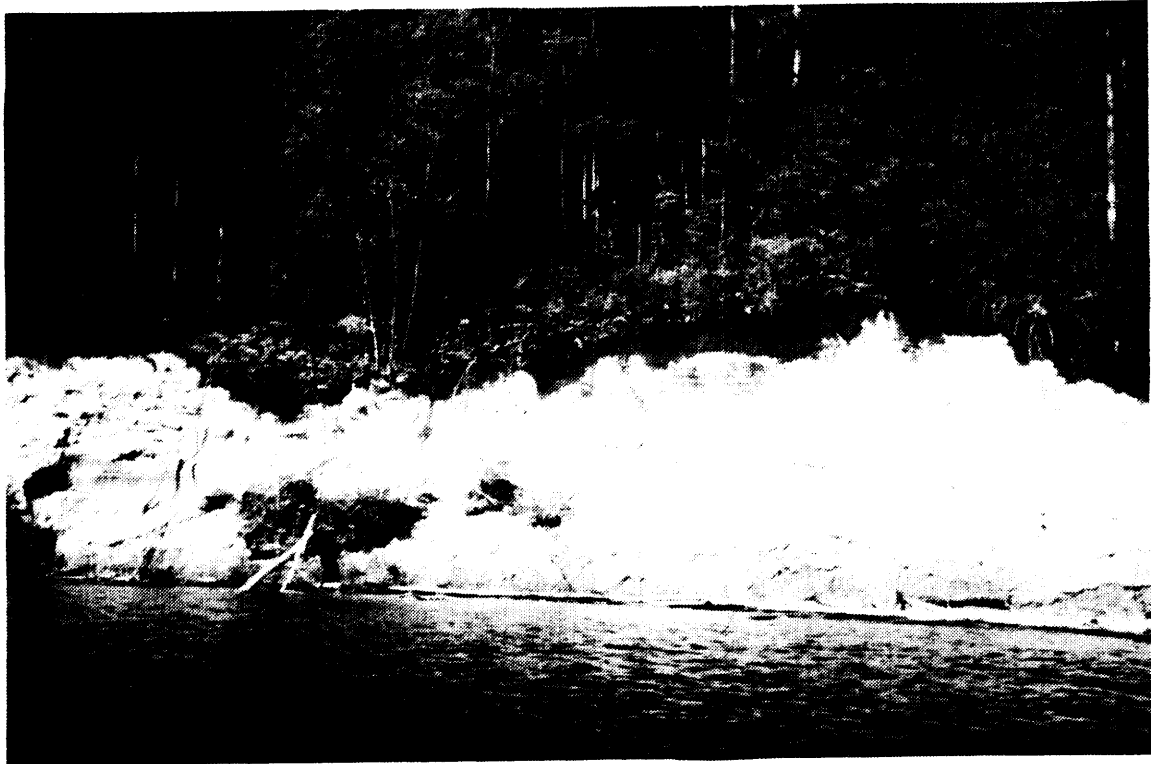
Near Ember Lake, southeast of Ferris Lake, large terraces and scarps cut in drift and bedrock were produced during meltwater drainage through this confined valley. P-forms, thought to be produced by subglacial meltwater erosion, occur on the down-ice ends of outcrops where Highway 560 crosses Michiwakenda Lake. P-forms also occur on outcrops along Highway 560 approximately 1.5 km west of Longpoint Lake.

### **Glaciolacustrine Deposits**

Glaciolacustrine deposits in the project area (Unit 6), consist of rhythmically laminated, rippled, or massive, silt and fine to medium sand, and laminated clay. Ripple drift cross-lamination and climbing ripple drift are common in the sandy deposits. Soft sediment deformation features such as folded clay beds and flame structures, are present in a few exposures. Dropstones are rare. Faulting and slumping were noted at a few locations. There were very few exposures of silt and clay rhythmites in the area.

Glaciolacustrine deposits occur in the broad topographic low areas and major north trending valleys of the project area. They are well exposed along the shores of Mattagami and Kapiskong lakes (Photo 9). Locally, glaciolacustrine deposits are up to 15 m in thickness.

The bulk of the sediment was added to the proglacial lakes and ponds by meltwater streams. Sediment was also eroded from drift-covered hills, eskers and kames by waves and redistributed by lake processes.



**Photo 9.** Rhythmically bedded glaciolacustrine sand exposed along the shores of Mattagami Lake.

The sandy glaciolacustrine deposits were deposited proximal to deltas and subaqueous fans in temporary proglacial lakes and ponds, primarily by density underflow currents. Broad sheets of nearshore sand were produced through wave erosion. Glaciofluvial deposits in topographic lows provided large quantities of sand to be eroded and distributed by proglacial lake waves and currents.

Glaciolacustrine silt to clay deposits are much less extensive. They were laid down primarily by suspension rainout and density underflow currents distal to deltas and subaqueous fans and in the central basins of the larger proglacial lakes. Rhythmically-bedded silt and clay found intercalated in kames are interpreted to represent periods of very low energy deposition in ice-contact environments.

Glaciolacustrine deposits can be quite extensive, covering up to tens of square kilometres. They are commonly wet and support a limited number of tree species, such as black spruce and cedar, in sparse, homogeneous forest stands. Veneers of glaciolacustrine sediment over bedrock knobs (Unit 2c) are found within and adjacent to the sites of former proglacial lake basins.

Few shoreline features have been identified. Most of the proglacial lakes were quite short-lived and had limited fetch. The upper extent of glaciolacustrine deposits and the occurrence of bare bedrock knobs define proglacial lakes with maximum lake levels of 366 to 381 m (1200 to 1250 ft). Beach deposits were found at an elevation of 343 m (1125 ft) in eastern Midlothian Township (Sado and Clarke 1974) and 373 m (1225 ft) on the Macmurchy-Natal township line, north of Houston Lake (E.V. Sado, field notes,

1974). Wave-washed till surfaces with boulder accumulations were found at 351 m (1150 ft) in Emerald Township along the power transmission line right-of-way.

A number of low-relief ridges less than 2 m high, interpreted as abandoned shoreline features or offshore bars have been identified at elevation 396 m (1300 ft) on the sand plains in the southwestern and southcentral parts of the Gowganda map sheet. The full extent of these proglacial lakes is unknown but they were probably controlled by topographic highs to the south in the Smoothwater Lake (NTS 41 P/7) map sheet.

A number of former proglacial lakes can be identified in the project area. The lakes appear to have formed as separate pondings with many islands, as opposed to a single, contiguous proglacial lake. They may, however, represent the initial stages of Lake Barlow-Ojibway over the region (see also Vincent and Hardy 1979). Proglacial lake shoreline elevations in the Shining Tree area are similar to beach levels reported south of Timmins (295 m, 315 m, and 335 m) and are probably those of glacial Lake Barlow-Ojibway.

Grainsize and carbonate contents of glaciolacustrine sediments were determined to characterize them and to provide information on their provenance (Figure 7). Two samples from silt and clay layers from near Firth Lake and Haines Creek had total carbonate contents of 16.7% and 19.1 % respectively. As these samples contain total carbonate values above those for unweathered till in the region, a distal sediment source must be considered. Silt and clay derived from the James Bay Lowlands would require long distance transport and connection of meltwater systems. In the Timmins area,

glacial Lake Barlow-Ojibway silts and clays also have higher carbonate contents than till samples.

### **Eolian Deposits**

Eolian deposits (Unit 7) consist of sorted, finely laminated to thinly bedded coarse silt to medium sand. They occur in large dune fields and as a widespread surficial veneer. Where this veneer overlies bedrock it is mapped as map unit 2c.

In the dune fields, parabolic and longitudinal forms are present. The dunes commonly range between 5 and 10 m in height, with some dunes exceeding 20 m in height (Photo 10). Coalescence of limbs has produced complex dune forms over 1 km in length. The form of the parabolic dunes and the dip directions of laminae and beds indicate that the dunes were deposited from a prevailing northwest wind.

The dune fields are located on and down-wind of glaciofluvial outwash and glaciolacustrine sand and silt deposits. The eolian reworking of waterlain deposits must have occurred in dry, non-vegetated conditions, after drainage of the proglacial lakes and lowering of the local groundwater level.

Grainsize results from four samples of dune sand have an average grainsize composition of 92% sand and 8% silt (Figure 7). The median diameter averaged 0.131 mm (fine sand) and the inclusive graphic standard deviation, a measure of sorting (Folk 1974), indicated the samples were only moderately to well sorted (0.43 phi to 0.88 phi). The lack of sorting is attributed to the immaturity of the eolian sediments.

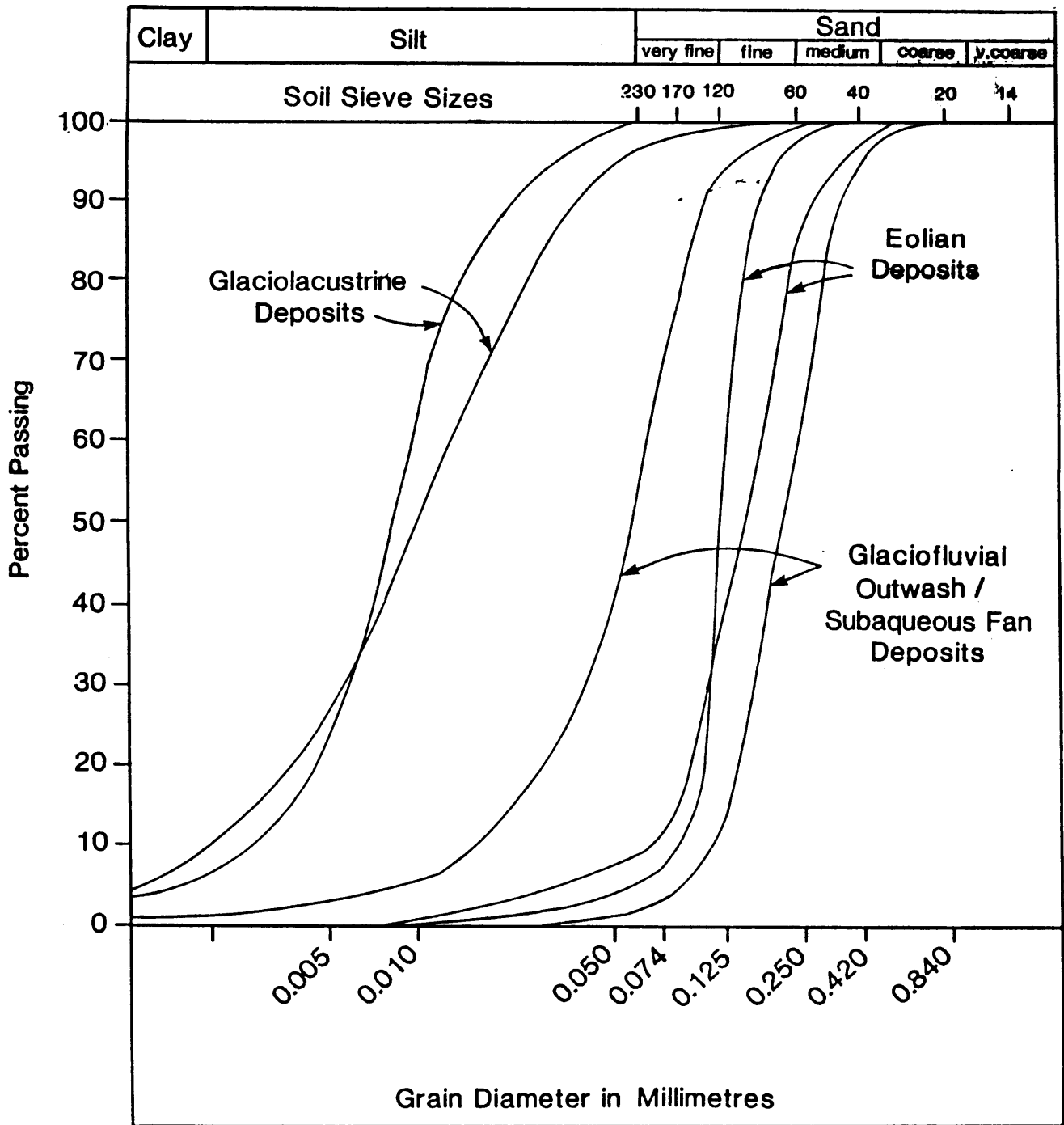


Figure 7. Glaciolacustrine and eolian grainsize distribution curves.

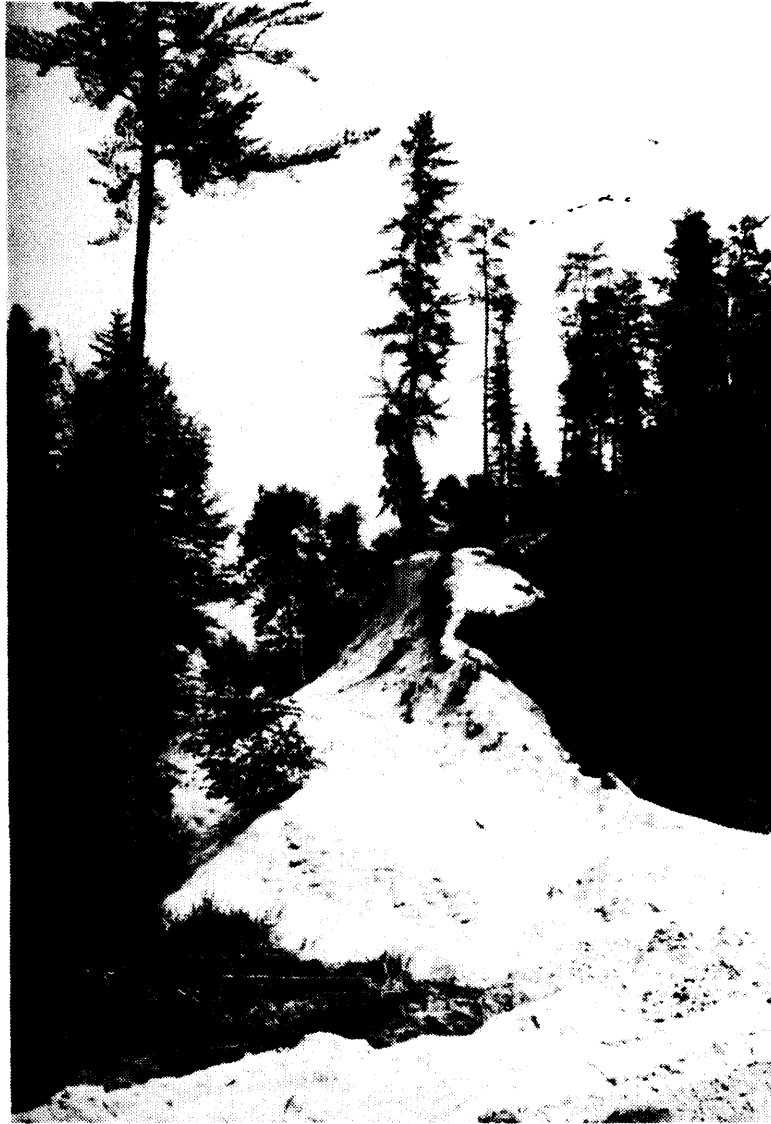


Photo 10. Large eolian dune.

Eolian sand and silt, less than 1 metre in thickness, covers other deposits, such as till, over extensive areas. The contact between the eolian sediment and the underlying deposit is commonly sharp with little evidence of mixing (Photo 11). Eolian sediment was differentiated from glaciolacustrine sand by its grainsize distribution, the lack of clay, the higher amount of void space and the tendency to be deposited on topographic highs versus lows. Roed and Hallet (1979b) have referred to these deposits as "blanket sand."

### **Organic Deposits**

Deposits of peat, muck and marl (Unit 8) up to a few metres in thickness are found in bogs and swamps occupying local topographic depressions with poor drainage. These include areas between sand dunes, along small valleys, in flood plains beside the meandering streams and rivers and in kettle holes. Thin organic deposits occur over extensive areas on glaciolacustrine sand plains, such as between Nursey and Kapiskong lakes, and south of Hangingstone Lake. In most cases, thin organic deposits were underlain by silty fine sand or silt. Areas of organic deposits are commonly flat, wet, with few or no trees but some shrub growth. Black spruce, alder and tamarack trees have been observed to grow on organic deposits greater than 1 m in thickness. The organic deposits consist of woody to amorphous organic matter with some admixed mineral material.

An inventory of the region's peatland distribution shows only a few "individual or close groupings of peatlands" (Monenco Ontario Limited 1981, Plate A-8, p.153). An evaluation of the region's peat resources has shown that the typical small size and high



Photo 11. Till sample site.

water table in the peatlands and the distance to market generally preclude development of the peat resources for fuel or horticultural purposes and that any peatlands are best left as wildlife habitat (Monenco Ontario Limited 1981).

### **Alluvial Deposits**

Alluvial deposits (Unit 9), consisting of sand, silt, gravel and some organic material, are found along the larger watercourses and are especially well developed in areas of glaciofluvial and glaciolacustrine deposits. The grainsize characteristics of the alluvium depend upon the parent material. Alluvial deposits are present along the Donnegana, Grassy, West Montreal, Montreal and Bear rivers and along Wapus and Calcite creeks. Most deposits are of very restricted areal extent and thickness, grade laterally into organic or other deposits and due to their limited size are not shown on the accompanying maps. Alluvium from abandoned streams and alluvium from modern streams are not differentiated on the map.

### **Man-Emplaced Deposits**

Man-emplaced deposits (Unit 10) include mine development waste rock and tailings, lumber mill waste, municipal waste and fill. Small areas of mine waste rock and tailings are found near the following sites: the former Ronda Mine and other small workings just east of the village of Shining Tree; the former Tyrinite Mine in Knight Township; the former United Asbestos and Stairs Mines in Midlothian Township; the former silver mines in Haultain and Nichol Townships; and the many small adits throughout the Gowganda map area. Lumber mill waste is found near Jess Lake in Macmurchy Township. Small deposits of municipal waste are found at public waste

disposal sites located along the main roads. Considerable quantities of fill have been placed within the towns of Shining Tree and Gowganda and along Highway 560 but are too small to be mapped at 1:50,000 scale.

## QUATERNARY HISTORY AND STRATIGRAPHY

The sequence of Quaternary events has been compiled from studies of the deposits, their superposition and depositional environments. As is typical for higher elevation areas in the Canadian Shield which had no extensive proglacial lake coverage, no sections with multiple tills or sequences of waterlain sediments were found and no organic materials suitable for dating or paleoenvironmental reconstruction were encountered.

The surficial sedimentary sequence records one glacial cycle, the main Wisconsinan ice advance and decay, late glacial and postglacial glaciofluvial and glaciolacustrine activity, and postglacial eolian, fluvial and biological activity.

The main (Late?) Wisconsinan ice advance removed most (if not all) of the former soil, unconsolidated deposits and the surface layer of fresh and weathered bedrock. Preferential excavation along faults and lineaments occurred, enlarging many valleys. The one till found in the project area likely correlates with the Matheson till found at or near surface in the Timmins and Matheson areas. Glacial erosion by the southwards flowing ice was pervasive and obliterated most traces of former ice flow events. Only a small number of striations, grooves and facets from a former (early to mid Wisconsinan?), southwesterly ice flow event are still present (Figure 4).

The ice cover melted from over the area about 10 000 years BP (Dyke and Prest 1987), leaving a widespread drift veneer over the irregular bedrock surface. Field evidence indicates that deglaciation over the region was characterized by stagnation and melting in place (Roed and Hallett 1979a; Finamore 1986; Alcock 1987, 1988, 1989), as opposed to the marginal retreat and readvance proposed by Boissonneau (1965, 1968). The only large or laterally extensive recessional moraine in the region is the Sultan Scarp. Ice readvances during deglaciation are not recognized.

The well-developed and integrated esker systems which stretch over considerable distances also provide evidence against readvances. If major readvances had occurred, any exposed eskers in the proglacial zone would have been overridden, sheared and capped with reworked sediments, as occurs in the Timmins area within the zone of the Cochrane re-advance (Richard 1983).

The Sultan Scarp, located along the southern boundary of the project area, is recognized as a former ice-marginal position, the only major stillstand of the ice sheet in the project area (Roed and Hallett 1979a). The Sultan Scarp is a discontinuous, north-facing ice-contact slope. At this ice marginal position, eskers terminate in broad, coalescing fans of outwash sand and gravels which were deposited in subaerial and subaqueous environments. Temporary ponding of meltwater is indicated by glaciolacustrine deposits and the presence of raised beaches on the sand plain south of the Sultan Scarp. The sand plain is incised by meltwater channels in the southwestern part of the Shining Tree map area, indicating continued meltwater output (possibly in the form of periodic floods) after the major period of sediment aggradation.

The ice marginal position which formed the Sultan Scarp is likely correlative to the Chapleau II moraine position described by Boissonneau (1968) which he interpreted to have been deposited during a readvance. The Sultan Scarp may correlate with the Roulier Moraine in northwestern Quebec mapped by Veillette (1986a, b). The Roulier Moraine marks an ice-marginal position in glacial Lake Barlow (Veillette et al. 1989, Figure 20h, p.65). Little or no readvance of the ice margin is indicated.

These moraines represents a regional scale halt in the retreat of the ice sheet margin. The position of the ice sheet margin during this halt was topographically controlled at several locations where it was up against uplands, such as the southern end of the Beauty Lake esker. However, it was unconstrained by topography in the southwestern part of the Shining Tree map area. A single ice-marginal position is marked in many locations by the Sultan Scarp but in other places, the single scarp is replaced by an unorganized mix of hummocky ice-contact sediments which passes into generally flat-lying outwash sediments.

Sado and Clarke (1974) described two field sites near Campbell and Frank lakes which suggested to them that a late glacial readvance overrode previous deposited sediments. Evidence of ice readvance was not recognized in the rest of the project area. The sites of Sado and Clarke (1974) may be explained by normal ice-marginal processes, such as localized debris flows.

A few minor recessional moraines, commonly associated with ice-contact deposits, are found in the project area. Over much of the higher elevation terrain, little drift is present over the bedrock surface and no moraines were observed on the airphotos.

Upon deglaciation, most topographic lows were inundated by short-lived proglacial lakes into which deltas and subaqueous fans and glaciolacustrine sediments were deposited. Lake washing and winnowing of the drift-mantled hills and glaciofluvial deposits produced bare bedrock knobs, lag deposits of boulders over till at the upper reaches of wave influence, and blankets of nearshore sand.

Lake drainage was controlled by sills along the major valleys. Drainage of the proglacial lakes and subsequent subaerial exposure of waterlain sediments allowed extensive eolian reworking of these deposits. Formation and migration of sand dunes and deposition of a widespread veneer of loess resulted. Following cessation of eolian activity, soil development and vegetation growth began on these deposits.

Accumulation of organic material in poorly drained topographic lows and along watercourses has occurred since the revegetation of the landscape. Fluvial reworking of mainly waterlain sediments has built up minor accumulations of modern alluvial deposits along the major watercourses. Floodplain development has generally been hampered by bedrock outcrops and coarse-grained surficial deposits adjoining the watercourse.

Since about 1900, mining, logging and human occupation have produced a number of small deposits of waste rock, tailings, sawmill waste and municipal waste, usually near the major transportation routes.

## **ECONOMIC GEOLOGY**

### **Aggregate Resources**

Aggregate resources are locally abundant in vicinity of the main transportation corridors and are derived from eskers, kames and outwash deposits. In higher elevation, remote areas, supplies may be inadequate and till or glaciolacustrine or eolian sand may be used as a substitute for fill or borrow. Few rock types deleterious to aggregate quality, such as chert, foliated metamorphic rock types or fissile sedimentary rocks were noted in till clast lithological counts or surveys of gravel pit rock types.

Many potential sand and gravel deposits would require the stripping of veneers of glaciolacustrine or eolian silty fine sand.

### **Industrial Minerals**

The industrial mineral potential of two deep and laterally extensive glaciofluvial sand deposits along Highway 560 in Westbrook and Garvey townships, immediately southeast of the project area, have been evaluated by Guillet (1983). Preliminary tests, including beneficiation by screening, attrition scrubbing and magnetic separation, were carried out on the raw material, an impure feldspathic sand. The results indicated a

feldspathic sand could be produced which may be suitable for fiberglass and coloured container glass manufacture (Guillet 1983).

## **Mineral Exploration Utilizing Overburden Geochemistry**

### *Introduction*

In the Shining Tree area, deposits and occurrences of silver, gold, bismuth, cobalt, copper, iron, molybdenum, nickel, lead, zinc, barite and asbestos occur (Bright 1970, 1989; Carter 1989; MacKean, 1968; McIlwaine 1971, 1978). Within the project area, several mines were previously in operation. These include silver mines in the Gowganda map area (Castle No. 1 Mine, Castle Tretheway Mine, Rustex Mine, Mann Mine), gold mines in the Shining Tree and Sinclair Lake map areas (Ronda Mine, Stairs Mine) and an asbestos mine in Midlothian Township (United Asbestos Mine).

The mineral potential of the area has been evaluated by Springer (1977). Zones of high gold and silver potential coincide with areas of bedrock-drift complex near the former producing mines and most active properties.

Boyle (1968) reviewed the geochemistry of silver and its deposits, including those in the Gowganda area, and the results of geochemical prospecting in soils and tills. Previous studies in the Cobalt area (Boyle 1968, p.218-219) indicated that geochemical analyses of glaciolacustrine clay and the soil developed on them were not effective in detecting native silver mineralization. However, analyses of the less than 0.177 mm (-80 mesh) fraction of till which underlies the glaciolacustrine clay or sand, and overlies the bedrock surface, were effective in outlining broad dispersal trains.

Samples of the A horizon of soils gave higher values and contrast than B horizon soil samples. In soils, the elements Ag, As, Sb and Mn and in certain locations Ni, Co and Hg were effective indicator elements. Cobalt area results should be generally applicable to the Gowganda area.

A case study of gold dispersion in till was conducted by Stewart and van Hees (1982) in the Matachewan area, northeast of the Sinclair Lake map area. The results, which are generally applicable to the project area, indicated that distinct dispersal trains from subcropping mineralized bedrock were present in a number of size fractions of surface till samples.

Aultman (1988) studied the nature of gold dispersal in till from several small gold occurrences in the Shining Tree area. The mineralization at these occurrences occurs as both free and sulphide-held gold over small subcrop areas (Carter 1980, p.65-69).

Results from the surface till samples collected up to several hundred metres down-ice of the known gold occurrences indicate gold grains are present in the sand-sized heavy mineral fraction (Figure 8). As well, anomalous gold geochemical values are present in the silt and clay and the heavy mineral concentrate fractions (Aultman 1988).

Several of the samples with higher gold grain counts and geochemical values near the source probably represent a simple subglacial dispersal train. The presence of other

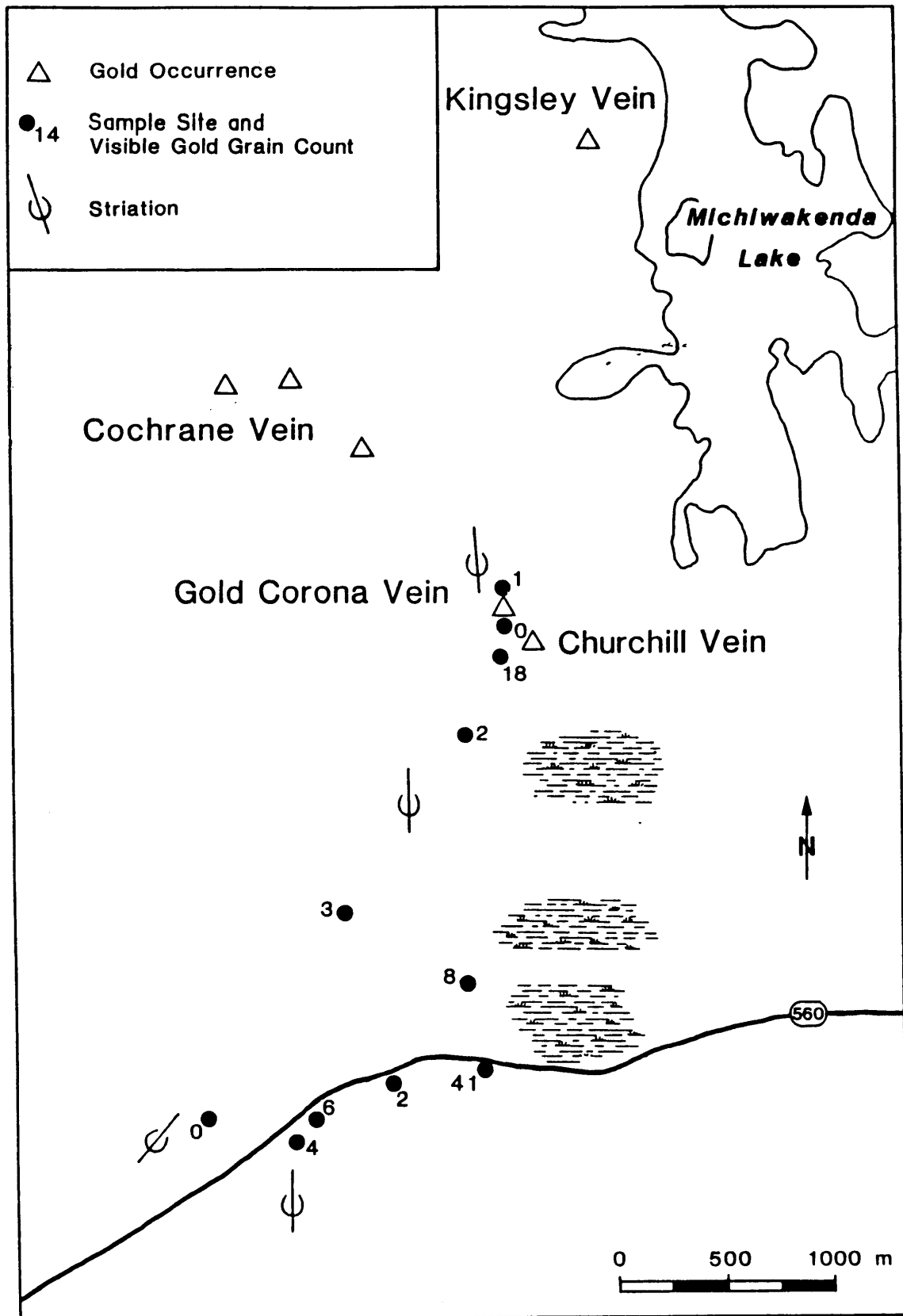


Figure 8. Distribution of gold grains in surface till samples, Beilby Lake Area, Churchill Township.

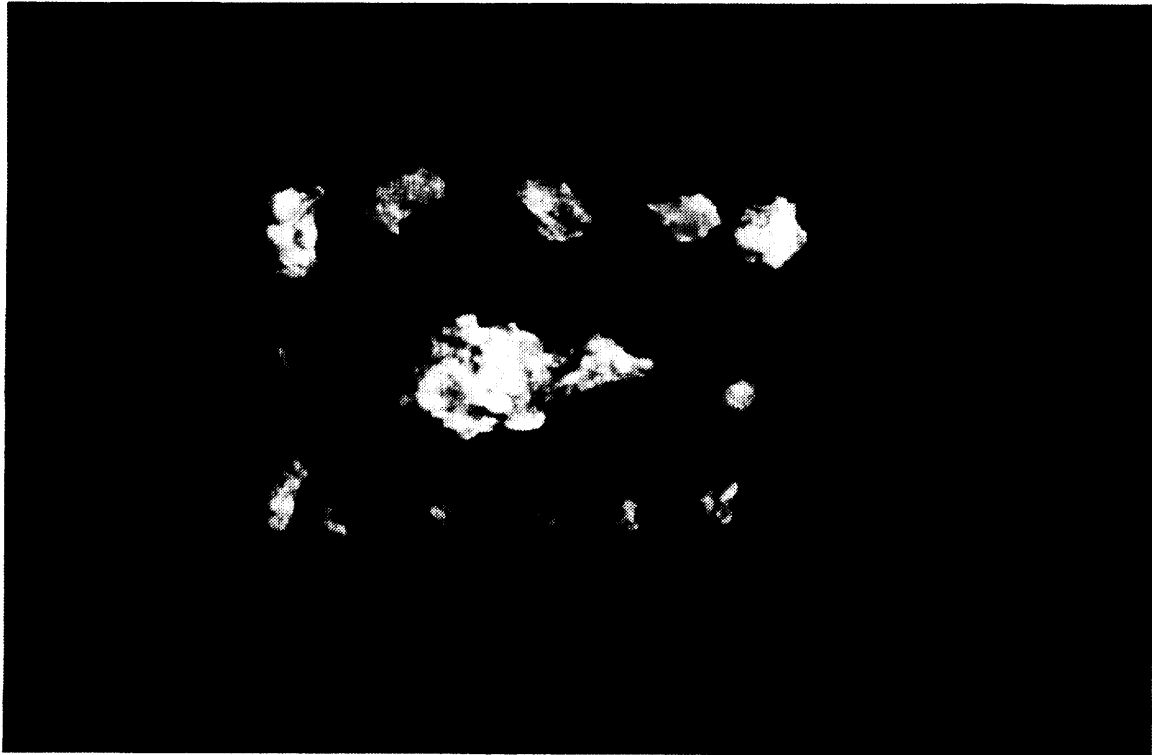
high values more than several hundred metres from source would suggest that some englacial transport also took place. It is believed that shearing within the glacier, caused by the irregular bedrock surface, distributed mineralized debris farther up into the ice; resulting in longer transport distances before deposition.

The Geological Survey of Canada has published results from a regional lake sediment geochemical sampling program which included the entire Shining Tree project area (Hornbrook and Friske 1988).

#### Present Survey

In order to develop a data base suitable for evaluating different methods of geochemical sampling and determine the background values in different sample media over certain bedrock types, a program of till sampling was carried out in conjunction with the Quaternary field mapping program.

Till samples were collected at approximately 1 km intervals where possible (Photo 11). Where weathered till was encountered, samples for geochemical analysis of the less than 0.063 mm (-230 mesh; silt and clay fraction) were collected from the C soil horizon. Where unweathered or partially weathered till was found, a bulk sample (approximately 10 kg) was collected for heavy mineral concentrate (S.G. greater than 3.3) preparation, visible gold grain counts (Photo 12) and heavy mineral grain counts. The heavy mineral concentrates were later geochemically analyzed. At sites where a bulk till sample was collected, a sample for geochemical analysis of the less than 0.063 mm fraction was also



**Photo 12.** Visible gold grains recovered from sample.

collected for comparative purposes. At selected till sample sites, approximately 100 clasts (2 to 15 cm a-axis) were collected and clast lithologies identified.

A total of 203 samples of weathered surface till were collected and the less than 0.063 mm fraction analysed for several major and trace elements. A total of 143 samples of slightly to unweathered till were collected for heavy mineral concentrate preparation and analyses.

The specific analyses performed include:

- 1) Atomic absorption (AA) analysis of the less than 0.063 mm (-230 mesh; silt and clay) fraction of weathered surface till;
- 2) Instrumental neutron activation analysis (INAA) for selected elements of the non-magnetic and magnetic fractions of the heavy mineral concentrate (S.G. greater than or equal to 3.3);
- 3) Fire assay analysis for selected elements of the non-magnetic and magnetic heavy mineral concentrate (S.G. as above);
- 4) Determination of the number, shape and size of visible gold grains in the heavy mineral concentrate produced by tabling of till samples;
- 5) Mineralogical identification of heavy mineral grains using 100 point counts under a binocular microscope.

In weathered till samples, the silt and clay particles scavenge mobile metal cations released through weathering of sulphides or other mineral grains in the till. In unweathered samples, the original sulphide or native metal grains, derived from

mineralized bedrock through erosion and crushing of rock debris, should be concentrated in the heavy mineral concentrate.

A geological data base, including sample number, UTM location, till matrix texture and carbonate content, silt and clay geochemistry, heavy mineral counts, heavy mineral geochemistry and till clast lithological results, compiled from laboratory and field results, is presented in the Appendices A to H. The sample results from Aultman (1988) are included in the Appendices B, E, F and G, but were not included in any of the summary statistical calculations at the end of each appendix. This was done so as not to bias the main group of geochemical or mineralogical results which were randomly collected from over the project area.

Geochemical results from the Gowganda map area are listed separately in the Appendices A to H and are not included in the geochemical summary statistics. These results are not directly comparable with 1986 and 1987 data due to a change in laboratory analytical techniques at the Ontario Geological Survey Geoscience Laboratories (see the appendix note pages for specific information). Gold grain count and mineralogical identification data from all years, however, can be compared.

Three types of geochemical landscapes can be defined in the project area: areas of thin and discontinuous drift covering bedrock (bedrock-drift complex); areas with thin glaciolacustrine or eolian deposits overlying till (commonly with less than 10 m of Quaternary sediments over bedrock); and areas where thick glaciofluvial and

glaciolacustrine deposits occur (commonly with greater than 10 m of overburden). Effective drift prospecting strategies are different in each of these areas.

Much of the higher elevation areas of Archean metavolcanic and felsic intrusive bedrock and Proterozoic sedimentary bedrock are covered by thin drift (bedrock-drift complex). In these areas, discontinuous patches of drift, often weathered till less than a few metres thick, are found. This landscape type is common in the northwestern, northeastern, south central and eastern portions of the project area. Mineral exploration using bedrock mapping and trenching, geophysics and till geochemistry, where sufficient drift is present, is best used in these areas.

Large portions of the metavolcanic-metasedimentary bedrock belt are overlain by a shallow but generally continuous blanket of till and/or glaciolacustrine or eolian deposits ranging from 1 to 10 m in thickness. Where till is covered by glaciolacustrine or eolian sediments, the area is suitable for till geochemical programs involving backhoe trenching or small drills.

In the areas of thick drift, till for sampling may be hard to find and interpretation of geochemical results may be difficult. Thick till is commonly in the form of hummocky disintegration moraine and is usually associated with glaciofluvial ice-contact and outwash deposits. Glaciolacustrine and eolian deposits may also form a thick cover over the till. In these areas, geochemical surveys must be carried out very selectively and only locally-derived, subglacial till should be sampled. Glaciofluvial, glaciolacustrine or eolian deposits are not of local deviation. In areas dominated by glaciofluvial

sediments, it is rare for till to be preserved at depth. Till geochemical surveys are of limited use and geophysical surveys may be more suitable.

The sequence and directions of former ice flows is important to know for mineral indicator tracing. Striations are the primary ice directional indicator for the project area. These commonly ranged from  $180^{\circ} \pm 30^{\circ}$ . Crosscutting striations were noted at several locations and appear to indicate late shifts in the ice direction in response to local topographic influences. At a few locations, bedrock outcrops streamlined by southerly flowing ice were found with southwesterly oriented leeside facets or grooves. These facets likely represent preserved portions of large grooves from earlier ice flows. No tills or indicator dispersal patterns associated with the southwest flow have yet been found in the Shining Tree project area.

The irregular bedrock topography of the area may have caused eroded rock debris to be transported in an englacial position in the glacier. This may affect the size, shape and length of geochemical dispersal patterns. Bedrock ridges or valleys may also have deflected dispersal trains in the project area.

It would be expected that most dispersal patterns would be ribbon to fan shaped and be oriented generally southwards, in the direction of the most recent ice flow. As ice flow direction varies locally, indicator tracing programs should take into account local striation information.

Boulder tracing, surface till geochemical analysis and backhoe trenching are effective exploration methods in those areas with till at or near the surface. Tracing trains of mineralized or altered rock boulders would be a viable exploration technique in areas where subglacial till forms the surface material, as the boulders should be locally derived and form a distinct dispersal plume. Near the source subcrop, the mineralized boulders would be found at some depth in the till and so trenching would be required to locate the head of the boulder train.

Both the silt-clay fraction and the non-magnetic heavy mineral concentrate fraction (S.G. $\geq$ 3.3) prepared from the less than 2 mm till matrix can be used for geochemical exploration. Where the surface till is weathered, the less than 0.063 mm fraction should be used; sulphide grains would be weathered and mobile elements, such as the base metals, would be attached to organic or clay particles. The heavy mineral fraction can be utilized for unweathered till or for those minerals such as gold and silver which do not weather rapidly in the surface environment.

As most of the bedrock-drift complex terrain has relatively thin drift and only restricted pockets of thicker (greater than 5 m) drift, backhoe trenching to expose bedrock and sample till is a workable technique. In areas of thick till or glaciofluvial or glaciolacustrine sand, small drills may be able to penetrate to the till-bedrock interface for geochemical or bedrock sampling.

The areas southeast of Wasapika Lake, and west of Porphyry Lake and Breeze Lake, which have potential for gold mineralization, are overlain by esker gravels.

Exploration should focus on bedrock trenching, geophysics and drilling as the local glacial drift will be distantly derived.

Traditional soil geochemical sampling would not be effective in those areas where thick or non-local glaciofluvial, glaciolacustrine or eolian deposits form the soil parent material. In these situations, plant roots may not have penetrated to a sufficient depth to remove metals or indicator elements from mineralized till or bedrock. Little or no transport of these elements to the leaves, branches and bark would have occurred and therefore vegetation litter and soil would not be enriched as a result of mineralization.

Geochemical prospecting in the Gowganda area should be carried out prudently due to the contamination present near old mine dumps, trenches and roadways (Boyle et al. 1967).

In the project area, there is no evidence as yet of multiple till sheets from different source areas or till of exotic provenance which would complicate interpretation of geochemical results. However, only the upper 4 to 5 m of the till sheet has been examined and sampled.

## **ENGINEERING GEOLOGY**

Regional engineering geology terrain maps at scale 1:100 000 (Roed and Hallett 1979a; Roed 1979) are available for the project area. The irregular bedrock surface will adversely affect road building due to the need for blasting and the volume of fill

required. This is particularly true in bedrock and bedrock-drift areas (Map units 1 and 2).

Where till is present at surface, it is commonly non-plastic, and sometimes compact and dense. It usually presents no major foundation problems. Large boulders, however, over 1 m in diameter, may be present and may make excavation difficult.

In areas where glaciolacustrine fine-grained sediments occur at surface, slope stability problems may occur. Road construction across areas of glaciolacustrine or eolian fine sands may encounter compaction problems. A cover of coarse, graded material may be required for the road bed in these areas. Thin organic deposits should be removed before a road bed is laid down as this material is prone to differential settling.

Along the shores of Mattagami Lake, a hydroelectric reservoir, steep shore bluffs have been eroded in the glaciolacustrine fine sand deposits by wave action as a result of changing water levels. Slumps and gully erosion can be expected to continue that may present hazards to cottage owners and boaters.

The groundwater potential in bedrock-drift complex deposit areas is low, but should be better in areas of glaciofluvial, lacustrine and eolian deposits. Many existing sanitary landfill sites are located in abandoned borrow pits in glaciofluvial ice-contact and outwash deposits. As these deposits usually have high permeability, the migration rates of the resultant leachates could be high.

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## APPENDIX A

### Summary of Grainsize and Carbonate Results from Till Samples, Shining Tree Area

#### Notes:

- 1) All analyses were carried out by the Geoscience Laboratory, Ontario Geological Survey;
- 2) Sand-silt boundary is 0.063 mm; clay-silt boundary is 0.002 mm; Md. is median diameter in millimetres, determined graphically;
- 3) Grain diameters on cumulative frequency curves plotted as percent passing at mesh size;
- 4) 1986 and 1987 grainsize analyses utilized seiving and hydrometer methods; 1989 grainsize analyses utilized seiving and optical particle size analyzer;
- 5) Carbonate analyzes were carried out on material finer than 0.074 mm (-200 mesh) using the Chittick apparatus.

APPENDIX A. Summary of grainsize and carbonate results from till samples and listing of samples and sample locations analyzed in appendices A to H

| SAMPLE NUMBER | Eastings | Northing | Township  | Sand (%) | Silt (%) | Clay (%) | Median (mm) | Percent Calcite | Percent Dolomite | Cal.+ |      | Cal./ |      |
|---------------|----------|----------|-----------|----------|----------|----------|-------------|-----------------|------------------|-------|------|-------|------|
|               |          |          |           |          |          |          |             |                 |                  | Dol.  | Dol. | Dol.  | Dol. |
| BI186-1       | 485700   | 5273900  | Macmurchy | 55.7     | 39.5     | 4.8      | 0.088       | 0.68            | 0.57             | 1.25  | 1.19 |       |      |
| BI186-2       | 485750   | 5273400  | Macmurchy | 55.6     | 40.6     | 3.8      | 0.084       | 0.55            | 0.92             | 1.47  | 0.60 |       |      |
| BI186-5       | 477800   | 5264250  | Asquith   | 64.9     | 32.6     | 2.5      | 0.119       | 0.46            | 0.78             | 1.24  | 0.59 |       |      |
| ST86-005      | 485800   | 5274000  | Natal     | 57.3     | 39       | 3.7      | 0.095       | 0.75            | 1.38             | 2.13  | 0.54 |       |      |
| ST86-006A     | 478400   | 5265300  | Asquith   | 61.3     | 32.8     | 5.9      | 0.113       | 0.57            | 0.57             | 1.14  | 1.00 |       |      |
| ST86-006B     | 478400   | 5265300  | Asquith   | 64.9     | 33.8     | 1.3      | 0.105       | 0.43            | 1.24             | 1.67  | 0.35 |       |      |
| ST86-009      | 482900   | 5288300  | Kelvin    | 59.4     | 32.7     | 7.9      | 0.098       | 0.57            | 0.67             | 1.24  | 0.85 |       |      |
| ST86-015      | 493400   | 5286000  | Natal     | 61.6     | 35.3     | 3.1      | 0.115       | 0.57            | 0.67             | 1.24  | 0.85 |       |      |
| ST86-016      | 495200   | 5276700  | Tyrrrell  | 93       | 6        | 1        | 0.55        | 0.43            | 0.9              | 1.33  | 0.48 |       |      |
| ST86-021      | 486700   | 5275400  | Macmurchy | 74.2     | 24.1     | 1.7      | 0.3         | 0.57            | 0.78             | 1.35  | 0.73 |       |      |
| ST86-024      | 493900   | 5278200  | Macmurchy | 65.5     | 31.4     | 3.1      | 0.15        | 0.46            | 0.67             | 1.13  | 0.69 |       |      |
| ST86-027      | 496400   | 5276900  | Tyrrrell  | 63.8     | 33.1     | 3.1      | 0.124       | 0.68            | 0.67             | 1.35  | 1.01 |       |      |
| ST86-030      | 499200   | 5277500  | Tyrrrell  | 78.7     | 20.1     | 1.2      | 0.2         | 0.57            | 0.67             | 1.24  | 0.85 |       |      |
| ST86-033      | 496300   | 5268300  | Leonard   | 62.9     | 36.2     | 0.9      | 0.125       | 0.5             | 0.46             | 0.96  | 1.09 |       |      |
| ST86-037      | 485300   | 5273200  | Macmurchy | 55.2     | 40.4     | 4.4      | 0.082       | 0.57            | 0.57             | 1.14  | 1.00 |       |      |
| ST86-039      | 496700   | 5263300  | Leonard   | 31.9     | 65       | 3.1      | 0.033       | 0.5             | 0.46             | 0.96  | 1.09 |       |      |
| ST86-042      | 483600   | 5270700  | Churchill | 84       | 14.8     | 1.2      | 0.4         | 0.5             | 0.57             | 1.07  | 0.88 |       |      |
| ST86-043      | 482200   | 5270000  | Churchill | 52.9     | 44.6     | 2.5      | 0.07        | 0.68            | 0.57             | 1.25  | 1.19 |       |      |
| ST86-048      | 483700   | 5271900  | Churchill | 56.4     | 38.5     | 5.1      | 0.1         | 0.68            | 0.57             | 1.25  | 1.19 |       |      |
| ST86-049      | 483700   | 5271900  | Churchill | 69.4     | 25.8     | 4.8      | 0.27        | 0.68            | 0.57             | 1.25  | 1.19 |       |      |
| ST86-057      | 466000   | 5286500  | Cabot     | 68.3     | 30.2     | 1.5      | 0.147       | 0.57            | 0.78             | 1.35  | 0.73 |       |      |
| ST86-059      | 488500   | 5275400  | Macmurchy | 85.5     | 13.5     | 1        | 0.233       | 0.43            | 0.9              | 1.33  | 0.48 |       |      |
| ST86-060      | 485600   | 5276800  | Macmurchy | 62.4     | 32.8     | 4.8      | 0.145       | 0.34            | 0.67             | 1.01  | 0.51 |       |      |
| ST86-063      | 464800   | 5278700  | Brunswick | 27.8     | 69.9     | 2.3      | 0.043       | 2.05            | 9.28             | 11.33 | 0.22 |       |      |
| ST86-067      | 476200   | 5261000  | Asquith   | 73.7     | 25.4     | 0.9      | 0.165       | 0.68            | 0.57             | 1.25  | 1.19 |       |      |
| ST86-068      | 475100   | 5263800  | Asquith   | 55       | 43.5     | 1.5      | 0.079       | 0.43            | 1.03             | 1.46  | 0.42 |       |      |
| ST86-069      | 475600   | 5265600  | Asquith   | 78.9     | 19.8     | 1.3      | 0.207       | 0.55            | 1.03             | 1.58  | 0.53 |       |      |
| ST86-070      | 476300   | 5264100  | Asquith   | 67.4     | 30.8     | 1.8      | 0.116       | 0.46            | 0.78             | 1.24  | 0.59 |       |      |
| ST86-072B     | 479600   | 5270600  | Churchill | 57.4     | 41.7     | 0.9      | 0.085       | 0.43            | 0.9              | 1.33  | 0.48 |       |      |
| ST86-072C     | 479600   | 5270600  | Churchill | 55       | 41.6     | 3.4      | 0.083       | 0.73            | 2.05             | 2.78  | 0.36 |       |      |
| ST86-074      | 477700   | 5273000  | Churchill | 60.1     | 37.7     | 2.2      | 0.099       | 0.46            | 0.78             | 1.24  | 0.59 |       |      |
| ST86-076      | 486000   | 5264900  | Fawcett   | 61.1     | 36.9     | 2        | 0.118       | 0.68            | 0.8              | 1.48  | 0.85 |       |      |
| ST86-077A     | 477400   | 5269900  | Churchill | 83.8     | 15       | 1.2      | 0.305       | 0.43            | 0.9              | 1.33  | 0.48 |       |      |
| ST86-077B     | 477400   | 5269900  | Churchill | 54.8     | 41.4     | 3.8      | 0.081       | 0.43            | 0.9              | 1.33  | 0.48 |       |      |
| T86-079       | 480400   | 5277500  | Churchill | 67.3     | 29.4     | 3.3      | 0.125       | 0.46            | 0.78             | 1.24  | 0.59 |       |      |
| ST86-081      | 479800   | 5275800  | Churchill | 54.9     | 42.4     | 2.7      | 0.081       | 0.46            | 0.78             | 1.24  | 0.59 |       |      |
| ST86-082      | 478400   | 5276900  | Churchill | 71.9     | 25.9     | 2.2      | 0.151       | 0.34            | 0.67             | 1.01  | 0.51 |       |      |
| ST86-083      | 476600   | 5278300  | Churchill | 93.7     | 6.3      | 0        | 0.248       | 0.34            | 0.67             | 1.01  | 0.51 |       |      |
| ST86-084      | 473900   | 5277700  | Connaught | 64.9     | 28.9     | 6.2      | 0.135       | 0.46            | 0.67             | 1.13  | 0.69 |       |      |
| ST86-085      | 474600   | 5278900  | Connaught | 47.5     | 50.3     | 2.2      | 0.061       | 0.43            | 1.03             | 1.46  | 0.42 |       |      |
| ST86-087      | 471800   | 5281400  | Cabot     | 50.9     | 45.1     | 4        | 0.066       | 0.34            | 0.78             | 1.12  | 0.44 |       |      |
| ST86-088      | 471800   | 5282900  | Cabot     | 56.8     | 39.4     | 3.8      | 0.086       | 0.46            | 0.78             | 1.24  | 0.59 |       |      |

| SAMPLE NUMBER | Eastings | Northing | Township    | Sand (%) | Silt (%) | Clay (%) | Median (mm) | Percent Calcite | Percent Dolomite | Cal.+ |       | Cal./ |      |
|---------------|----------|----------|-------------|----------|----------|----------|-------------|-----------------|------------------|-------|-------|-------|------|
|               |          |          |             |          |          |          |             |                 |                  | Dol.  | Dol.  | Dol.  | Dol. |
| ST86-089      | 472300   | 5281000  | Cabot       | 58.5     | 39       | 2.5      | 0.093       | 0.34            | 0.78             | 1.12  | 1.12  | 0.44  | 0.44 |
| ST86-090      | 482600   | 5284200  | Kelvin      | 46.4     | 44.4     | 9.2      | 0.055       | 0.68            | 0.57             | 1.25  | 1.25  | 1.19  | 1.19 |
| ST86-100      | 479900   | 5266500  | Asquith     | 65.6     | 32.6     | 1.8      | 0.125       | 0.66            | 1.13             | 1.79  | 1.79  | 0.58  | 0.58 |
| ST86-101      | 479500   | 5266200  | Asquith     | 81.4     | 17.3     | 1.3      | 0.02        | 0.43            | 1.03             | 1.46  | 1.46  | 0.42  | 0.42 |
| ST86-102      | 492200   | 5264300  | Fawcett     | 57.2     | 41.3     | 1.5      | 0.099       | 0.8             | 0.8              | 1.6   | 1.6   | 1.00  | 1.00 |
| ST86-103      | 478100   | 5267800  | Asquith     | 62.2     | 35.6     | 2.2      | 0.107       | 0.46            | 0.57             | 1.03  | 1.03  | 0.81  | 0.81 |
| ST86-104      | 479700   | 5268100  | Asquith     | 66.1     | 31.7     | 2.2      | 0.138       | 0.55            | 1.24             | 1.79  | 1.79  | 0.44  | 0.44 |
| ST86-105      | 478800   | 5269200  | Asquith     | 45.3     | 52.7     | 2        | 0.057       | 0.46            | 0.78             | 1.24  | 1.24  | 0.59  | 0.59 |
| ST86-106      | 478500   | 5269800  | Churchill   | 57.2     | 42.1     | 0.7      | 0.082       | 0.52            | 1.49             | 2.01  | 2.01  | 0.35  | 0.35 |
| ST86-107A     | 461600   | 5267900  | Londonderry | 70.6     | 28.7     | 0.7      | 0.133       | 0.57            | 0.78             | 1.35  | 1.35  | 0.73  | 0.73 |
| ST86-107B     | 461600   | 5267900  | Londonderry | 67.2     | 31.2     | 1.6      | 0.137       | 0.57            | 0.67             | 1.24  | 1.24  | 0.85  | 0.85 |
| ST86-108A     | 462100   | 5263900  | Londonderry | 47.8     | 50.6     | 1.6      | 0.06        | 0.68            | 0.57             | 1.25  | 1.25  | 1.19  | 1.19 |
| ST86-108B     | 462100   | 5263900  | Londonderry | 54       | 45.1     | 0.9      | 0.074       | 0.43            | 1.03             | 1.46  | 1.46  | 0.42  | 0.42 |
| ST86-109      | 484400   | 5267500  | Asquith     | 62.7     | 34.5     | 2.8      | 0.118       | 0.43            | 1.03             | 1.46  | 1.46  | 0.42  | 0.42 |
| ST86-110      | 483000   | 5260400  | Asquith     | 55.8     | 41.6     | 2.6      | 0.082       | 0.77            | 1.03             | 1.8   | 1.8   | 0.75  | 0.75 |
| ST86-111      | 478200   | 5260100  | Asquith     | 76.4     | 22.6     | 1        | 0.206       | 0.57            | 0.57             | 1.14  | 1.14  | 1.00  | 1.00 |
| ST86-112      | 484800   | 5267600  | Asquith     | 72.3     | 25.8     | 1.9      | 0.195       | 0.57            | 0.78             | 1.35  | 1.35  | 0.73  | 0.73 |
| ST86-113      | 482800   | 5280000  | Kelvin      | 51.3     | 45.7     | 3        | 0.116       | 0.34            | 0.78             | 1.12  | 1.12  | 0.44  | 0.44 |
| ST86-114      | 483900   | 5275100  | Churchill   | 70.8     | 27.3     | 1.9      | 0.206       | 0.43            | 1.13             | 1.56  | 1.56  | 0.38  | 0.38 |
| ST86-115      | 482100   | 5278800  | Churchill   | 46.6     | 50.8     | 2.6      | 0.057       | 0.46            | 0.78             | 1.24  | 1.24  | 0.59  | 0.59 |
| ST86-116      | 481700   | 5280500  | Kelvin      | 46.9     | 50.9     | 2.2      | 0.057       | 0.57            | 0.57             | 1.14  | 1.14  | 1.00  | 1.00 |
| ST86-117      | 477200   | 5262300  | Macmurchy   | 71.2     | 24.4     | 4.4      | 0.229       | 0.46            | 0.67             | 1.13  | 1.13  | 0.69  | 0.69 |
| ST86-118      | 477500   | 5263400  | Asquith     | 65.5     | 33.2     | 1.3      | 0.108       | 0.32            | 1.01             | 1.33  | 1.33  | 0.32  | 0.32 |
| ST86-119      | 474900   | 5260200  | Miramichi   | 56       | 42       | 2        | 0.082       | 0.43            | 1.03             | 1.46  | 1.46  | 0.42  | 0.42 |
| ST86-120      | 474900   | 5260200  | Miramichi   | 63       | 34.8     | 2.2      | 0.125       | 0.57            | 0.67             | 1.24  | 1.24  | 0.85  | 0.85 |
| ST86-121      | 485700   | 5259600  | Fawcett     | 69.5     | 27.7     | 2.8      | 0.147       | 0.43            | 1.03             | 1.46  | 1.46  | 0.42  | 0.42 |
| ST86-122      | 485500   | 5259500  | Fawcett     | 73.1     | 24.6     | 2.3      | 0.177       | 0.46            | 0.8              | 1.26  | 1.26  | 0.58  | 0.58 |
| ST86-123      | 483500   | 5260500  | Asquith     | 64.6     | 32.3     | 3.1      | 0.123       | 0.55            | 4.11             | 4.66  | 4.66  | 0.13  | 0.13 |
| ST86-124      | 486800   | 5262900  | Fawcett     | 76       | 22.1     | 1.9      | 0.202       | 0.57            | 0.57             | 1.14  | 1.14  | 1.00  | 1.00 |
| ST86-125      | 489100   | 5273300  | Macmurchy   | 83.2     | 14.5     | 2.3      | 0.239       | 0.32            | 0.92             | 1.24  | 1.24  | 0.35  | 0.35 |
| BH87-1A       | 480000   | 5293500  | Kemp        | 58       | 39       | 3        | 0.088       | 0.36            | 0                | 0.36  | 0.36  |       |      |
| BH87-1B       | 480000   | 5293500  | Kemp        | 57       | 38       | 5        | 0.085       | 0.23            | 0                | 0.23  | 0.23  |       |      |
| BH87-2A       | 479200   | 5295300  | Kemp        | 63       | 33       | 4        | 0.094       | 0.46            | 0.36             | 0.82  | 0.82  | 1.28  | 1.28 |
| BH87-2B       | 479200   | 5295300  | Kemp        | 47       | 48       | 5        | 0.056       | 1.43            | 4.36             | 5.79  | 5.79  | 0.33  | 0.33 |
| BH87-3        | 478200   | 5297300  | Kemp        | 58       | 38.5     | 3.5      | 0.093       | 0.46            | 0.36             | 0.82  | 0.82  | 1.28  | 1.28 |
| BH87-4A       | 478500   | 5298300  | Kemp        | 62       | 36       | 2        | 0.11        | 0.57            | 0.57             | 1.14  | 1.14  | 1.00  | 1.00 |
| BH87-4B       | 478500   | 5298300  | Kemp        | 51       | 44       | 5        | 0.067       | 0.64            | 1.72             | 2.36  | 2.36  | 0.37  | 0.37 |
| BH87-5A       | 467100   | 5277100  | Kemp        | 55       | 41       | 4        | 0.081       | 0.46            | 0.46             | 0.92  | 0.92  | 1.00  | 1.00 |
| BH87-5B       | 467100   | 5277100  | Kemp        | 61       | 34       | 5        | 0.108       | 0.55            | 1.03             | 1.58  | 1.58  | 0.53  | 0.53 |
| BH87-6        | 477200   | 5294300  | Kemp        | 66       | 31       | 3        | 0.145       | 1.2             | 2.93             | 44.13 | 44.13 | 0.41  | 0.41 |
| BH87-7A       | 476500   | 5294500  | Kemp        | 56       | 40.5     | 3.5      | 0.088       | 4.03            | 8.74             | 12.77 | 12.77 | 0.46  | 0.46 |
| BH87-7B       | 476500   | 529400   | Kemp        | 61.5     | 36       | 2.5      | 0.107       | 0.82            | 0.13             | 0.95  | 0.95  | 6.31  | 6.31 |
| BH87-7C       | 476500   | 5294500  | Kemp        | 56       | 40       | 4        | 0.079       | 0.82            | 0.23             | 1.05  | 1.05  | 3.57  | 3.57 |
| BH87-9        | 480000   | 5300600  | Sothman     | 73       | 24.5     | 2.5      | 0.185       | 0.59            | 0.1              | 0.69  | 0.69  | 5.9   | 5.9  |

| SAMPLE NUMBER | Easting | Northing | Township   | Sand (%) | Silt (%) | Clay (%) | Median (mm) | Percent Calcite | Percent Dolomite | Cal.+ Dol. | Cal./Dol. |
|---------------|---------|----------|------------|----------|----------|----------|-------------|-----------------|------------------|------------|-----------|
| BH87-10B      | 478000  | 53011700 | Sothman    | 52.5     | 46       | 1.5      | 0.073       | 0.23            | 0                | 0.23       | 0.52      |
| BH87-11B      | 485100  | 5299200  | Halliday   | 80.5     | 16.5     | 3        | 0.179       | 0.23            | 0.44             | 0.67       | 1.28      |
| BH87-12A      | 480100  | 5294200  | Kemp       | 61       | 35       | 4        | 0.107       | 0.46            | 0.36             | 0.82       | 1.00      |
| BH87-12B      | 480100  | 529400   | Kemp       | 54       | 40       | 6        | 0.077       | 0.34            | 0.34             | 0.68       | 0.58      |
| BH87-13       | 481600  | 5291500  | Kemp       | 66.5     | 31.5     | 2        | 0.137       | 2.55            | 4.42             | 6.97       | 1.00      |
| BH87-14       | 483100  | 5285300  | Kelvin     | 60       | 38       | 2        | 0.094       | 0.57            | 0.57             | 1.14       | 1.00      |
| ST87-007      | 467100  | 5277100  | Connaught  | 61.5     | 34       | 4.5      | 0.121       | 0.34            | 0.33             | 0.67       | 1.03      |
| ST87-009      | 467100  | 5278900  | Connaught  | 79.5     | 18.5     | 2        | 0.214       | 0.46            | 0.36             | 0.82       | 1.28      |
| SL87-011      | 489000  | 5304500  | Halliday   | 65       | 34       | 1        | 0.118       | 0.55            | 1.34             | 1.89       | 0.41      |
| SL87-012      | 488500  | 5305300  | Halliday   | 75       | 23.5     | 1.5      | 0.159       | 0.43            | 1.11             | 1.54       | 0.39      |
| SL87-013      | 488400  | 5306400  | Halliday   | 62       | 37       | 1        | 0.116       | 0.55            | 1.34             | 1.89       | 0.41      |
| SL87-016      | 488800  | 5303200  | Halliday   | 66       | 31       | 3        | 0.113       | 0.43            | 1.11             | 1.54       | 0.39      |
| SL87-018      | 489600  | 5302500  | Halliday   | 65       | 34       | 1        | 0.106       | 0.91            | 0.8              | 1.71       | 1.14      |
| SL87-022      | 490300  | 5300000  | Halliday   | 61.5     | 36.5     | 2        | 0.094       | 0.66            | 0.9              | 1.56       | 0.73      |
| SL87-036      | 499500  | 5313300  | Montrose   | 55.5     | 41.5     | 3        | 0.083       | 0.76            | 0.78             | 1.54       | 0.97      |
| SL87-038      | 499000  | 5314800  | Montrose   | 56       | 42       | 2        | 0.079       | 0.55            | 0.9              | 1.45       | 0.61      |
| SL87-069      | 480100  | 5293200  | Kemp       | 64       | 33.5     | 2.5      | 0.116       | 0.57            | 0.57             | 1.14       | 1.00      |
| SL87-075      | 479800  | 5290600  | Kemp       | 46       | 50       | 4        | 0.055       | 0.91            | 0.57             | 1.48       | 1.60      |
| SL87-080      | 479400  | 5292700  | Kemp       | 68       | 31       | 1        | 0.142       | 0.76            | 0.57             | 1.33       | 1.33      |
| SL87-082      | 479700  | 5293400  | Kemp       | 82       | 17.5     | 0.5      | 0.266       | 0.76            | 0.67             | 1.43       | 1.13      |
| SL87-086      | 479100  | 5294200  | Kemp       | 72       | 27       | 1        | 0.129       | 0.68            | 0.57             | 1.25       | 1.19      |
| SL87-090      | 478400  | 5296000  | Kemp       | 59       | 40       | 1        | 0.097       | 0.68            | 0.67             | 1.35       | 1.01      |
| SL87-096      | 478200  | 5296500  | Kemp       | 62       | 36       | 2        | 0.109       | 0.46            | 0.67             | 1.13       | 0.69      |
| SL87-098      | 496400  | 5308300  | Montrose   | 77       | 22       | 1        | 0.177       | 0.66            | 1.03             | 1.69       | 0.64      |
| SL87-100      | 496500  | 5306600  | Midlothian | 62       | 36       | 2        | 0.103       | 0.66            | 1.13             | 1.79       | 0.58      |
| SL87-102      | 464500  | 5316000  | Gouin      | 68.5     | 28.5     | 3        | 0.16        | 0.66            | 0.92             | 1.58       | 0.72      |
| SL87-105      | 466700  | 5316000  | Moher      | 73       | 25.5     | 1.5      | 0.123       | 0.76            | 0.9              | 1.66       | 0.84      |
| SL87-107      | 466800  | 5314900  | Moher      | 72       | 27       | 1        | 0.134       | 0.76            | 0.9              | 1.66       | 0.84      |
| SL87-132      | 469800  | 5309800  | Moher      | 77.5     | 21       | 1.5      | 0.183       | 0.66            | 0.92             | 1.58       | 0.72      |
| SL87-133A     | 469900  | 5309700  | Moher      | 63       | 34.5     | 2.5      | 0.116       | 0.91            | 0.9              | 1.81       | 1.01      |
| SL87-133B     | 469900  | 5309700  | Moher      | 67       | 30       | 3        | 0.119       | 0.66            | 0.92             | 1.58       | 0.72      |
| SL87-134      | 471600  | 5308900  | Moher      | 73       | 26       | 1        | 0.177       | 0.82            | 0.57             | 1.39       | 1.44      |
| SL87-136      | 471100  | 5309200  | Kemp       | 67       | 31       | 2        | 0.142       | 0.82            | 0.78             | 1.6        | 1.05      |
| SL87-141      | 480900  | 5291600  | Kemp       | 61       | 37       | 2        | 0.103       | 0.68            | 0.69             | 1.37       | 0.99      |
| SL87-157      | 497500  | 5310100  | Montrose   | 71       | 27       | 2        | 0.119       | 0.82            | 0.57             | 1.39       | 1.44      |
| SL87-161      | 488800  | 5296200  | Mond       | 62       | 36       | 2        | 0.106       | 0.34            | 0.46             | 0.8        | 0.74      |
| SL87-164      | 467000  | 5307700  | Nursey     | 64.5     | 30       | 5.5      | 0.151       | 0.23            | 0.23             | 0.46       | 1.00      |
| SL87-219A     | 477200  | 5294300  | Kemp       | 68       | 30       | 2        | 0.164       | 0.36            | 0.1              | 0.46       | 3.6       |
| SL87-219B     | 477200  | 5294300  | Kemp       | 66.5     | 32.5     | 1        | 0.119       | 0.11            | 0.1              | 0.21       | 1.1       |
| SL87-221      | 476500  | 5294300  | Kemp       | 62       | 35       | 3        | 0.119       | 0.91            | 1.24             | 2.15       | 0.73      |
| SL87-229      | 476000  | 5293200  | Kemp       | 76       | 21       | 3        | 0.151       | 0.34            | 0.46             | 0.8        | 0.74      |
| SL87-272      | 467900  | 5291000  | Burrows    | 62       | 35       | 3        | 0.109       | 0.43            | 0.92             | 1.35       | 0.47      |
| SL87-290      | 469400  | 5293700  | Burrows    | 73.5     | 25       | 1.5      | 0.146       | 0.46            | 0.36             | 0.82       | 1.28      |
| SL87-322      | 475700  | 5306200  | Sothman    | 75       | 23       | 2        | 0.213       | 0.48            | 0.21             | 0.69       | 2.29      |

| SAMPLE NUMBER | Eastings | Northing | Township   | Sand (%) | Silt (%) | Clay (%) | Median (mm) | Percent Calcite | Percent Dolomite | Cal.+ |       | Cal./ |      |
|---------------|----------|----------|------------|----------|----------|----------|-------------|-----------------|------------------|-------|-------|-------|------|
|               |          |          |            |          |          |          |             |                 |                  | Dol.  | Dol.  | Dol.  | Dol. |
| SL87-353      | 484400   | 534400   | Sample     | 62       | 29       | 9        | 0.129       | 0.46            | 0.44             | 0.9   | 1.05  | 0.85  | 1.05 |
| SL87-356      | 490400   | 5297300  | Mond       | 62       | 32       | 6        | 0.097       | 0.46            | 0.44             | 0.9   | 1.05  | 0.69  | 1.05 |
| SL87-357      | 490500   | 5296400  | Mond       | 63.5     | 34       | 2.5      | 0.109       | 0.32            | 0.67             | 0.99  | 0.48  | 0.60  | 0.48 |
| SL87-358      | 490800   | 5294600  | Mond       | 67       | 30.5     | 2.5      | 0.125       | 0.32            | 0.57             | 0.89  | 0.89  | 0.51  | 0.56 |
| SL87-359      | 491000   | 5293600  | Mond       | 68       | 30.5     | 1.5      | 0.138       | 0.57            | 0.67             | 1.24  | 1.24  | 0.77  | 0.85 |
| SL87-361      | 491400   | 5292100  | Mond       | 83       | 16       | 1        | 0.138       | 0.46            | 0.67             | 1.13  | 1.13  | 0.43  | 0.69 |
| SL87-363      | 487700   | 5275100  | Macmurchy  | 66       | 32       | 2        | 0.133       | 0.46            | 0.67             | 1.13  | 1.13  | 0.48  | 0.69 |
| SL87-364      | 487700   | 5275000  | Macmurchy  | 64       | 33.5     | 2.5      | 0.125       | 0.34            | 0.57             | 0.91  | 0.91  | 0.60  | 0.60 |
| SL87-383      | 471900   | 5313100  | Mond       | 65.5     | 31       | 3.5      | 0.119       | 0.34            | 0.67             | 1.01  | 1.01  | 0.35  | 0.51 |
| SL87-394      | 492600   | 5295600  | Mond       | 31       | 63       | 6        | 0.035       | 0.2             | 0.57             | 0.77  | 0.77  | 0.35  | 0.35 |
| SL87-395      | 494200   | 5295000  | Mond       | 73       | 26       | 1        | 0.195       | 0.34            | 0.44             | 0.78  | 0.78  | 0.77  | 0.77 |
| SL87-411      | 464800   | 5291900  | Mattagami  | 74       | 24       | 2        | 0.201       | 0.2             | 0.46             | 0.66  | 0.66  | 0.43  | 0.43 |
| SL87-412      | 463100   | 5292500  | Mattagami  | 63.5     | 35.5     | 1        | 0.125       | 0.43            | 0.9              | 1.33  | 1.33  | 0.48  | 0.48 |
| SL87-415      | 464600   | 5298700  | Emerald    | 79       | 20.5     | 0.5      | 0.195       | 0.18            | 0.92             | 1.1   | 1.1   | 0.20  | 0.20 |
| SL87-416      | 465100   | 5296400  | Mattagami  | 52.5     | 41.5     | 6        | 0.069       | 0.48            | 0.1              | 0.58  | 0.58  | 4.80  | 4.80 |
| SL87-418      | 471900   | 5297100  | Burrows    | 57       | 40.5     | 2.5      | 0.106       | 0.46            | 0.67             | 1.13  | 1.13  | 0.69  | 0.69 |
| SL87-423      | 480200   | 5296500  | Kemp       | 66       | 30.5     | 3.5      | 0.13        | 1.57            | 7.96             | 9.53  | 9.53  | 0.20  | 0.20 |
| SL87-439      | 495800   | 5302800  | Midlothian | 70       | 27       | 3        | 0.164       | 0.34            | 0.33             | 0.67  | 0.67  | 1.03  | 1.03 |
| SL87-440      | 496100   | 5302200  | Midlothian | 80       | 19       | 1        | 0.156       | 0.68            | 0.36             | 1.04  | 1.04  | 1.89  | 1.89 |
| SL87-450      | 463500   | 5309600  | Gouin      | 57.5     | 40.5     | 2        | 0.097       | 0.93            | 0.33             | 1.26  | 1.26  | 2.82  | 2.82 |
| SL87-451      | 463900   | 5305300  | Emerald    | 63       | 36       | 1        | 0.114       | 0.93            | 0.33             | 1.26  | 1.26  | 2.82  | 2.82 |
| SL87-452      | 464700   | 5298200  | Mattagami  | 64.5     | 33       | 2.5      | 0.107       | 3.89            | 6.68             | 10.57 | 10.57 | 0.58  | 0.58 |
| SL87-458      | 482900   | 5288400  | Kelvin     | 75       | 23       | 2        | 0.235       | 0.82            | 0.44             | 1.26  | 1.26  | 1.86  | 1.86 |
| SL87-461      | 498100   | 5304300  | Midlothian | 61       | 37.5     | 1.5      | 0.091       | 0.46            | 0.46             | 0.92  | 0.92  | 1.00  | 1.00 |
| SL87-513      | 463100   | 5311600  | Gouin      | 49.5     | 49       | 1.5      | 0.063       | 0.2             | 0.69             | 0.89  | 0.89  | 0.29  | 0.29 |
| SL87-514      | 463400   | 5310800  | Gouin      | 67       | 29       | 4        | 0.151       | 0.2             | 0.57             | 0.77  | 0.77  | 0.35  | 0.35 |
| SL87-517      | 464100   | 5312700  | Gouin      | 77       | 22       | 1        | 0.195       | 0.34            | 0.67             | 1.01  | 1.01  | 0.51  | 0.51 |
| SL87-518      | 463800   | 5311900  | Gouin      | 58       | 39.5     | 2.5      | 0.088       | 0.34            | 0.57             | 0.91  | 0.91  | 0.60  | 0.60 |
| SL87-521      | 483000   | 5309300  | Sample     | 62.5     | 35.5     | 2        | 0.109       | 0.43            | 0.96             | 1.39  | 1.39  | 0.45  | 0.45 |
| SL87-527      | 484700   | 5309500  | Sample     | 72.5     | 25.5     | 2        | 0.188       | 0.93            | 0.33             | 1.26  | 1.26  | 2.82  | 2.82 |
| SL87-528      | 463500   | 5290300  | Mattagami  | 65.5     | 32.5     | 2        | 0.118       | 0.82            | 0.33             | 1.15  | 1.15  | 2.48  | 2.48 |
| SL87-546      | 485300   | 5313800  | Hutt       | 65.5     | 32.5     | 2        | 0.118       | 0.82            | 0.33             | 1.15  | 1.15  | 2.48  | 2.48 |
| SL87-547      | 486800   | 5313100  | Hutt       | 64.5     | 34.5     | 1        | 0.11        | 0.48            | 0.21             | 0.69  | 0.69  | 2.29  | 2.29 |
| SL87-548      | 487000   | 5310900  | Hutt       | 64       | 34       | 2        | 0.108       | 0.46            | 0.36             | 0.82  | 0.82  | 1.28  | 1.28 |
| SL87-551      | 488200   | 5306800  | Halliday   | 68.5     | 29.5     | 2        | 0.141       | 0.59            | 0.23             | 0.82  | 0.82  | 2.57  | 2.57 |
| SL87-552      | 488400   | 5305600  | Halliday   | 78.5     | 20.5     | 1        | 0.156       | 0.34            | 0.33             | 0.67  | 0.67  | 1.03  | 1.03 |
| SL87-555      | 481800   | 5298600  | Sothman    | 78.5     | 20.5     | 1        | 0.228       | 0.68            | 0.46             | 1.14  | 1.14  | 1.48  | 1.48 |
| SL87-559      | 499400   | 5310000  | Montrose   | 48       | 46.5     | 5.5      | 0.059       | 0.34            | 0.33             | 0.67  | 0.67  | 1.03  | 1.03 |
| SL87-560      | 499200   | 5307700  | Midlothian | 59       | 39       | 2        | 0.099       | 0.46            | 0.56             | 1.02  | 1.02  | 0.82  | 0.82 |
| SL87-561      | 498100   | 5304300  | Midlothian | 60.5     | 36.5     | 3        | 0.11        | 0.46            | 0.46             | 0.92  | 0.92  | 1.00  | 1.00 |
| GW89-004      | 501500   | 5273800  | Tyrrell    | 61.5     | 35.5     | 3        | 0.11        | 0.43            | 1.13             | 1.56  | 1.56  | 0.38  | 0.38 |
| GW89-008      | 500100   | 5270300  | Tyrrell    |          |          |          |             |                 |                  |       |       |       |      |
| GW89-011      | 500000   | 5278500  | Tyrrell    |          |          |          |             |                 |                  |       |       |       |      |
| GW89-30A      | 507700   | 5278500  | Milner     |          |          |          |             |                 |                  |       |       |       |      |

| SAMPLE NUMBER | Eastings | Northing | Township   | Sand (%) | Silt (%) | Clay (%) | Median (mm) | Percent Calcite | Percent Dolomite | Cal.+ Dol. | Cal./Dol. |
|---------------|----------|----------|------------|----------|----------|----------|-------------|-----------------|------------------|------------|-----------|
| GW89-030B     | 507700   | 5278500  | Milner     | 87.5     | 10.5     | 2        | 0.37        | 0.43            | 1.34             | 1.77       | 0.32      |
| GW89-048      | 512700   | 5275800  | Milner     |          |          |          |             |                 |                  |            |           |
| GW89-057      | 519200   | 5281800  | Haultain   |          |          |          |             |                 |                  |            |           |
| GW89-071      | 534100   | 5281900  | Chown      | 74       | 24       | 2        | 0.161       | 0.43            | 1.03             | 1.46       | 0.42      |
| GW89-085      | 537600   | 5261900  | Corkill    |          |          |          |             |                 |                  |            |           |
| GW89-095      | 501500   | 5287700  | Knight     |          |          |          |             |                 |                  |            |           |
| GW89-115      | 519500   | 5277600  | Nichol     | 77       | 21.5     | 1.5      | 0.292       | 0.66            | 0.92             | 1.58       | 0.72      |
| GW89-117      | 519200   | 5278600  | Nichol     | 75       | 22       | 3        | 0.25        | 0.43            | 1.13             | 1.56       | 0.38      |
| GW89-119      | 521500   | 5277300  | Nichol     |          |          |          |             |                 |                  |            |           |
| GW89-127      | 528100   | 5278700  | Lawson     | 86.5     | 11.5     | 2        | 0.272       | 0.43            | 1.03             | 1.46       | 0.42      |
| GW89-128      | 509000   | 5282400  | Van Hise   |          |          |          |             |                 |                  |            |           |
| GW89-138      | 515900   | 5286800  | Haultain   |          |          |          |             |                 |                  |            |           |
| GW89-151      | 519200   | 528055   | Haultain   |          |          |          |             |                 |                  |            |           |
| GW89-159      | 526850   | 5268350  | Corkill    | 79       | 18       | 3        | 0.25        | 0.43            | 0.9              | 1.33       | 0.48      |
| GW89-172      | 533350   | 5283199  | Chown      | 61       | 37       | 2        | 0.114       | 0.55            | 1.03             | 1.58       | 0.53      |
| GW89-185      | 515850   | 5273350  | Milner     |          |          |          |             |                 |                  |            |           |
| GW89-195      | 516200   | 5260950  | Charters   |          |          |          |             |                 |                  |            |           |
| GW89-196      | 514200   | 5260200  | Leith      |          |          |          |             |                 |                  |            |           |
| GW89-200      | 518650   | 5263200  | Charters   | 68       | 30       | 2        | 0.132       | 0.43            | 1.01             | 1.44       | 0.43      |
| GW89-218      | 527450   | 5263050  | Corkhill   |          |          |          |             |                 |                  |            |           |
| GW89-228      | 500600   | 5276550  | Tyrrell    | 57       | 40       | 3        | 0.083       | 0.55            | 1.03             | 1.58       | 0.53      |
| GW89-229      | 500700   | 5277850  | Tyrrell    | 80       | 17       | 3        | 0.243       | 0.66            | 1.03             | 1.69       | 0.64      |
| GW89-230      | 500250   | 5277600  | Tyrrell    |          |          |          |             |                 |                  |            |           |
| GW89-238      | 533000   | 5276350  | Lawson     |          |          |          |             |                 |                  |            |           |
| SL89-246      | 496350   | 5305600  | Midlothian | 65       | 33       | 2        | 0.114       | 0.66            | 1.03             | 1.69       | 0.64      |
| SL89-247      | 496350   | 5305650  | Midlothian |          |          |          |             |                 |                  |            |           |
| COUNT         |          |          |            | 181      | 181      | 181      | 181         | 181             | 181              | 181        | 181       |
| AVERAGE       |          |          |            | 64.7     | 32.8     | 2.6      | 0.13        | 0.59            | 0.95             | 1.54       | 0.91      |
| MAXIMUM       |          |          |            | 93.7     | 69.9     | 9.2      | 0.55        | 4.03            | 9.28             | 12.77      | 6.31      |
| MINIMUM       |          |          |            | 27.8     | 6.0      | 0.0      | 0.02        | 0.11            | 0.00             | 0.21       | 0.00      |
| STD. DEV.     |          |          |            | 10.6     | 10.0     | 1.5      | 0.07        | 0.45            | 1.24             | 1.62       | 0.85      |

AULTMAN SAMPLES, CHURCHILL TOWNSHIP

| Sample Number | Eastings | Northing | Township  |
|---------------|----------|----------|-----------|
| JTA-1         | 483640   | 5271980  | Churchill |
| JTA-2         | 483670   | 5272060  | Churchill |
| JTA-3B        | 483090   | 5270540  | Churchill |
| JTA-7         | 483120   | 5270620  | Churchill |
| JTA-8A        | 482870   | 5270620  | Churchill |
| JTA-9         | 483370   | 5270700  | Churchill |
| JTA-11        | 483240   | 5271160  | Churchill |
| JTA-12        | 483570   | 5271670  | Churchill |
| JTA-14        | 483650   | 5271880  | Churchill |
| JTA-17        | 483590   | 5270970  | Churchill |



## APPENDIX B

### Heavy Mineral Concentrate and Gold Grain Count Results

#### Notes:

- 1) Heavy mineral concentrates were prepared by Overburden Drilling Management Ltd., Nepean, Ontario (Averill et al, 1986). The -2.00 mm (-10 mesh) fraction from bulk till samples was passed over a shaker table and the heavy fraction further concentrated using methylene iodide (S.G. > 3.3). This heavy fraction was separated into magnetic and non-magnetic heavy mineral concentrates.

During Tabling, if 2 or more visible gold grains were seen, the sample was hand panned and examined under a binocular microscope, and the gold grains, or any other economic or indicator minerals, were counted and sized.

APPENDIX B. Heavy mineral concentrate and gold grain count results

| Sample Number | Weight (kg wet) |           |            |             | Weight (grams dry) |             |             |          | M.I. Concentrate |          |           |         | Au    |       | Weight % of Heavy Fraction |                | Normalized Au Grains |  |
|---------------|-----------------|-----------|------------|-------------|--------------------|-------------|-------------|----------|------------------|----------|-----------|---------|-------|-------|----------------------------|----------------|----------------------|--|
|               | Table Split     | +10 Chips | Table Feed | Table Conc. | Table              | M.I. Lights | Conc. Total | Non Mag. | Mag.             | No. V.G. | Calc. ppb | Non Mag | Mag   | Mag   | 10 g HMC                   | Per 10 kg Feed | Conc. Factor         |  |
| BI186-1       | 12.3            | 3.3       | 9.0        | 110.8       | 88.5               | 22.5        | 15.8        | 6.7      | 0                | 0        | 0.176     | 0.074   | 0.00  | 0.00  | 0.0                        | 400            |                      |  |
| BI186-2       | 11.2            | 3.1       | 8.1        | 90.1        | 66.7               | 23.6        | 17.1        | 6.5      | 0                | 0        | 0.211     | 0.080   | 0.00  | 0.00  | 0.0                        | 343            |                      |  |
| BI186-5       | 13.1            | 2.9       | 10.2       | 87.8        | 59.7               | 28.1        | 18.7        | 9.4      | 0                | 0        | 0.183     | 0.092   | 0.00  | 0.00  | 0.0                        | 363            |                      |  |
| ST86-005      | 11.8            | 4.2       | 7.6        | 141.3       | 122.1              | 19.2        | 12.7        | 6.5      | 1                | 118      | 0.167     | 0.086   | 0.52  | 1.3   | 396                        |                |                      |  |
| ST86-006A     | 11.3            | 2.8       | 8.5        | 150.0       | 126.5              | 23.5        | 17.3        | 6.2      | 0                | 0        | 0.204     | 0.073   | 0.00  | 0.00  | 0.0                        | 362            |                      |  |
| ST86-006B     | 4.1             | 0.9       | 3.2        | 106.3       | 89.9               | 16.4        | 12.4        | 4.0      | 0                | 0        | 0.388     | 0.125   | 0.00  | 0.00  | 0.0                        | 195            |                      |  |
| ST86-009      | 10.7            | 3.6       | 7.1        | 145.9       | 126.9              | 19.0        | 14.0        | 5.0      | 0                | 0        | 0.197     | 0.070   | 0.00  | 0.00  | 0.0                        | 374            |                      |  |
| ST86-015      | 11.2            | 4.8       | 6.4        | 121.1       | 101.3              | 19.8        | 14.3        | 5.5      | 5                | 147      | 0.223     | 0.086   | 2.53  | 7.8   | 323                        |                |                      |  |
| ST86-016      | 10.8            | 5.6       | 5.2        | 197.9       | 165.8              | 32.1        | 22.1        | 10.0     | 3                | 2330     | 0.425     | 0.192   | 0.93  | 5.8   | 162                        |                |                      |  |
| ST86-021      | 10.6            | 8.5       | 2.1        | 126.1       | 114.9              | 11.2        | 7.3         | 3.9      | 2                | 209      | 0.348     | 0.186   | 1.79  | 9.5   | 188                        |                |                      |  |
| ST86-024      | 12.5            | 8.0       | 4.5        | 166.4       | 149.0              | 17.4        | 11.8        | 5.6      | 0                | 0        | 0.262     | 0.124   | 0.00  | 0.00  | 0.0                        | 259            |                      |  |
| ST86-027      | 13.1            | 5.4       | 7.7        | 133.6       | 110.0              | 23.6        | 15.2        | 8.4      | 3                | 613      | 0.197     | 0.109   | 1.27  | 3.9   | 326                        |                |                      |  |
| ST86-030      | 12.8            | 6.8       | 6.0        | 122.9       | 93.0               | 30.1        | 18.9        | 11.2     | 4                | 332      | 0.315     | 0.186   | 1.33  | 6.7   | 199                        |                |                      |  |
| ST86-033      | 9.0             | 4.3       | 4.7        | 148.4       | 137.9              | 10.5        | 6.7         | 3.8      | 0                | 0        | 0.143     | 0.081   | 0.00  | 0.00  | 0.0                        | 448            |                      |  |
| ST86-037      | 9.7             | 4.9       | 4.8        | 119.9       | 101.1              | 18.8        | 13.5        | 5.3      | 5                | 365      | 0.281     | 0.110   | 2.66  | 10.4  | 255                        |                |                      |  |
| ST86-039      | 9.3             | 2.9       | 6.4        | 130.7       | 120.1              | 10.6        | 6.0         | 4.6      | 0                | 0        | 0.094     | 0.072   | 0.00  | 0.00  | 0.0                        | 604            |                      |  |
| ST86-042      | 10.8            | 8.6       | 2.2        | 126.9       | 111.0              | 15.9        | 9.9         | 6.0      | 41               | 7082     | 0.450     | 0.273   | 25.79 | 186.4 | 138                        |                |                      |  |
| ST86-043      | 8.6             | 2.1       | 6.5        | 131.9       | 109.2              | 22.9        | 15.5        | 7.4      | 7                | 2137     | 0.238     | 0.114   | 3.06  | 10.8  | 284                        |                |                      |  |
| ST86-048      | 9.9             | 3.3       | 6.6        | 151.9       | 135.2              | 116.7       | 11.1        | 5.6      | 0                | 0        | 0.168     | 0.085   | 0.00  | 0.00  | 0.0                        | 395            |                      |  |
| ST86-049      | 8.9             | 6.0       | 2.9        | 134.9       | 125.4              | 9.5         | 6.2         | 3.3      | 0                | 0        | 0.214     | 0.114   | 0.00  | 0.00  | 0.0                        | 305            |                      |  |
| ST86-057      | 8.7             | 4.3       | 4.4        | 193.1       | 141.9              | 51.2        | 32.6        | 18.6     | 24               | 3943     | 0.741     | 0.423   | 4.69  | 54.5  | 86                         |                |                      |  |
| ST86-059      | 10.5            | 6.6       | 3.9        | 162.9       | 133.7              | 29.2        | 20.6        | 8.6      | 0                | 0        | 0.528     | 0.221   | 0.00  | 0.00  | 0.0                        | 134            |                      |  |
| ST86-060      | 10.2            | 5.5       | 4.7        | 122.2       | 111.0              | 11.2        | 10.4        | 0.8      | 3                | 493      | 0.221     | 0.017   | 2.68  | 6.4   | 420                        |                |                      |  |
| ST86-063      | 9.0             | 2.8       | 6.2        | 152.4       | 138.2              | 14.2        | 9.4         | 4.8      | 3                | 1860     | 0.152     | 0.077   | 2.11  | 4.8   | 437                        |                |                      |  |
| ST86-067      | 9.4             | 2.2       | 7.2        | 226.7       | 189.4              | 37.3        | 28.9        | 8.4      | 0                | 0        | 0.401     | 0.117   | 0.00  | 0.00  | 0.0                        | 193            |                      |  |
| ST86-068      | 8.2             | 3.9       | 4.3        | 128.4       | 110.0              | 18.4        | 11.9        | 6.5      | 0                | 0        | 0.277     | 0.151   | 0.00  | 0.00  | 0.0                        | 234            |                      |  |
| ST86-069      | 9.9             | 4.7       | 5.2        | 169.4       | 141.7              | 27.7        | 19.1        | 8.6      | 0                | 0        | 0.367     | 0.165   | 0.00  | 0.00  | 0.0                        | 188            |                      |  |
| ST86-070      | 9.1             | 3.2       | 5.9        | 144.2       | 115.6              | 28.6        | 20.7        | 7.9      | 3                | 484      | 0.351     | 0.134   | 1.05  | 5.1   | 206                        |                |                      |  |
| ST86-072B     | 8.2             | 1.9       | 6.3        | 157.8       | 143.5              | 14.3        | 10.1        | 4.2      | 2                | 508      | 0.160     | 0.067   | 1.40  | 3.2   | 441                        |                |                      |  |
| ST86-072C     | 11.0            | 1.8       | 9.2        | 163.6       | 143.1              | 20.5        | 14.4        | 6.1      | 0                | 0        | 0.157     | 0.066   | 0.00  | 0.00  | 0.0                        | 449            |                      |  |
| ST86-074      | 9.2             | 2.5       | 6.7        | 158.6       | 132.5              | 26.1        | 18.7        | 7.4      | 4                | 1092     | 0.230     | 0.079   | 4.14  | 12.8  | 324                        |                |                      |  |
| ST86-076      | 8.9             | 4.2       | 4.7        | 146.3       | 132.0              | 14.5        | 10.8        | 3.7      | 6                | 1639     | 0.792     | 0.417   | 1.09  | 13.2  | 83                         |                |                      |  |
| ST86-077A     | 10.9            | 5.6       | 5.3        | 216.2       | 152.1              | 64.1        | 42.0        | 22.1     | 7                | 254      | 0.227     | 0.101   | 2.07  | 4.8   | 435                        |                |                      |  |
| ST86-077B     | 9.7             | 1.3       | 8.4        | 180.5       | 153.1              | 19.3        | 19.1        | 8.5      | 4                | 141      | 0.272     | 0.121   | 0.71  | 2.8   | 254                        |                |                      |  |
| ST86-079      | 9.2             | 2.0       | 7.2        | 203.0       | 174.7              | 28.3        | 19.6        | 8.7      | 2                | 81       | 0.234     | 0.087   | 0.00  | 0.00  | 0.0                        | 311            |                      |  |
| ST86-081      | 8.8             | 2.7       | 6.1        | 168.5       | 147.5              | 19.6        | 14.3        | 5.3      | 0                | 0        | 0.275     | 0.061   | 1.29  | 4.3   | 297                        |                |                      |  |
| ST86-082      | 9.8             | 2.9       | 6.9        | 192.4       | 169.2              | 23.2        | 19.0        | 4.2      | 3                | 166      | 0.561     | 0.218   | 1.38  | 10.7  | 128                        |                |                      |  |
| ST86-083      | 8.0             | 2.4       | 5.6        | 277.4       | 233.8              | 43.6        | 31.4        | 12.2     | 6                | 1261     | 0.194     | 0.094   | 2.76  | 17.6  | 157                        |                |                      |  |
| ST86-084      | 9.7             | 6.3       | 3.4        | 136.9       | 115.2              | 21.7        | 15.1        | 6.6      | 6                | 6046     |           |         |       |       |                            |                |                      |  |

| Sample Number | Weight (kg wet) |           |            |             | Weight (grams dry) |             |          |      | M.I. Concentrate |           |         |       | Au    | Weight % of Heavy Fraction |              |                | Normalized Au Grains |  |  |
|---------------|-----------------|-----------|------------|-------------|--------------------|-------------|----------|------|------------------|-----------|---------|-------|-------|----------------------------|--------------|----------------|----------------------|--|--|
|               | Table Split     | +10 Chips | Table Feed | Table Conc. | M.I. Lights        | Conc. Total | Non Mag. | Mag. | No. V.G.         | Calc. ppb | Non Mag | Mag   |       | Mag                        | Per 10 g HMC | Per 10 kg Feed | Conc. Factor         |  |  |
| ST86-085      | 8.6             | 3.3       | 5.3        | 87.8        | 67.9               | 19.9        | 13.4     | 6.5  | 0                | 0         | 0.253   | 0.123 | 0.000 | 0.0                        | 266          |                |                      |  |  |
| ST86-087      | 10.4            | 3.1       | 7.3        | 132.8       | 111.8              | 21.0        | 16.0     | 5.0  | 9                | 956       | 0.219   | 0.068 | 4.29  | 12.3                       | 348          |                |                      |  |  |
| ST86-088      | 12.7            | 3.7       | 9.0        | 158.3       | 120.3              | 38.0        | 23.5     | 14.5 | 7                | 864       | 0.261   | 0.161 | 1.84  | 7.8                        | 237          |                |                      |  |  |
| ST86-089      | 11.3            | 4.4       | 6.9        | 207.1       | 167.3              | 39.8        | 27.2     | 12.6 | 12               | 1182      | 0.394   | 0.183 | 3.02  | 17.4                       | 173          |                |                      |  |  |
| ST86-090      | 9.0             | 3.2       | 5.8        | 178.5       | 168.7              | 9.8         | 7.8      | 2.0  | 0                | 0         | 0.134   | 0.034 | 0.00  | 0.0                        | 592          |                |                      |  |  |
| ST86-100      | 6.9             | 2.2       | 4.7        | 158.9       | 139.3              | 19.6        | 14.7     | 4.9  | 0                | 0         | 0.313   | 0.104 | 0.00  | 0.0                        | 240          |                |                      |  |  |
| ST86-101      | 8.3             | 2.3       | 6.0        | 160.1       | 129.1              | 31.0        | 22.0     | 9    | 0                | 0         | 0.367   | 0.150 | 0.00  | 0.0                        | 194          |                |                      |  |  |
| ST86-102      | 5.7             | 1.8       | 3.9        | 137.1       | 116.4              | 20.7        | 15.6     | 5.1  | 3                | 359       | 0.400   | 0.131 | 1.45  | 7.7                        | 188          |                |                      |  |  |
| ST86-103      | 12.4            | 2.2       | 10.2       | 202.3       | 170.0              | 32.3        | 23.2     | 9.1  | 8                | 621       | 0.227   | 0.089 | 2.48  | 7.8                        | 316          |                |                      |  |  |
| ST86-104      | 8.9             | 2.1       | 6.8        | 123.5       | 94.6               | 28.9        | 20.5     | 8.4  | 2                | 610       | 0.301   | 0.124 | 0.69  | 2.9                        | 235          |                |                      |  |  |
| ST86-105      | 10.4            | 0.8       | 9.6        | 79.5        | 56.7               | 22.8        | 16.1     | 6.7  | 0                | 0         | 0.168   | 0.070 | 0.00  | 0.0                        | 421          |                |                      |  |  |
| ST86-106      | 4.4             | 0.8       | 3.6        | 61.1        | 47.9               | 13.2        | 9.7      | 3.5  | 0                | 0         | 0.269   | 0.097 | 0.00  | 0.0                        | 273          |                |                      |  |  |
| ST86-107A     | 10.1            | 1.7       | 8.4        | 105.6       | 65.9               | 39.7        | 27.5     | 12.2 | 0                | 0         | 0.327   | 0.145 | 0.00  | 0.0                        | 212          |                |                      |  |  |
| ST86-107B     | 5.2             | 1.5       | 3.7        | 89.5        | 66.1               | 23.4        | 16.9     | 6.5  | 0                | 0         | 0.457   | 0.176 | 0.00  | 0.0                        | 158          |                |                      |  |  |
| ST86-108A     | 9.7             | 2.0       | 7.7        | 99.9        | 75.6               | 24.3        | 16.8     | 7.5  | 6                | 102       | 0.218   | 0.097 | 2.47  | 7.8                        | 317          |                |                      |  |  |
| ST86-108B     | 4.6             | 1.0       | 3.6        | 68.2        | 50.0               | 18.2        | 13.5     | 4.7  | 0                | 0         | 0.375   | 0.131 | 0.00  | 0.0                        | 198          |                |                      |  |  |
| ST86-109      | 8.5             | 3.0       | 5.5        | 82.0        | 61.6               | 20.4        | 13.5     | 6.9  | 4                | 104       | 0.245   | 0.125 | 1.96  | 7.3                        | 270          |                |                      |  |  |
| ST86-110      | 11.4            | 3.4       | 8.0        | 120.6       | 97.2               | 23.4        | 14.9     | 8.5  | 4                | 313       | 0.186   | 0.106 | 1.71  | 5.0                        | 342          |                |                      |  |  |
| ST86-111      | 11.3            | 4.5       | 6.8        | 121.2       | 86.3               | 34.9        | 22.3     | 12.6 | 11               | 1335      | 0.328   | 0.185 | 3.15  | 16.2                       | 195          |                |                      |  |  |
| ST86-112      | 8.8             | 4.5       | 4.3        | 156.9       | 136.8              | 19.8        | 13.3     | 6.5  | 0                | 0         | 0.309   | 0.151 | 0.00  | 0.0                        | 217          |                |                      |  |  |
| ST86-113      | 9.2             | 4.8       | 4.4        | 112.4       | 101.6              | 10.8        | 8.2      | 2.6  | 0                | 0         | 0.186   | 0.059 | 0.00  | 0.0                        | 407          |                |                      |  |  |
| ST86-114      | 9.5             | 2.0       | 7.5        | 170.2       | 155.0              | 15.2        | 10.9     | 4.3  | 0                | 0         | 0.145   | 0.057 | 0.00  | 0.0                        | 493          |                |                      |  |  |
| ST86-115      | 7.2             | 3.0       | 4.2        | 62.4        | 58.8               | 3.6         | 3.4      | 0.2  | 0                | 0         | 0.081   | 0.005 | 0.00  | 0.0                        | 1167         |                |                      |  |  |
| ST86-116      | 7.2             | 3.4       | 3.8        | 62.3        | 56.4               | 5.9         | 4.1      | 1.8  | 0                | 0         | 0.108   | 0.047 | 0.00  | 0.0                        | 644          |                |                      |  |  |
| ST86-117      | 5.1             | 2.2       | 2.9        | 123.8       | 114.6              | 9.2         | 6.3      | 2.9  | 0                | 0         | 0.217   | 0.100 | 0.00  | 0.0                        | 315          |                |                      |  |  |
| ST86-118      | 5.9             | 0.6       | 5.3        | 142.5       | 115.1              | 27.4        | 19.7     | 7.7  | 5                | 200       | 0.372   | 0.165 | 1.82  | 9.4                        | 193          |                |                      |  |  |
| ST86-119      | 2.8             | 0.8       | 2.0        | 84.5        | 72.7               | 11.8        | 8.7      | 3.1  | 0                | 0         | 0.435   | 0.155 | 0.00  | 0.0                        | 169          |                |                      |  |  |
| ST86-120      | 5.1             | 0.5       | 4.6        | 137.3       | 116.7              | 20.6        | 14.4     | 6.2  | 0                | 0         | 0.313   | 0.135 | 0.00  | 0.0                        | 223          |                |                      |  |  |
| ST86-121      | 12.9            | 4.8       | 8.1        | 153.2       | 124.4              | 28.6        | 18.6     | 10.2 | 0                | 0         | 0.230   | 0.126 | 0.00  | 0.0                        | 281          |                |                      |  |  |
| ST86-122      | 12.2            | 4.3       | 7.9        | 82.1        | 49.7               | 32.4        | 21.2     | 11.2 | 0                | 0         | 0.268   | 0.142 | 0.00  | 0.0                        | 244          |                |                      |  |  |
| ST86-123      | 11.9            | 2.7       | 9.2        | 174.2       | 144.9              | 29.3        | 19.6     | 9.7  | 0                | 0         | 0.213   | 0.105 | 0.00  | 0.0                        | 314          |                |                      |  |  |
| ST86-124      | 11.8            | 3.8       | 8.0        | 146.8       | 116.2              | 30.6        | 21.6     | 9    | 0                | 0         | 0.270   | 0.112 | 0.00  | 0.0                        | 261          |                |                      |  |  |
| ST86-125      | 8.9             | 4.1       | 4.8        | 130.7       | 107.8              | 22.9        | 16.9     | 6    | 4                | 2888      | 0.352   | 0.125 | 1.75  | 8.3                        | 210          |                |                      |  |  |
| BI87-1B       | 11.5            | 2.0       | 9.5        | 202.4       | 175.1              | 27.3        | 15.6     | 8.8  | 0                | 0         | 0.164   | 0.093 | 0.00  | 0.0                        | 348          |                |                      |  |  |
| BI87-2B       | 11.9            | 1.7       | 10.2       | 130.1       | 109.3              | 20.8        | 14.3     | 6.5  | 0                | 0         | 0.196   | 0.064 | 0.00  | 0.0                        | 490          |                |                      |  |  |
| BI87-4B       | 12.3            | 1.7       | 10.6       | 120.9       | 90.8               | 30.1        | 20.8     | 9.3  | 0                | 0         | 0.163   | 0.088 | 0.00  | 0.0                        | 352          |                |                      |  |  |
| BI87-5B       | 15.0            | 3.2       | 11.8       | 139.7       | 107.1              | 32.6        | 19.2     | 9.6  | 0                | 0         | 0.168   | 0.092 | 0.00  | 0.0                        | 362          |                |                      |  |  |
| BI87-6        | 13.3            | 2.5       | 10.8       | 139.4       | 111.4              | 28.0        | 18.1     | 9.9  | 0                | 0         | 0.168   | 0.092 | 0.00  | 0.0                        | 385          |                |                      |  |  |
| BI87-7A       | 12.4            | 1.1       | 11.3       | 55.7        | 29.0               | 26.7        | 18.2     | 8.5  | 0                | 0         | 0.161   | 0.075 | 0.00  | 0.0                        | 423          |                |                      |  |  |
| BI87-9        | 16.7            | 5.4       | 11.3       | 182.2       | 103.7              | 78.5        | 48.8     | 29.7 | 22               | 13314     | 0.432   | 0.263 | 2.80  | 19.5                       | 144          |                |                      |  |  |
| BI87-10B      | 11.7            | 3.1       | 8.6        | 99.0        | 72.8               | 26.2        | 17.6     | 8.6  | 7                | 116       | 0.205   | 0.100 | 2.67  | 8.1                        | 328          |                |                      |  |  |

| Sample Number | Weight (kg wet) |           |            |             | Weight (grams dry) |            |             |          | M.I. Concentrate |          |           |         | Au   |         | Weight % of Heavy Fraction |              |  | Normalized Au Grains |  |  |
|---------------|-----------------|-----------|------------|-------------|--------------------|------------|-------------|----------|------------------|----------|-----------|---------|------|---------|----------------------------|--------------|--|----------------------|--|--|
|               | Table Split     | +10 Chips | Table Feed | Table Conc. | Table Lights       | M.I. Total | Conc. Total | Non Mag. | Mag.             | No. V.G. | Calc. Ppb | Non Mag | Mag  | Per HMC | Per 10 kg Feed             | Conc. Factor |  |                      |  |  |
| BI187-11B     | 8.3             | 4.3       | 4.0        | 129.7       | 88.2               | 41.5       | 27.9        | 13.6     | 10               | 2713     | 0.698     | 0.340   | 2.41 | 25.0    | 96                         |              |  |                      |  |  |
| BI187-12A     | 12.4            | 1.7       | 10.7       | 136.8       | 122.1              | 14.7       | 8.5         | 6.2      | 5                | 288      | 0.079     | 0.058   | 3.40 | 4.7     | 728                        |              |  |                      |  |  |
| BI187-12B     | 12.4            | 1.7       | 10.7       | 102.8       | 75.9               | 26.9       | 17.9        | 9        | 0                | 0        | 0.167     | 0.084   | 0.00 | 0.0     | 398                        |              |  |                      |  |  |
| BI187-13      | 15.1            | 8.7       | 6.4        | 131.6       | 122.9              | 8.7        | 6.0         | 2.7      | 2                | 13662    | 0.094     | 0.042   | 2.30 | 3.1     | 736                        |              |  |                      |  |  |
| SL87-011      | 12.5            | 5.5       | 7.0        | 96.0        | 69.0               | 27.6       | 18.0        | 9.6      | 4                | 5453     | 0.257     | 0.137   | 1.45 | 5.7     | 254                        |              |  |                      |  |  |
| SL87-012      | 11.5            | 1.7       | 9.8        | 114.7       | 92.3               | 22.4       | 15.2        | 7.2      | 0                | 0        | 0.155     | 0.073   | 0.00 | 0.0     | 438                        |              |  |                      |  |  |
| SL87-013      | 14.2            | 6.3       | 7.9        | 135.0       | 108.3              | 26.7       | 17.4        | 9.3      | 5                | 23621    | 0.220     | 0.118   | 1.87 | 6.3     | 296                        |              |  |                      |  |  |
| SL87-016      | 13.5            | 2.1       | 11.4       | 153.5       | 119.7              | 33.8       | 21.6        | 12.2     | 2                | 31       | 0.189     | 0.107   | 0.59 | 1.8     | 337                        |              |  |                      |  |  |
| SL87-018      | 11.8            | 2.5       | 9.3        | 216.3       | 186.0              | 30.3       | 20.5        | 9.8      | 7                | 4388     | 0.220     | 0.105   | 2.31 | 7.5     | 307                        |              |  |                      |  |  |
| SL87-022      | 13.4            | 2.0       | 11.4       | 121.2       | 85.6               | 35.6       | 22.4        | 13.2     | 5                | 450      | 0.196     | 0.116   | 1.40 | 4.4     | 320                        |              |  |                      |  |  |
| SL87-036      | 12.5            | 3.5       | 9.0        | 158.6       | 137.8              | 20.8       | 14.3        | 6.5      | 2                | 28       | 0.159     | 0.072   | 0.96 | 2.2     | 433                        |              |  |                      |  |  |
| SL87-038      | 13.5            | 1.5       | 12.0       | 185.3       | 151.7              | 33.6       | 23.8        | 9.8      | 5                | 82       | 0.198     | 0.082   | 1.49 | 4.2     | 357                        |              |  |                      |  |  |
| SL87-069      | 13.2            | 2.4       | 10.8       | 170.4       | 127.4              | 43.0       | 29.8        | 13.2     | 8                | 48       | 0.276     | 0.122   | 1.86 | 7.4     | 251                        |              |  |                      |  |  |
| SL87-075      | 12.5            | 1.4       | 11.1       | 90.4        | 65.1               | 25.3       | 17.5        | 7.8      | 10               | 1953     | 0.158     | 0.070   | 3.95 | 9.0     | 439                        |              |  |                      |  |  |
| SL87-080      | 12.6            | 2.7       | 9.9        | 57.6        | 28.9               | 28.7       | 18.7        | 10.0     | 4                | 38       | 0.189     | 0.101   | 1.39 | 4.0     | 345                        |              |  |                      |  |  |
| SL87-082      | 13.1            | 4.5       | 8.6        | 78.3        | 29.4               | 48.9       | 29.1        | 19.8     | 16               | 2262     | 0.338     | 0.230   | 3.27 | 18.6    | 176                        |              |  |                      |  |  |
| SL87-086      | 11.5            | 2.4       | 9.1        | 62.5        | 32.4               | 30.1       | 19.6        | 10.5     | 7                | 3074     | 0.215     | 0.115   | 2.33 | 7.7     | 302                        |              |  |                      |  |  |
| SL87-090      | 12.6            | 2.8       | 9.8        | 63.3        | 39.6               | 23.7       | 15.8        | 7.9      | 0                | 0        | 0.161     | 0.081   | 0.00 | 0.0     | 414                        |              |  |                      |  |  |
| SL87-096      | 11.2            | 2.4       | 8.8        | 56.3        | 36.0               | 20.3       | 13.1        | 7.2      | 5                | 890      | 0.149     | 0.082   | 2.46 | 5.7     | 433                        |              |  |                      |  |  |
| SL87-098      | 12.9            | 4.5       | 8.4        | 217.6       | 187.4              | 30.2       | 20.0        | 10.2     | 10               | 5066     | 0.238     | 0.121   | 3.31 | 11.9    | 278                        |              |  |                      |  |  |
| SL87-100      | 12.9            | 4.5       | 8.4        | 120.5       | 94.9               | 25.6       | 18.7        | 6.9      | 7                | 816      | 0.223     | 0.082   | 2.73 | 8.3     | 328                        |              |  |                      |  |  |
| SL87-102      | 14.2            | 4.3       | 9.9        | 106.9       | 55.6               | 51.3       | 33.9        | 17.4     | 6                | 1133     | 0.342     | 0.176   | 1.17 | 6.1     | 193                        |              |  |                      |  |  |
| SL87-105      | 15.9            | 3.0       | 12.9       | 190.2       | 112.2              | 78.0       | 55.4        | 22.6     | 5                | 407      | 0.429     | 0.175   | 0.64 | 3.9     | 165                        |              |  |                      |  |  |
| SL87-107      | 14.7            | 4.1       | 10.6       | 181.9       | 89.4               | 92.5       | 67.8        | 24.7     | 0                | 0        | 0.640     | 0.233   | 0.00 | 0.0     | 115                        |              |  |                      |  |  |
| SL87-132      | 13.9            | 2.9       | 11.0       | 227.7       | 151.5              | 76.2       | 54.3        | 21.9     | 0                | 0        | 0.494     | 0.199   | 0.00 | 0.0     | 144                        |              |  |                      |  |  |
| SL87-134      | 12.9            | 3.2       | 9.7        | 242.7       | 172.5              | 70.2       | 48.9        | 22.2     | 0                | 0        | 0.504     | 0.229   | 0.00 | 0.0     | 138                        |              |  |                      |  |  |
| SL87-141      | 12.2            | 2.8       | 9.4        | 88.1        | 54.8               | 33.3       | 23.5        | 9.8      | 4                | 670      | 0.250     | 0.104   | 1.20 | 4.3     | 282                        |              |  |                      |  |  |
| SL87-157      | 13.7            | 5.0       | 8.7        | 101.4       | 51.2               | 50.2       | 37.4        | 12.8     | 0                | 0        | 0.430     | 0.147   | 0.00 | 0.0     | 173                        |              |  |                      |  |  |
| SL87-161      | 13.1            | 3.8       | 9.3        | 66.3        | 39.5               | 26.8       | 18.7        | 8.1      | 6                | 343      | 0.201     | 0.087   | 2.24 | 6.5     | 347                        |              |  |                      |  |  |
| SL87-164      | 15.2            | 6.4       | 8.8        | 99.1        | 64.4               | 34.7       | 22.7        | 12.0     | 0                | 0        | 0.258     | 0.136   | 0.00 | 0.0     | 254                        |              |  |                      |  |  |
| SL87-219A     | 12.8            | 4.5       | 8.3        | 123.1       | 88.0               | 35.1       | 24.5        | 10.6     | 0                | 0        | 0.295     | 0.128   | 0.00 | 0.0     | 236                        |              |  |                      |  |  |
| SL87-229      | 13.2            | 5.1       | 8.1        | 145.6       | 93.9               | 51.7       | 37.1        | 14.6     | 0                | 0        | 0.458     | 0.180   | 0.00 | 0.0     | 157                        |              |  |                      |  |  |
| SL87-272      | 18.3            | 4.2       | 14.1       | 149.4       | 100.3              | 49.1       | 33.1        | 16.0     | 4                | 1757     | 0.235     | 0.113   | 0.81 | 2.8     | 287                        |              |  |                      |  |  |
| SL87-290      | 14.6            | 4.6       | 10.0       | 212.9       | 128.7              | 84.2       | 56.8        | 27.4     | 10               | 401      | 0.568     | 0.274   | 1.19 | 10.0    | 119                        |              |  |                      |  |  |
| SL87-322      | 12.9            | 4.7       | 8.2        | 143.9       | 108.8              | 35.1       | 25.3        | 9.8      | 0                | 0        | 0.309     | 0.120   | 0.00 | 0.0     | 234                        |              |  |                      |  |  |
| SL87-353      | 14.7            | 2.8       | 11.9       | 78.3        | 48.3               | 30.0       | 21.0        | 9.0      | 4                | 115      | 0.176     | 0.076   | 1.33 | 3.4     | 397                        |              |  |                      |  |  |
| SL87-356      | 14.1            | 1.2       | 12.9       | 82.4        | 50.3               | 32.1       | 22.2        | 9.9      | 6                | 200      | 0.172     | 0.077   | 1.87 | 4.7     | 402                        |              |  |                      |  |  |
| SL87-357      | 17.0            | 3.2       | 13.8       | 117.6       | 74.6               | 43.0       | 29.4        | 13.6     | 0                | 0        | 0.213     | 0.099   | 0.00 | 0.0     | 321                        |              |  |                      |  |  |
| SL87-358      | 13.4            | 3.0       | 10.4       | 67.1        | 39.9               | 27.2       | 18.6        | 8.6      | 3                | 371      | 0.179     | 0.083   | 1.10 | 2.9     | 382                        |              |  |                      |  |  |
| SL87-359      | 13.3            | 3.8       | 9.5        | 103.3       | 65.8               | 37.5       | 24.5        | 13.0     | 7                | 121      | 0.258     | 0.137   | 1.87 | 7.4     | 253                        |              |  |                      |  |  |
| SL87-361      | 14.3            | 4.2       | 10.1       | 135.4       | 97.3               | 38.1       | 25.8        | 12.3     | 9                | 448      | 0.255     | 0.122   | 2.36 | 8.9     | 265                        |              |  |                      |  |  |

| Sample Number | Weight (kg wet) |           |            |             | Weight (grams dry) |             |          |      | M.I. Concentrate |           |         |       | Au           |                | Weight % of Heavy Fraction |         |     | Normalized Au Grains |                |              |
|---------------|-----------------|-----------|------------|-------------|--------------------|-------------|----------|------|------------------|-----------|---------|-------|--------------|----------------|----------------------------|---------|-----|----------------------|----------------|--------------|
|               | Table Split     | +10 Chips | Table Feed | Table Conc. | M.I. Lights        | Conc. Total | Non Mag. | Mag. | No. V.G.         | Calc. ppb | Non Mag | Mag   | Per 10 g HMC | Per 10 kg Feed | Conc. Factor               | Non Mag | Mag | Per 10 g HMC         | Per 10 kg Feed | Conc. Factor |
|               |                 |           |            |             |                    |             |          |      |                  |           |         |       |              |                |                            |         |     |                      |                |              |
| SL87-363      | 13.0            | 4.5       | 8.5        | 105.1       | 70.3               | 34.8        | 21.4     | 13.4 | 0                | 0         | 0.252   | 0.158 | 0.00         | 0.0            | 244                        |         |     |                      |                |              |
| SL87-364      | 14.2            | 6.8       | 7.4        | 61.6        | 37.7               | 23.9        | 15.2     | 8.7  | 8                | 1193      | 0.205   | 0.118 | 3.35         | 10.8           | 310                        |         |     |                      |                |              |
| SL87-394      | 16.2            | 3.2       | 13.0       | 89.7        | 50.2               | 39.5        | 26.9     | 12.6 | 6                | 146       | 0.207   | 0.097 | 1.52         | 4.6            | 329                        |         |     |                      |                |              |
| SL87-411      | 12.3            | 3.6       | 8.7        | 189.1       | 134.7              | 54.4        | 36.5     | 17.9 | 2                | 33        | 0.420   | 0.206 | 0.37         | 2.3            | 160                        |         |     |                      |                |              |
| SL87-412      | 16.0            | 5.3       | 10.7       | 280.0       | 219.3              | 60.7        | 38.6     | 22.1 | 0                | 0         | 0.361   | 0.207 | 0.00         | 0.0            | 176                        |         |     |                      |                |              |
| SL87-415      | 13.4            | 5.6       | 7.8        | 219.5       | 161.5              | 58.0        | 37.2     | 20.8 | 0                | 0         | 0.477   | 0.267 | 0.00         | 0.0            | 134                        |         |     |                      |                |              |
| SL87-439      | 13.6            | 2.4       | 11.2       | 126.9       | 88.1               | 38.8        | 28.3     | 10.5 | 2                | 45        | 0.253   | 0.094 | 0.52         | 1.8            | 289                        |         |     |                      |                |              |
| SL87-440      | 17.6            | 5.0       | 12.6       | 158.8       | 121.3              | 37.5        | 30.8     | 6.7  | 4                | 216       | 0.244   | 0.053 | 1.07         | 3.2            | 336                        |         |     |                      |                |              |
| SL87-521      | 13.4            | 2.4       | 11.0       | 167.8       | 123.2              | 44.6        | 32.9     | 11.7 | 0                | 0         | 0.299   | 0.106 | 0.00         | 0.0            | 247                        |         |     |                      |                |              |
| SL87-527      | 13.7            | 2.2       | 11.5       | 165.6       | 118.6              | 47.0        | 35.6     | 11.4 | 0                | 0         | 0.310   | 0.099 | 0.00         | 0.0            | 245                        |         |     |                      |                |              |
| SL87-546      | 12.5            | 2.4       | 10.1       | 140.8       | 99.9               | 40.9        | 29.0     | 11.9 | 3                | 51        | 0.287   | 0.118 | 0.73         | 3.0            | 247                        |         |     |                      |                |              |
| SL87-547      | 12.8            | 1.8       | 11.0       | 170.5       | 119.1              | 51.4        | 37.8     | 13.6 | 0                | 0         | 0.344   | 0.124 | 0.00         | 0.0            | 214                        |         |     |                      |                |              |
| SL87-548      | 10.8            | 2.2       | 8.6        | 64.4        | 39.5               | 24.9        | 16.5     | 8.4  | 2                | 114       | 0.192   | 0.098 | 0.80         | 2.3            | 345                        |         |     |                      |                |              |
| SL87-551      | 12.3            | 3.6       | 8.7        | 113.5       | 86.8               | 26.7        | 17.6     | 9.1  | 0                | 0         | 0.202   | 0.105 | 0.00         | 0.0            | 326                        |         |     |                      |                |              |
| SL87-560      | 13.6            | 2.0       | 11.6       | 104.3       | 79.3               | 25.0        | 17.6     | 7.4  | 4                | 163       | 0.152   | 0.064 | 1.60         | 3.4            | 464                        |         |     |                      |                |              |
| GW89-008      | 13.2            | 3.5       | 9.7        | 227.6       | 198.1              | 29.5        | 20.1     | 9.4  | 0                | 0         | 0.207   | 0.103 | 0.00         | 0.0            | 329                        |         |     |                      |                |              |
| GW89-030B     | 14.8            | 7.1       | 7.7        | 139.9       | 108.2              | 31.7        | 23.8     | 7.9  | 1                | 207       | 0.309   | 0.097 | 0.32         | 1.3            | 243                        |         |     |                      |                |              |
| GW89-117      | 13.5            | 5.0       | 8.5        | 197.0       | 156.4              | 40.6        | 24.4     | 16.2 | 0                | 0         | 0.287   | 0.052 | 0.00         | 0.0            | 209                        |         |     |                      |                |              |
| GW89-159      | 13.3            | 5.0       | 8.3        | 224.9       | 151.1              | 73.8        | 45.5     | 28.3 | 1                | 299       | 0.548   | 0.029 | 0.14         | 1.2            | 112                        |         |     |                      |                |              |
| GW89-228      | 14.1            | 2.5       | 11.6       | 118.2       | 87.2               | 31.0        | 21.3     | 9.7  | 0                | 0         | 0.184   | 0.120 | 0.00         | 0.0            | 374                        |         |     |                      |                |              |
| GW89-229      | 15.1            | 7.3       | 7.8        | 95.9        | 77.7               | 18.2        | 12.4     | 5.8  | 0                | 0         | 0.159   | 0.134 | 0.00         | 0.0            | 429                        |         |     |                      |                |              |
| SL89-246      | 13.5            | 4.3       | 9.2        | 184.2       | 145.5              | 38.7        | 27.8     | 10.9 | 33               | 523       | 0.302   | 0.084 | 8.53         | 35.9           | 238                        |         |     |                      |                |              |
| Average       | 11.4            | 3.5       | 7.9        | 138.0       | 107.4              | 30.6        | 21.0     | 9.6  | 3                | 889       | 0.277   | 0.117 | 1.21         | 5.6            | 301                        |         |     |                      |                |              |
| Maximum       | 18.3            | 8.7       | 14.1       | 280.0       | 233.8              | 92.5        | 67.8     | 29.7 | 41               | 23621     | 0.792   | 0.423 | 25.79        | 186.4          | 1167                       |         |     |                      |                |              |
| Minimum       | 2.8             | 0.5       | 2.0        | 55.7        | 28.9               | 3.6         | 3.4      | 0.2  | 0                | 0         | 0.079   | 0.000 | 0.00         | 0.0            | 83                         |         |     |                      |                |              |
| Std.Dev.      | 2.8             | 1.7       | 2.7        | 46.9        | 41.8               | 15.9        | 10.9     | 5.4  | 6                | 2715      | 0.128   | 0.069 | 2.45         | 16.7           | 139                        |         |     |                      |                |              |

AULTMAN SAMPLES, CHURCHILL TOWNSHIP

| Sample Number | Weight (kg wet) |           |            | Weight (grams dry) |             |             |          | M.I. Concentrate |          | Au        |         | Weight % of Heavy Fraction |              | Normalized Au Grains |              |
|---------------|-----------------|-----------|------------|--------------------|-------------|-------------|----------|------------------|----------|-----------|---------|----------------------------|--------------|----------------------|--------------|
|               | Table Split     | +10 Chips | Table Feed | Table Conc.        | M.I. Lights | Conc. Total | Non Mag. | Mag.             | No. V.G. | Calc. ppb | Non Mag | Mag                        | Per 10 g HMC | Per 10 kg Feed       | Conc. Factor |
| JTA-1         | 14.77           | 5.49      | 9.28       | 54.6               | 37.3        | 28.2        | 26.0     | 2.2              | 0        | 0         | 0.280   | 0.024                      | 0.00         | 0.0                  | 329          |
| JTA-2         | 15.43           | 6.19      | 9.24       | 46.5               | 30.2        | 46.5        | 41.7     | 4.8              | 1        | 13912     | 0.451   | 0.052                      | 0.22         | 1.1                  | 199          |
| JTA-3B        | 10.0            | 3.0       | 7.0        | 131.6              | 107.4       | 24.2        | 16.0     | 8.2              | 4        | 27        | 0.229   | 0.117                      | 1.65         | 5.7                  | 289          |
| JTA-7         | 9.8             | 3.8       | 6.0        | 105.5              | 87.8        | 17.7        | 11.6     | 6.1              | 6        | 130       | 0.193   | 0.102                      | 3.39         | 10.0                 | 339          |
| JTA-8A        | 5.9             | 1.7       | 4.2        | 91.5               | 75.4        | 16.1        | 11.1     | 5.0              | 0        | 0         | 0.264   | 0.119                      | 0.00         | 0.0                  | 261          |
| JTA-9         | 5.7             | 2.0       | 3.7        | 67.7               | 59.3        | 8.4         | 6.3      | 2.1              | 2        | 115       | 0.170   | 0.057                      | 2.38         | 5.4                  | 440          |
| JTA-11        | 9.9             | 3.2       | 6.7        | 138.8              | 115.7       | 23.1        | 14.7     | 8.4              | 3        | 1519      | 0.219   | 0.125                      | 1.30         | 4.5                  | 290          |
| JTA-12        | 7.7             | 2.8       | 4.9        | 100.0              | 83.9        | 16.1        | 11.0     | 5.1              | 2        | 36        | 0.224   | 0.104                      | 1.24         | 4.1                  | 304          |
| JTA-14        | 10.7            | 5.5       | 5.2        | 127.9              | 115.5       | 12.4        | 8.6      | 3.8              | 18       | 472       | 0.165   | 0.073                      | 14.52        | 34.6                 | 419          |
| JTA-17        | 9.0             | 3.3       | 5.7        | 95.8               | 81.0        | 14.8        | 9.7      | 5.1              | 8        | 136       | 0.170   | 0.089                      | 5.41         | 14.0                 | 385          |
| Average       | 9.9             | 3.7       | 6.2        | 96                 | 79.4        | 20.8        | 15.7     | 5.1              | 4.4      | 1634.7    | 0.237   | 0.086                      | 3            | 7.9                  | 325.6        |

## APPENDIX C

### Heavy Mineral Grain Counts

A 100 point count of the heavy mineral concentrate was carried out using the line scan method, with an inspection of the entire sample for the presence of indicator or accessory minerals. The mineral abbreviations are as follows:

|    |            |    |                  |
|----|------------|----|------------------|
| GT | Garnet     | SE | Sphene           |
| EP | Epidote    | SR | Staurolite       |
| PX | Pyroxine   | GO | Goethite         |
| HB | Hornblende | KY | Kyanite          |
| IL | Ilmenite   | QF | Quartz, Feldspar |
| HM | Hematite   |    |                  |
| PY | Pyrite     |    |                  |
| RT | Rutile     |    |                  |
| ZR | Zircon     |    |                  |

APPENDIX C: Heavy mineral grain counts, Shining Tree area

| Sample    | GT | EP | PX | HB | IL | HM | PY | RT | ZR | SE | SR | GO | KY | QF | Remarks From Tabling, Panning and Microscopic Examination |
|-----------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|---|
| BI186-1   | 27 | 35 | 13 | 11 | 4  | 10 | -T | T  |    | -T |    |    |    |    |   |
| BI186-2   | 24 | 44 | 15 | 7  | 4  | 6  | -T | -T |    | T  |    |    |    |    |   |
| BI186-5   | 23 | 31 | 18 | 7  | 6  | 14 |    | 1  |    | -T |    |    |    |    |   |
| ST86-005  | 28 | 34 | 11 | 17 | 2  | 6  | 2  |    |    | 2  |    |    |    | 5  | No Sulphides  |
| ST86-006A | 27 | 31 | 10 | 27 | 0  | 4  | -T | -T | 1  | -T |    |    |    | 3  |   |
| ST86-006B | 22 | 52 | 10 | 13 | 1  | 1  |    | 1  | -T | 1  |    |    |    | 2  |   |
| ST86-009  | 35 | 37 | 11 | 13 | 1  | 2  |    | 1  |    | -T |    |    |    | 3  | No Sulphides  |
| ST86-015  | 22 | 42 | 17 | 15 | 0  | 4  |    | -T |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-016  | 21 | 36 | 21 | 15 | 1  | 6  | -T | -T |    | -T |    | T  |    | 2  | No Sulphides  |
| ST86-021  | 16 | 47 | 12 | 19 | 0  | 5  |    | 1  |    | -T |    |    |    | 2  | No Sulphides  |
| ST86-024  | 37 | 35 | 9  | 13 | 1  | 4  |    | 1  |    | T  |    |    |    | 2  | No Sulphides  |
| ST86-027  | 25 | 48 | 8  | 15 | 2  | 2  |    | -T |    | -T |    |    |    | 6  | No Sulphides  |
| ST86-030  | 26 | 48 | 14 | 6  | 0  | 5  |    | 1  |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-033  | 18 | 58 | 6  | 17 | 0  | 1  | -T | 1  |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-037  | 28 | 31 | 16 | 18 | 1  | 5  |    | 1  |    | -T |    |    |    | 9  | No Sulphides  |
| ST86-039  | 29 | 34 | 19 | 16 | 0  | 1  | -T | 1  |    | -T |    |    |    | 4  | No Sulphide   |
| ST86-042  | 28 | 38 | 17 | 8  | 2  | 7  |    | 1  | -T |    |    |    |    | 1  | No Sulphides  |
| ST86-043  | 24 | 45 | 12 | 15 | 1  | 3  |    | -T |    | -T |    |    |    | 4  | No Sulphides  |
| ST86-048  | 26 | 41 | 15 | 15 | 1  | 2  |    | -T |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-049  | 26 | 46 | 12 | 12 | 0  | 3  |    | 1  |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-057  | 15 | 61 | 8  | 15 | 0  | 1  |    | 1  |    | 1  |    |    |    | 2  | No Sulphides  |
| ST86-059  | 27 | 42 | 15 | 14 | 0  | 1  |    | -T |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-060  | 21 | 42 | 20 | 12 | 1  | 4  |    | 1  |    | -T |    |    |    | 2  | No Sulphides  |
| ST86-063  | 28 | 41 | 15 | 11 | 1  | 2  | 1  | -T |    | 1  |    |    |    | 1  | No Sulphides  |
| ST86-067  | 16 | 48 | 18 | 14 | 1  | 3  |    | 1  |    | 1  |    |    |    | 2  | No Sulphides  |
| ST86-068  | 7  | 70 | 8  | 12 | 0  | 3  |    | -T |    | -T |    |    |    | 2  | No Sulphides  |
| ST86-069  | 13 | 54 | 15 | 17 | 0  | T  |    | 1  |    | 1  |    |    |    | 1  | No Sulphides  |
| ST86-070  | 19 | 50 | 11 | 15 | 0  | 4  |    | 1  |    | 1  |    |    |    | 1  | No Sulphides  |
| ST86-072B | 7  | 68 | 12 | 12 | 0  | 1  |    | -T |    | -T |    |    |    | 7  | No Sulphides  |
| ST86-072C | 34 | 30 | 18 | 13 | 2  | 3  |    | -T |    | -T |    |    |    | 2  | No Sulphides  |
| ST86-074  | 22 | 43 | 14 | 18 | 1  | 2  |    | T  |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-076  | 22 | 53 | 10 | 10 | 2  | 3  |    | -T |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-077A | 37 | 36 | 13 | 12 | 1  | 1  |    | -T |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-077B | 32 | 32 | 21 | 10 | 1  | 3  |    | 1  |    | T  |    |    |    | 1  | No Sulphides  |
| ST86-079  | 25 | 32 | 12 | 21 | 3  | 6  |    | 1  |    | 1  |    |    |    | 1  | No Sulphides  |
| ST86-081  | 32 | 35 | 9  | 18 | 0  | 5  |    | 1  |    | 1  |    |    |    | 3  | No Sulphides  |
| ST86-082  | 21 | 48 | 15 | 13 | 0  | 2  |    | 1  |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-083  | 22 | 44 | 14 | 17 | 1  | 2  |    | -T |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-084  | 28 | 46 | 10 | 12 | 1  | 3  | T  | 1  |    | -T |    |    |    | 1  | No Sulphides  |
| ST86-085  | 18 | 54 | 12 | 14 | 0  | 1  | -T | 1  |    | -T |    |    |    | 1  | No Sulphides  |

Remarks From  
Tabling Panning  
and Microscopic  
Examination

| Sample    | GT | EP | PX | HB | IL | HM | PY | RT | ZR | SE | SR | GO | KY | QF | Remarks      |
|-----------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|--------------|
| ST86-087  | 21 | 35 | 18 | 18 | 4  | 4  |    |    | -T | -T |    |    |    | 3  | No Sulphides |
| ST86-088  | 20 | 47 | 13 | 15 | 3  | 2  |    | -T |    | -T |    |    |    | 1  | No Sulphides |
| ST86-089  | 19 | 54 | 11 | 14 | 0  | 2  |    |    |    |    |    |    |    | 1  | No Sulphides |
| ST86-090  | 20 | 39 | 6  | 27 | 1  | 7  | T  |    |    | -T |    |    |    | 1  | No Sulphides |
| ST86-100  | 15 | 51 | 18 | 12 | 2  | 2  |    | -T |    | -T |    |    |    | 2  | No Sulphides |
| ST86-101  | 20 | 40 | 21 | 14 | 2  | 3  |    | T  |    | -T |    |    |    | 2  | No Sulphides |
| ST86-102  | 28 | 32 | 21 | 10 | 3  | 6  |    | -T |    | -T |    |    |    | 4  | No Sulphides |
| ST86-103  | 20 | 50 | 8  | 11 | 4  | 4  |    | T  |    | -T |    |    |    | 1  | No Sulphides |
| ST86-104  | 12 | 53 | 11 | 15 | 1  | 8  |    | T  |    | -T |    |    |    | 3  | No Sulphides |
| ST86-105  | 26 | 32 | 19 | 13 | 1  | 9  |    | T  |    | -T |    |    |    | 3  | No Sulphides |
| ST86-106  | 6  | 63 | 12 | 14 | 1  | 4  |    | -T |    |    |    |    |    | 4  | No Sulphides |
| ST86-107A | 21 | 34 | 24 | 15 | 1  | 3  |    | 1  |    | 1  |    |    |    | 1  | No Sulphides |
| ST86-107B | 19 | 46 | 20 | 14 | 0  | 1  |    | T  |    | -T |    |    |    | 8  | No Sulphides |
| ST86-108A | 23 | 40 | 18 | 11 | 3  | 5  |    | T  |    | T  |    |    |    | 5  | No Sulphides |
| ST86-108B | 22 | 45 | 21 | 9  | 1  | 2  |    | T  |    | T  |    |    |    | 4  | No Sulphides |
| ST86-109  | 31 | 45 | 9  | 10 | 1  | 4  |    | T  |    | -T |    |    |    | 3  | No Sulphides |
| ST86-110  | 26 | 34 | 16 | 18 | 1  | 3  |    | 1  |    | -T |    |    |    | 5  | No Sulphides |
| ST86-111  | 20 | 38 | 17 | 21 | 1  | 3  |    | -T |    | -T |    |    |    | 3  | No Sulphides |
| ST86-112  | 20 | 45 | 20 | 5  | 2  | 7  | 1  |    |    | -T |    |    |    | 5  | No Sulphides |
| ST86-113  | 13 | 61 | 14 | 8  | 0  | 4  |    | -T |    | -T |    |    |    | 1  | No Sulphides |
| ST86-114  | 29 | 31 | 18 | 8  | 5  | 9  |    | -T |    | T  |    |    |    | 8  | No Sulphides |
| ST86-115  | 3  | 75 | 6  | 13 | 0  | 3  |    | -T |    | -T |    |    |    | 4  | No Sulphides |
| ST86-116  | 14 | 64 | 7  | 11 | 1  | 2  |    | 1  |    | -T |    |    |    | 3  | No Sulphides |
| ST86-117  | 17 | 48 | 24 | 10 | 0  | 1  | T  |    |    | -T |    |    |    | 5  | No Sulphides |
| ST86-118  | 19 | 46 | 19 | 11 | 1  | 4  |    | T  |    |    |    |    |    |    | No Sulphides |
| ST86-119  | 20 | 45 | 22 | 7  | 1  | 5  |    | -T |    | -T |    |    |    |    | No Sulphides |
| ST86-120  | 29 | 26 | 19 | 14 | 3  | 9  |    | T  |    | T  |    |    |    |    | No Sulphides |
| ST86-121  | 23 | 47 | 16 | 11 | 0  | 3  |    | -T |    | -T |    |    |    |    | No Sulphides |
| ST86-122  | 34 | 28 | 13 | 10 | 6  | 8  |    |    |    | 1  |    |    |    |    | No Sulphides |
| ST86-123  | 32 | 33 | 21 | 9  | 1  | 2  |    | -T |    | -T |    |    |    |    | No Sulphides |
| ST86-124  | 12 | 48 | 14 | 18 | 3  | 5  |    | -T |    | -T |    |    |    |    | No Sulphides |
| ST86-125  | 28 | 37 | 17 | 13 | 2  | 3  |    | -T |    | -T |    |    |    |    | No Sulphides |
| BI187-1B  | 33 | 24 | 10 | 17 | 4  | 9  |    | T  |    | 3  |    |    |    | 15 | No Sulphides |
| BI187-2B  | 33 | 22 | 8  | 12 | 9  | 12 |    | 1  |    | 2  |    |    |    | 15 | No Sulphides |
| BI187-4B  | 42 | 25 | 7  | 12 | 5  | 7  |    | T  |    | 3  |    |    | 1  | 15 | No Sulphides |
| BI187-5B  | 29 | 21 | 15 | 13 | 10 | 10 |    | 1  |    | 1  |    |    |    | 20 | No Sulphides |
| BI187-6   | 37 | 24 | 4  | 11 | 7  | 10 |    | 3  |    | 2  |    | T  |    | 16 | No Sulphides |
| BI187-7A  | 39 | 30 | 5  | 5  | 9  | 8  |    | 1  |    | 3  |    |    |    | 9  | No Sulphides |
| BI187-9   | 25 | 22 | 12 | 15 | 9  | 11 |    | 3  |    | 2  |    |    |    | 10 | No Sulphides |
| BI187-10B | 33 | 31 | 7  | 7  | 9  | 11 |    | 1  |    | 1  |    |    |    | 13 | No Sulphides |
| BI187-11B | 37 | 20 | 10 | 14 | 5  | 10 |    | 3  |    | 1  |    |    |    | 6  | No Sulphides |

**Remarks From  
Tabling, Panning  
and Microscopic  
Examination**

| Sample    | GT | EP | PX | HB | IL | HM | PY | RT | ZR | SE | SR | GO | KY | QF | Remarks      |
|-----------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|--------------|
| BI187-12A | 40 | 25 | 12 | 6  | 9  | 6  |    | 1  | T  | 1  |    | T  |    | 17 | No Sulphides |
| BI187-12B | 43 | 19 | 8  | 11 | 6  | 10 |    | 1  | T  | 2  |    |    |    | 17 | No Sulphides |
| BI187-13  | 27 | 21 | 18 | 12 | 7  | 11 |    | 2  | 1  | 1  |    | T  |    | 10 | No Sulphides |
| SL87-011  | 39 | 26 | 10 | 10 | 3  | 8  | -T | 2  | 2  | T  |    | -T |    | 7  | No Sulphides |
| SL87-012  | 30 | 29 | 9  | 12 | 6  | 9  |    | 3  | T  | 2  |    |    |    | 9  | No Sulphides |
| SL87-013  | 30 | 26 | 14 | 9  | 7  | 11 |    | 1  | 1  | 1  |    | T  |    | 11 | No Sulphides |
| SL87-016  | 44 | 23 | 11 | 6  | 6  | 9  |    | T  | 1  | T  |    |    |    | 15 | No Sulphides |
| SL87-018  | 37 | 31 | 9  | 10 | 5  | 6  |    | 1  | 1  | 1  |    |    |    | 25 | No Sulphides |
| SL87-022  | 41 | 20 | 10 | 9  | 6  | 9  |    | 1  | 1  | 2  | 1  |    |    | 13 | No Sulphides |
| SL87-036  | 41 | 18 | 13 | 8  | 6  | 12 |    | T  | 1  | 1  |    |    |    | 14 | No Sulphides |
| SL87-038  | 39 | 16 | 21 | 5  | 12 | 7  |    | T  | T  | T  |    |    |    | 15 | No Sulphides |
| SL87-069  | 31 | 26 | 11 | 8  | 9  | 11 |    | 2  | T  | 2  |    |    |    | 10 | No Sulphides |
| SL87-075  | 38 | 28 | 7  | 2  | 10 | 10 |    | 3  | T  | 2  | T  |    |    | 11 | No Sulphides |
| SL87-080  | 35 | 20 | 7  | 9  | 8  | 16 |    | 1  | 3  | 1  |    |    |    | 10 | No Sulphides |
| SL87-082  | 41 | 20 | 8  | 5  | 11 | 11 |    | 1  | T  | 3  |    |    |    | 6  | No Sulphides |
| SL87-086  | 32 | 23 | 15 | 8  | 10 | 7  |    | 1  | 1  | 3  |    |    |    | 5  | No Sulphides |
| SL87-090  | 22 | 29 | 8  | 17 | 9  | 11 |    | 2  | 1  | 1  |    |    |    | 8  | No Sulphides |
| SL87-096  | 41 | 23 | 6  | 10 | 11 | 7  |    | T  | 1  | 1  | T  |    |    | 10 | No Sulphides |
| SL87-098  | 24 | 31 | 6  | 5  | 9  | 18 |    | 3  | 2  | 1  | 1  |    |    | 12 | No Sulphides |
| SL87-100  | 37 | 31 | 9  | 6  | 9  | 5  |    | 1  | T  | 2  |    | T  |    | 10 | No Sulphides |
| SL87-102  | 27 | 33 | 9  | 17 | 5  | 5  |    | 2  | T  | 2  |    |    |    | 12 | No Sulphides |
| SL87-105  | 35 | 34 | 3  | 11 | 8  | 5  |    | T  | 2  | 2  |    |    |    | 10 | No Sulphides |
| SL87-107  | 26 | 45 | 8  | 11 | 3  | 3  |    | 2  | T  | 2  |    |    |    | 11 | No Sulphides |
| SL87-132  | 33 | 21 | 11 | 14 | 8  | 12 |    | T  | T  | 1  |    |    |    | 11 | No Sulphides |
| SL87-134  | 29 | 34 | 19 | 4  | 3  | 5  |    | 2  | 1  | 2  |    |    |    | 7  | No Sulphides |
| SL87-141  | 31 | 29 | 7  | 11 | 11 | 9  |    | 1  | 1  | T  |    |    |    | 11 | No Sulphides |
| SL87-157  | 24 | 19 | 15 | 5  | 10 | 11 |    | T  | T  | 2  |    |    |    | 15 | No Sulphides |
| SL87-161  | 40 | 29 | 10 | 5  | 8  | 6  |    | 2  | T  | 2  |    | T  |    | 11 | No Sulphides |
| SL87-164  | 29 | 33 | 12 | 7  | 5  | 8  |    | 3  | 1  | 2  |    |    |    | 12 | No Sulphides |
| SL87-219A | 29 | 27 | 8  | 13 | 5  | 14 |    | 2  | 1  | 1  |    |    |    | 13 | No Sulphides |
| SL87-229  | 31 | 30 | 12 | 10 | 8  | 9  |    | T  | T  | T  |    |    |    | 10 | No Sulphides |
| SL87-272  | 32 | 28 | 11 | 7  | 12 | 6  |    | T  | 1  | 3  |    |    |    | 10 | No Sulphides |
| SL87-290  | 29 | 35 | 17 | 13 | 2  | 3  |    | T  | 1  | T  |    | T  |    | 13 | No Sulphides |
| SL87-322  | 25 | 31 | 22 | 5  | 4  | 9  |    | 1  | T  | 3  |    |    |    | 9  | No Sulphides |
| SL87-353  | 30 | 20 | 13 | 17 | 6  | 11 |    | 3  | -T | T  |    |    |    | 12 | No Sulphides |
| SL87-356  | 32 | 17 | 10 | 19 | 7  | 9  |    | 2  | T  | 4  |    | T  |    | 11 | No Sulphides |
| SL87-357  | 32 | 20 | 17 | 17 | 5  | 8  |    | 1  | T  | T  |    |    |    | 10 | No Sulphides |
| SL87-358  | 36 | 24 | 5  | 7  | 9  | 13 |    | T  | 2  | 3  |    | 1  |    | 11 | No Sulphides |
| SL87-359  | 35 | 29 | 12 | 5  | 8  | 8  |    | 1  | T  | 1  |    |    |    | 8  | No Sulphides |
| SL87-361  | 38 | 26 | 10 | 9  | 7  | 8  |    | 2  | T  | T  |    |    |    | 11 | No Sulphides |
| SL87-363  | 40 | 36 | 6  | 4  | 3  | 10 |    | 1  | T  | T  |    |    |    | 8  | No Sulphides |

Remarks From  
Tabling, Panning  
and Microscopic  
Examination

| Sample  | GT   | EP   | PX   | HB   | IL    | HM   | PY | RT   | ZR   | SE   | SR   | GO   | KY | QF   | Remarks                 |
|---|------|------|------|------|-------|------|----|------|------|------|------|------|----|------|-------------------------|
| SL87-364  | 42   | 34   | 8    | 5    | 7     | 4    |    | T    | T    | T    |      |      |    | 10   |                         |
| SL87-394  | 42   | 21   | 11   | 5    | 8     | 9    |    | 3    | T    | 1    | T    | T    |    | 11   | No Sulphides            |
| SL87-411  | 21   | 45   | 13   | 8    | 2     | 5    |    | 1    | T    | 4    | 1    |      |    | 6    | No Sulphides            |
| SL87-412  | 29   | 43   | 9    | 7    | 3     | 7    |    |      | T    | 2    |      |      |    | 14   |                         |
| SL87-415  | 16   | 46   | 16   | 8    | 2     | 4    |    | 3    | 1    | 3    | 1    |      |    | 12   |                         |
| SL87-439  | 40   | 20   | 12   | 5    | 7     | 10   |    | 3    | 1    | 1    | 1    |      |    | 11   | No Sulphides            |
| SL87-440  | 32   | 21   | 12   | 8    | 9     | 11   |    | 1    | 2    | 4    |      | T    |    | 9    | No Sulphides            |
| SL87-521  | 36   | 22   | 13   | 12   | 5     | 9    |    | 2    | T    | 1    |      |      |    | 11   |                         |
| SL87-527  | 40   | 27   | 11   | 12   | 2     | 6    |    | T    | 1    | T    | 1    |      |    | 14   | No Sulphides            |
| SL87-546  | 38   | 20   | 14   | 10   | 6     | 8    |    | T    | T    | 4    | T    |      |    | 12   |                         |
| SL87-547  | 33   | 26   | 6    | 8    | 7     | 16   |    | T    | 1    | 2    | 1    |      |    | 10   | No Sulphides            |
| SL87-548  | 37   | 26   | 5    | 4    | 7     | 11   |    | 6    | T    | 4    |      |      |    | 6    | No Sulphides            |
| SL87-551  | 35   | 20   | 12   | 11   | 6     | 11   |    | 2    | 1    | 2    |      |      |    | 12   |                         |
| SL87-560  | 33   | 26   | 6    | 11   | 5     | 15   |    | 2    | 1    | 1    |      |      |    | 9    | No Sulphides            |
| SL89-246  | 33   | 26   | 21   | 5    | 7     | 7    |    | T    | T    | 1    |      | 1    |    | 1    | No Sulphides            |
| GW89-008  | 21   | 40   | 14   | 5    | 13    | 4    |    | -T   | 2    | 1    | -T   |      |    | -T   | See * Below             |
| GW89-030B                                       | 18   | 12   | 52   | 1    | 9     | 6    |    | 2    | 2    | -T   |      |      |    | 1    |                         |
| GW89-117  | 8    | 28   | 43   | 6    | 6     | 5    |    | 1    | 2    | 1    |      |      |    | -T   |                         |
| GW89-159  | 20   | 24   | 19   | 9    | 12    | 15   |    |      | 1    | T    |      |      |    | 1    |                         |
| GW89-228  | 18   | 26   | 30   | 3    | 7     | 13   |    |      | 3    |      |      |      |    | 3    |                         |
| GW89-229  | 27   | 22   | 28   | 7    | 7     | 7    |    |      | 2    |      |      |      |    | 1    |                         |
| AVERAGE   | 27.4 | 35.1 | 13.5 | 11.2 | 4.18  | 6.39 |    | 0.88 | 0.66 | 0.99 | 0.51 | 0.18 |    | 7.47 |                         |
| MANIMUM   | 44   | 75   | 52   | 27   | 13    | 18   |    | 6    | 3    | 4    | 14   | 1    |    | 25   |                         |
| MINIMUM   | 3    | 12   | 3    | 1    | 0     | 0    |    | 0    | 0    | 0    | 0    | 0    |    | 0    |                         |
| STD. DEV.                                       | 8.74 | 12.3 | 6.52 | 4.65 | 3.55  | 3.85 |    | 1.07 | 0.79 | 1.15 | 2.07 | 0.39 |    | 0    |                         |
| * Est. 0.5% Limonitized Pyrite, Sample Oxidized |      |      |      |      |       |      |    |      |      |      |      |      |    |      |                         |
| Aultman Samples, Churchill Township             |      |      |      |      |       |      |    |      |      |      |      |      |    |      |                         |
| JTA-3B  | 40   | 37   | 6    | 6    | 1     | 10   |    |      |      | T    | T    |      |    | 4    | no sulphides            |
| JTA-7   | 40   | 36   | 6    | 4    | 5     | 8    |    | T    |      | 1    |      |      |    | 1    | trace limonite from py. |
| JTA-8A  | 37   | 35   | 12   | 4    | 2     | 5    |    | 2    |      | T    |      | 3    |    | 3    | trace specular hematite |
| JTA-9   | 21   | 42   | 11   | 8    | 2     | 15   |    |      |      |      |      |      |    | 1    | no sulphides            |
| JTA-11  | 36   | 37   | 6    | 8    | 3     | 10   |    |      |      | T    |      | 1    |    | 3    | no sulphides            |
| JTA-12  | 37   | 35   | 10   | 6    | 3     | 7    |    |      |      | 1    | 1    |      |    | 2    | no sulphides            |
| JTA-14  | 35   | 31   | 13   | 7    | 2     | 11   |    | 1    |      | T    | T    |      |    | 4    | no sulphides            |
| JTA-17  | 39   | 32   | 9    | 4    | 4     | 12   |    | T    |      | T    | T    |      |    | 3    | no sulphides            |
| AVERAGE   | 35.6 | 35.6 | 9.12 | 5.87 | 22.75 | 9.75 |    | 0.75 | 0.66 | 0.28 | 0.25 | 2    |    | 2.57 |                         |
| MAXIMUM   | 40   | 42   | 13   | 8    | 5     | 15   |    | 2    | 3    | 1    | 1    | 3    |    | 4    |                         |
| MINIMUM   | 21   | 31   | 6    | 4    | 1     | 5    |    | 0    | 0    | 0    | 0    | 1    |    | 1    |                         |
| STD. DEV.                                       | 5.78 | 3.15 | 2.66 | 1.61 | 1.19  | 2.9  |    | 0.82 | 0.79 | 0.45 | 0.43 | 1    |    | 1.17 |                         |

## APPENDIX D

### Clast Lithological Composition of Till Samples

Clast lithology types were identified for approximately 100 clasts with long axis > 2 cm. The clasts were collected from till sample sites, washed and examined for glacial abrasion features and the constituent rock type. As the geologists identifying the clasts were different in each year, and the identification of small rock fragments is tentative, this data should only be used for general information on the till composition.

APPENDIX D: Clast lithology compositional data, Shining Tree area

| Sample     | Total Count | Felsic Intrus. | Int.-Maf Intrus. | Mafic Metavolc. | Fel.-Int. Metavolc. | Breccia-Tuff | Schistic | Archean Metaseds. ite | Quartzite | Banded Iron FM. | Sandstone | Siltstone Mudstone Slate | Conglom. | Chert | Limestone | Vein Quartz | Withd. Pebbles Other |
|------------|-------------|----------------|------------------|-----------------|---------------------|--------------|----------|-----------------------|-----------|-----------------|-----------|--------------------------|----------|-------|-----------|-------------|----------------------|
| BH86-1     | 100         | 2.0            | 10.0             | 16.0            | 58.0                | 0.0          | 0.0      | 0.0                   | 8.0       | 0.0             | 2.0       | 1.0                      | 0.0      | 2.0   | 0.0       | 0.0         | 1.0                  |
| ST186-005  | 108         | 3.7            | 22.2             | 19.4            | 45.4                | 0.0          | 3.7      | 0.0                   | 1.9       | 0.0             | 0.0       | 0.9                      | 1.9      | 0.0   | 0.0       | 0.0         | 0.9                  |
| ST186-006B | 98          | 4.0            | 14.3             | 25.5            | 28.6                | 2.0          | 5.1      | 0.0                   | 2.0       | 0.0             | 0.0       | 3.0                      | 3.0      | 0.0   | 0.0       | 0.0         | 12.2                 |
| ST186-009  | 101         | 3.0            | 10.9             | 26.7            | 21.8                | 7.9          | 0.0      | 0.0                   | 1.0       | 0.0             | 3.0       | 4.0                      | 5.9      | 0.0   | 0.0       | 0.0         | 15.8                 |
| ST186-015  | 99          | 6.0            | 12.1             | 22.2            | 24.2                | 1.0          | 0.0      | 0.0                   | 13.1      | 0.0             | 0.0       | 2.0                      | 15.0     | 0.0   | 0.0       | 0.0         | 3.0                  |
| ST186-016  | 105         | 4.8            | 18.0             | 31.4            | 17.1                | 1.9          | 0.0      | 0.0                   | 10.5      | 0.0             | 1.0       | 0.0                      | 9.5      | 0.0   | 0.0       | 1.0         | 4.8                  |
| ST186-021  | 80          | 2.5            | 20.0             | 20.0            | 43.8                | 1.3          | 1.3      | 0.0                   | 6.3       | 0.0             | 0.0       | 0.0                      | 1.3      | 0.0   | 0.0       | 0.0         | 3.8                  |
| ST186-024  | 100         | 7.0            | 10.0             | 17.0            | 29.0                | 1.0          | 0.0      | 0.0                   | 9.0       | 0.0             | 0.0       | 2.0                      | 13.0     | 0.0   | 0.0       | 0.0         | 11.0                 |
| ST186-027  | 91          | 5.5            | 20.9             | 20.9            | 27.5                | 0.0          | 0.0      | 0.0                   | 1.0       | 0.0             | 6.6       | 1.0                      | 15.4     | 0.0   | 0.0       | 0.0         | 0.0                  |
| ST186-030  | 100         | 2.0            | 0.0              | 6.0             | 76.0                | 2.0          | 5.0      | 0.0                   | 2.0       | 0.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 7.0                  |
| ST186-033  | 98          | 1.0            | 5.1              | 4.1             | 26.5                | 34.7         | 0.0      | 0.0                   | 7.1       | 0.0             | 1.0       | 2.0                      | 9.0      | 0.0   | 0.0       | 0.0         | 9.0                  |
| ST186-037  | 92          | 2.2            | 15.1             | 28.0            | 28.0                | 1.0          | 1.0      | 0.0                   | 1.0       | 0.0             | 1.0       | 7.2                      | 6.0      | 0.0   | 0.0       | 0.0         | 9.7                  |
| ST186-039  | 102         | 2.0            | 17.6             | 28.4            | 18.6                | 1.0          | 0.0      | 0.0                   | 16.7      | 0.0             | 1.0       | 1.0                      | 5.9      | 0.0   | 1.0       | 0.0         | 5.9                  |
| ST186-042  | 99          | 3.0            | 16.0             | 24.0            | 36.0                | 2.0          | 3.0      | 0.0                   | 1.0       | 0.0             | 0.0       | 0.0                      | 7.0      | 0.0   | 0.0       | 0.0         | 7.0                  |
| ST186-043  | 101         | 5.9            | 13.9             | 36.6            | 23.8                | 4.0          | 1.0      | 0.0                   | 2.1       | 0.0             | 0.0       | 3.1                      | 3.1      | 0.0   | 0.0       | 0.0         | 7.0                  |
| ST186-048  | 97          | 6.2            | 6.2              | 26.8            | 30.9                | 4.1          | 6.2      | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 3.1      | 0.0   | 1.0       | 1.0         | 10.3                 |
| ST186-049  | 103         | 2.9            | 9.7              | 16.5            | 33.0                | 1.9          | 5.8      | 0.0                   | 2.9       | 0.0             | 0.0       | 4.9                      | 4.9      | 0.0   | 0.0       | 1.9         | 12.6                 |
| ST186-057  | 95          | 63.2           | 16.8             | 5.3             | 2.1                 | 0.0          | 9.5      | 0.0                   | 2.1       | 0.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 1.1                  |
| ST186-059  | 102         | 1.0            | 38.2             | 39.2            | 5.9                 | 0.0          | 1.0      | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 14.7                 |
| ST186-060  | 102         | 3.9            | 21.6             | 10.8            | 20.6                | 0.0          | 2.9      | 0.0                   | 2.9       | 0.0             | 0.0       | 0.0                      | 2.0      | 0.0   | 0.0       | 0.0         | 35.3                 |
| ST186-063  | 100         | 70.0           | 17.0             | 0.0             | 1.0                 | 0.0          | 10.0     | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 1.0      | 0.0   | 1.0       | 0.0         | 0.0                  |
| ST186-067  | 87          | 43.7           | 17.2             | 10.3            | 17.2                | 0.0          | 2.3      | 0.0                   | 1.1       | 2.3             | 0.0       | 1.1                      | 3.4      | 0.0   | 0.0       | 0.0         | 1.1                  |
| ST186-068  | 97          | 34.0           | 37.1             | 11.8            | 8.2                 | 0.0          | 3.1      | 0.0                   | 2.1       | 0.0             | 2.1       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 2.1                  |
| ST186-069  | 103         | 5.8            | 15.5             | 31.1            | 34.0                | 0.0          | 3.9      | 0.0                   | 0.0       | 2.9             | 0.0       | 1.0                      | 0.0      | 0.0   | 0.0       | 1.9         | 3.9                  |
| ST186-070  | 101         | 28.7           | 13.9             | 13.9            | 29.7                | 1.0          | 7.9      | 0.0                   | 1.0       | 0.0             | 0.0       | 1.0                      | 1.0      | 0.0   | 1.0       | 2.0         | 0.0                  |
| ST186-072B | 91          | 13.2           | 12.1             | 19.8            | 31.9                | 0.0          | 7.7      | 0.0                   | 3.3       | 0.0             | 0.0       | 1.1                      | 2.2      | 0.0   | 0.0       | 0.0         | 8.8                  |
| ST186-072C | 100         | 13.0           | 10.0             | 31.0            | 28.0                | 0.0          | 3.0      | 0.0                   | 0.0       | 2.0             | 0.0       | 2.0                      | 2.0      | 0.0   | 0.0       | 0.0         | 10.0                 |
| ST186-074  | 104         | 13.5           | 4.8              | 7.7             | 20.2                | 26.0         | 0.0      | 0.0                   | 7.7       | 0.0             | 0.0       | 1.0                      | 6.8      | 0.0   | 0.0       | 0.0         | 12.5                 |
| ST186-076  | 108         | 5.6            | 9.3              | 37.0            | 18.5                | 0.0          | 9.3      | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 4.6      | 0.0   | 0.0       | 1.0         | 14.8                 |
| ST186-077A | 102         | 18.6           | 7.8              | 21.6            | 36.3                | 0.0          | 1.0      | 0.0                   | 0.0       | 3.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 11.8                 |
| ST186-079  | 98          | 14.3           | 7.1              | 34.7            | 25.5                | 0.0          | 3.1      | 0.0                   | 2.0       | 0.0             | 1.0       | 0.0                      | 4.1      | 0.0   | 1.0       | 0.0         | 7.1                  |
| ST186-081  | 102         | 13.7           | 8.8              | 34.3            | 23.5                | 0.0          | 4.9      | 0.0                   | 1.0       | 0.0             | 0.0       | 0.0                      | 3.9      | 0.0   | 0.0       | 0.0         | 9.8                  |
| ST186-082  | 98          | 20.4           | 12.2             | 23.4            | 22.4                | 1.0          | 4.1      | 0.0                   | 2.0       | 0.0             | 1.0       | 0.0                      | 2.0      | 0.0   | 0.0       | 0.0         | 11.2                 |
| ST186-083  | 101         | 10.9           | 8.9              | 31.7            | 36.6                | 1.0          | 1.0      | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 2.0      | 0.0   | 0.0       | 0.0         | 7.0                  |
| ST186-084  | 96          | 9.5            | 14.7             | 12.6            | 35.8                | 0.0          | 6.3      | 0.0                   | 0.0       | 0.0             | 0.0       | 1.0                      | 2.1      | 0.0   | 0.0       | 0.0         | 18.9                 |
| ST186-085  | 99          | 4.0            | 1.0              | 3.0             | 81.8                | 0.0          | 0.0      | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 10.1                 |
| ST186-087  | 100         | 3.0            | 10.0             | 16.0            | 56.0                | 0.0          | 1.0      | 0.0                   | 1.0       | 5.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 1.0         | 7.0                  |
| ST186-088  | 107         | 9.3            | 12.1             | 17.8            | 47.7                | 0.0          | 1.0      | 0.0                   | 0.0       | 1.9             | 0.0       | 0.0                      | 2.8      | 1.0   | 0.0       | 1.0         | 5.6                  |
| ST186-089  | 106         | 12.3           | 8.5              | 25.5            | 45.3                | 0.0          | 0.0      | 0.0                   | 0.9       | 0.9             | 0.0       | 0.0                      | 2.8      | 0.0   | 0.0       | 0.0         | 5.7                  |
| ST186-101  | 116         | 12.9           | 17.2             | 15.5            | 34.5                | 0.0          | 4.3      | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 0.0       | 0.0         | 12.9                 |
| ST186-103  | 98          | 19.4           | 8.2              | 20.4            | 41.8                | 0.0          | 1.0      | 0.0                   | 1.0       | 0.0             | 0.0       | 0.0                      | 2.0      | 0.0   | 0.0       | 0.0         | 6.1                  |
| ST186-104  | 99          | 11.1           | 17.2             | 13.1            | 23.2                | 2.0          | 9.1      | 0.0                   | 3.0       | 0.0             | 1.0       | 0.0                      | 2.0      | 0.0   | 1.0       | 1.0         | 15.2                 |
| ST186-105  | 105         | 17.1           | 17.0             | 14.3            | 16.2                | 1.0          | 13.3     | 0.0                   | 6.7       | 0.0             | 0.0       | 0.0                      | 5.7      | 0.0   | 0.0       | 1.0         | 7.6                  |
| ST186-107B | 101         | 49.5           | 11.9             | 9.9             | 9.9                 | 0.0          | 13.9     | 0.0                   | 1.0       | 0.0             | 1.0       | 0.0                      | 1.0      | 0.0   | 2.0       | 0.0         | 0.0                  |
| ST186-108A | 101         | 53.4           | 24.8             | 6.9             | 2.0                 | 1.0          | 6.9      | 0.0                   | 2.0       | 0.0             | 0.0       | 0.0                      | 0.0      | 0.0   | 1.0       | 0.0         | 2.0                  |
| ST186-109  | 93          | 6.4            | 17.2             | 29.0            | 21.5                | 1.1          | 4.3      | 0.0                   | 0.0       | 0.0             | 1.1       | 1.1                      | 6.4      | 0.0   | 0.0       | 0.0         | 11.8                 |

| Sample    | Total Count | Felsic Intrus. | Intl-Maf Intrus. | Mafic Metavolc. | Fel-Int. Metavolc. | Breccia-Tuff | Schistic | Archean Metaseds. ite | Quartz-ite | Banded Iron FM. | Sandstone | Siltstone Mudstone | Shale State | Conglom. Chert | Limestone | Vein Quartz | Withd. Pebbles Other |
|-----------|-------------|----------------|------------------|-----------------|--------------------|--------------|----------|-----------------------|------------|-----------------|-----------|--------------------|-------------|----------------|-----------|-------------|----------------------|
| SI86-110  | 96          | 9.4            | 17.7             | 11.4            | 33.3               | 0.0          | 12.5     | 0.0                   | 5.2        | 0.0             | 0.0       | 0.0                | 4.2         | 0.0            | 0.0       | 0.0         | 6.3                  |
| SI86-111  | 101         | 36.6           | 19.8             | 12.9            | 12.9               | 1.0          | 10.9     | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 2.0         | 0.0            | 0.0       | 0.0         | 4.0                  |
| SI86-112  | 109         | 2.8            | 11.0             | 23.9            | 33.0               | 0.0          | 6.4      | 0.0                   | 1.8        | 0.0             | 0.0       | 0.0                | 1.8         | 0.0            | 0.0       | 0.0         | 19.3                 |
| SI86-113  | 116         | 3.4            | 7.8              | 20.7            | 50.9               | 0.0          | 0.0      | 0.0                   | 0.0        | 5.2             | 0.0       | 0.0                | 1.7         | 0.0            | 0.0       | 3.4         | 6.9                  |
| SI86-114  | 102         | 9.8            | 3.9              | 30.4            | 40.2               | 0.0          | 1.0      | 0.0                   | 0.0        | 1.0             | 0.0       | 0.0                | 2.0         | 0.0            | 0.0       | 2.0         | 9.8                  |
| SI86-115  | 99          | 1.0            | 29.3             | 26.3            | 18.2               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 25.3                 |
| SI86-116  | 98          | 5.1            | 11.2             | 27.6            | 33.7               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 4.1         | 0.0            | 0.0       | 0.0         | 17.3                 |
| SI86-118  | 93          | 18.3           | 20.4             | 22.6            | 14.0               | 2.2          | 11.8     | 0.0                   | 1.0        | 0.0             | 1.1       | 5.4                | 2.2         | 0.0            | 0.0       | 1.1         | 0.0                  |
| SI86-121  | 101         | 4.0            | 18.8             | 24.8            | 21.8               | 0.0          | 5.9      | 0.0                   | 4.0        | 0.0             | 3.0       | 4.0                | 10.9        | 0.0            | 0.0       | 0.0         | 3.0                  |
| SI86-122  | 94          | 13.8           | 22.3             | 19.1            | 21.3               | 0.0          | 7.4      | 0.0                   | 4.3        | 1.1             | 3.2       | 0.0                | 5.3         | 0.0            | 0.0       | 0.0         | 2.2                  |
| SI86-123  | 114         | 19.1           | 25.2             | 19.1            | 19.1               | 0.9          | 3.5      | 0.0                   | 2.6        | 0.0             | 0.0       | 2.6                | 0.9         | 0.0            | 0.0       | 0.9         | 5.2                  |
| SI86-124  | 98          | 7.5            | 15.3             | 19.4            | 29.6               | 0.0          | 21.4     | 0.0                   | 1.0        | 0.0             | 0.0       | 0.0                | 3.0         | 0.0            | 0.0       | 1.0         | 0.0                  |
| SI86-125  | 95          | 5.3            | 16.8             | 21.0            | 23.2               | 0.0          | 0.0      | 0.0                   | 6.3        | 0.0             | 1.0       | 6.4                | 2.1         | 0.0            | 0.0       | 1.0         | 16.8                 |
| BI87-1A   | 116         | 21.6           | 7.8              | 30.2            | 19.8               | 0.9          | 0.0      | 0.0                   | 0.0        | 0.0             | 2.6       | 14.7               | 0.0         | 0.0            | 0.0       | 0.9         | 0.9                  |
| BI87-1B   | 136         | 16.9           | 6.6              | 35.3            | 33.1               | 1.5          | 0.0      | 0.0                   | 0.0        | 0.0             | 3.7       | 2.9                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| BI87-2A   | 98          | 20.4           | 18.4             | 10.2            | 22.4               | 1.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 8.2       | 19.4               | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| BI87-2B   | 116         | 24.1           | 9.5              | 25.0            | 14.7               | 4.3          | 0.0      | 0.0                   | 0.0        | 0.0             | 14.7      | 6.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| BI87-3    | 111         | 9.9            | 3.6              | 16.2            | 9.0                | 1.8          | 0.0      | 0.0                   | 3.6        | 0.0             | 18.9      | 36.9               | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| BI87-4B   | 109         | 17.4           | 11.9             | 15.6            | 16.5               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 16.5      | 17.4               | 2.8         | 0.0            | 0.0       | 1.8         | 0.0                  |
| BI87-5A   | 113         | 6.2            | 10.6             | 23.9            | 22.1               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 9.7       | 26.5               | 0.0         | 0.0            | 0.0       | 0.9         | 0.0                  |
| BI87-5B   | 106         | 8.5            | 6.6              | 17.9            | 16.0               | 0.9          | 0.0      | 0.0                   | 0.0        | 0.0             | 5.7       | 29.2               | 0.9         | 14.2           | 0.0       | 0.0         | 0.0                  |
| BI87-6    | 83          | 12.0           | 6.0              | 10.8            | 6.0                | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 18.1      | 32.5               | 13.3        | 1.2            | 0.0       | 0.0         | 0.0                  |
| BI87-7A   | 107         | 17.8           | 6.5              | 24.3            | 20.6               | 5.6          | 0.9      | 0.0                   | 6.5        | 0.0             | 4.7       | 7.5                | 0.0         | 5.6            | 0.0       | 0.0         | 1.3                  |
| BI87-7B   | 79          | 13.9           | 10.1             | 3.8             | 12.7               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 21.5      | 19.0               | 0.0         | 16.5           | 0.0       | 0.0         | 0.0                  |
| BI87-7C   | 101         | 8.9            | 3.0              | 5.0             | 9.9                | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 9.9       | 53.5               | 4.0         | 5.9            | 0.0       | 0.0         | 0.0                  |
| BI87-9    | 105         | 41.0           | 0.0              | 18.1            | 27.6               | 0.0          | 1.0      | 0.0                   | 1.0        | 0.0             | 2.9       | 6.7                | 1.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| BI87-10B  | 115         | 10.4           | 9.6              | 19.1            | 36.3               | 5.2          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.9       | 13.9               | 0.0         | 0.0            | 0.0       | 0.9         | 1.7                  |
| BI87-11B  | 114         | 14.0           | 4.4              | 15.8            | 62.3               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 3.5                  |
| BI87-12A  | 100         | 12.0           | 19.0             | 12.0            | 24.0               | 4.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 11.0      | 18.0               | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| BI87-12B  | 99          | 18.2           | 10.1             | 21.2            | 24.2               | 4.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 15.2      | 0.0                | 5.1         | 0.0            | 1.0       | 1.0         | 0.0                  |
| BI87-13   | 95          | 2.1            | 0.0              | 3.2             | 43.2               | 13.7         | 0.0      | 0.0                   | 0.0        | 0.0             | 17.9      | 0.0                | 0.0         | 20.0           | 0.0       | 0.0         | 0.0                  |
| SI87-007  | 133         | 18.0           | 19.5             | 21.8            | 25.6               | 0.0          | 1.5      | 0.0                   | 0.0        | 0.0             | 3.8       | 7.5                | 0.0         | 0.0            | 0.0       | 0.0         | 2.3                  |
| SI87-009  | 111         | 12.6           | 11.7             | 28.8            | 33.3               | 0.0          | 10.8     | 0.0                   | 0.0        | 0.0             | 1.8       | 0.9                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-011  | 105         | 1.9            | 78.1             | 6.7             | 11.4               | 1.9          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-013  | 91          | 12.1           | 17.6             | 22.0            | 12.1               | 0.0          | 0.0      | 0.0                   | 36.3       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-069  | 102         | 23.5           | 13.7             | 29.4            | 20.6               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-075  | 88          | 20.5           | 13.6             | 20.5            | 3.4                | 0.0          | 0.0      | 0.0                   | 6.8        | 0.0             | 0.0       | 3.9                | 8.8         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-080  | 94          | 26.6           | 10.6             | 28.7            | 2.1                | 0.0          | 0.0      | 0.0                   | 5.3        | 25.5            | 0.0       | 35.2               | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-082  | 100         | 22.8           | 0.0              | 30.7            | 21.8               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 14.9               | 8.9         | 0.0            | 0.0       | 0.0         | 1.1                  |
| SI87-086  | 109         | 16.5           | 7.3              | 34.9            | 35.8               | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 5.5                | 0.0         | 0.0            | 0.0       | 0.0         | 0.9                  |
| SI87-090  | 104         | 14.4           | 12.5             | 13.5            | 12.5               | 0.0          | 0.0      | 0.0                   | 31.7       | 1.9             | 2.9       | 6.7                | 1.0         | 0.0            | 0.0       | 0.0         | 2.9                  |
| SI87-096  | 91          | 17.6           | 4.4              | 13.2            | 51.6               | 2.2          | 0.0      | 0.0                   | 0.0        | 0.0             | 1.1       | 5.5                | 4.4         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-098  | 87          | 0.0            | 16.1             | 27.6            | 35.6               | 13.8         | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 6.9                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-100  | 99          | 17.2           | 8.1              | 13.1            | 52.5               | 2.0          | 0.0      | 0.0                   | 4.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-102  | 169         | 55.0           | 23.7             | 10.1            | 5.3                | 0.0          | 1.2      | 3.6                   | 0.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.6         | 3.0                  |
| SI87-105  | 103         | 46.6           | 30.1             | 15.5            | 0.0                | 0.0          | 0.0      | 0.0                   | 7.8        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |
| SI87-107  | 108         | 39.8           | 40.7             | 11.1            | 4.6                | 0.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 1.9                | 0.0         | 0.0            | 0.0       | 1.9         | 0.0                  |
| SI87-132  | 97          | 26.8           | 10.3             | 14.4            | 17.5               | 0.0          | 0.0      | 0.0                   | 26.8       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 4.1                  |
| SI87-133A | 101         | 52.5           | 7.9              | 15.8            | 22.8               | 1.0          | 0.0      | 0.0                   | 0.0        | 0.0             | 0.0       | 0.0                | 0.0         | 0.0            | 0.0       | 0.0         | 0.0                  |

| Sample     | Total Count | Felsic Intrus. | Int.-Maf Intrus. | Mafic Metavolc. | Fel.-Int. Metavolc. | Breccia-Tuff | Schistitic | Archean Metascds. ite | Quartzite | Banded Iron FM. | Sandstone | Siltstone Mudstone | Shale Slate | Conglom. | Chert | Limestone | Vein Quartz | Withd. Pebbles | Other |
|------------|-------------|----------------|------------------|-----------------|---------------------|--------------|------------|-----------------------|-----------|-----------------|-----------|--------------------|-------------|----------|-------|-----------|-------------|----------------|-------|
| SI.87-134  | 91          | 51.6           | 24.2             | 19.8            | 1.1                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 2.2       | 1.1                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-136  | 110         | 44.5           | 20.9             | 24.5            | 7.3                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 2.7   |
| SI.87-141  | 94          | 14.9           | 8.5              | 8.5             | 51.1                | 6.4          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 10.6               | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-157  | 92          | 4.3            | 3.3              | 4.3             | 5.4                 | 81.5         | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-164  | 101         | 74.3           | 14.9             | 3.0             | 7.9                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-219A | 93          | 7.5            | 8.6              | 14.0            | 29.0                | 2.2          | 1.1        | 0.0                   | 0.0       | 0.0             | 1.1       | 5.4                | 6.5         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-219B | 100         | 21.0           | 0.0              | 13.0            | 31.0                | 1.0          | 1.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 30.0               | 4.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-221  | 96          | 9.4            | 8.3              | 10.4            | 5.2                 | 0.0          | 1.0        | 0.0                   | 0.0       | 0.0             | 24.0      | 33.3               | 0.0         | 0.0      | 0.0   | 2.1       | 0.0         | 1.0            | 0.0   |
| SI.87-229  | 97          | 9.3            | 7.2              | 8.2             | 11.3                | 4.1          | 0.0        | 0.0                   | 0.0       | 0.0             | 24.7      | 23.7               | 0.0         | 10.3     | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-272  | 92          | 29.3           | 2.2              | 21.7            | 29.3                | 3.3          | 1.1        | 0.0                   | 0.0       | 0.0             | 7.6       | 1.1                | 4.3         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-290  | 106         | 37.7           | 18.9             | 12.3            | 14.2                | 0.0          | 3.8        | 0.0                   | 0.0       | 0.0             | 1.9       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.9         | 3.8            | 0.0   |
| SI.87-322  | 86          | 33.7           | 9.3              | 34.9            | 7.0                 | 0.0          | 5.8        | 0.0                   | 0.0       | 0.0             | 1.2       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 8.1            | 0.0   |
| SI.87-353  | 108         | 22.2           | 13.0             | 36.1            | 22.2                | 0.9          | 0.0        | 0.0                   | 0.0       | 0.0             | 2.8       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 2.8            | 0.0   |
| SI.87-356  | 93          | 16.1           | 1.1              | 19.4            | 14.0                | 5.4          | 0.0        | 0.0                   | 0.0       | 0.0             | 10.8      | 30.1               | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 1.1            | 1.1   |
| SI.87-357  | 111         | 9.0            | 14.4             | 9.0             | 27.9                | 2.7          | 1.8        | 0.0                   | 0.0       | 0.0             | 2.7       | 15.3               | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 4.5            | 0.0   |
| SI.87-358  | 111         | 18.0           | 8.1              | 16.2            | 36.0                | 3.6          | 0.0        | 0.0                   | 0.0       | 0.0             | 4.5       | 12.6               | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.9            | 0.0   |
| SI.87-361  | 111         | 10.8           | 6.3              | 13.5            | 17.1                | 1.8          | 1.8        | 0.0                   | 0.0       | 0.0             | 5.4       | 18.9               | 1.8         | 5.4      | 0.0   | 0.0       | 0.0         | 0.9            | 0.0   |
| SI.87-383  | 106         | 75.5           | 15.1             | 9.4             | 0.0                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-394  | 93          | 2.2            | 7.5              | 8.6             | 9.7                 | 1.1          | 0.0        | 0.0                   | 0.0       | 0.0             | 30.1      | 34.4               | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 1.1            | 5.4   |
| SI.87-395  | 98          | 6.1            | 6.1              | 3.1             | 23.5                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 19.4      | 35.7               | 0.0         | 5.1      | 1.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-411  | 89          | 78.7           | 1.1              | 5.6             | 12.4                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 1.1       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 1.1         | 0.0            | 0.0   |
| SI.87-412  | 108         | 70.4           | 12.0             | 5.6             | 5.6                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.9                | 0.0         | 0.9      | 0.0   | 0.0       | 0.0         | 0.9            | 0.0   |
| SI.87-415  | 102         | 77.5           | 13.7             | 4.9             | 0.0                 | 0.0          | 3.9        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-416  | 80          | 87.5           | 6.3              | 1.3             | 5.0                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-418  | 103         | 51.5           | 25.2             | 10.7            | 6.8                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 4.9       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 1.0            | 0.0   |
| SI.87-439  | 101         | 11.9           | 4.0              | 38.6            | 35.6                | 2.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 5.0       | 3.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-440  | 107         | 14.0           | 5.6              | 24.3            | 48.6                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.9       | 5.6                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.9            | 0.0   |
| SI.87-517  | 124         | 47.6           | 13.7             | 12.1            | 16.9                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.5       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 2.4         | 0.8            | 0.0   |
| SI.87-518  | 111         | 55.0           | 16.2             | 6.3             | 11.7                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 9.0       | 0.0                | 0.0         | 1.8      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-521  | 116         | 13.8           | 17.2             | 20.7            | 28.4                | 0.0          | 0.9        | 0.0                   | 0.0       | 0.0             | 4.3       | 9.5                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 5.2            | 0.0   |
| SI.87-527  | 102         | 26.5           | 10.8             | 12.7            | 0.0                 | 47.1         | 1.0        | 0.0                   | 0.0       | 0.0             | 1.0       | 0.0                | 0.0         | 0.0      | 1.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-528  | 111         | 84.7           | 9.9              | 2.7             | 1.8                 | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.9         | 0.0            | 0.0   |
| SI.87-546  | 103         | 21.4           | 7.8              | 24.3            | 26.2                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 0.0       | 6.8                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 2.9            | 0.0   |
| SI.87-547  | 93          | 32.8           | 14.0             | 18.3            | 23.7                | 1.1          | 1.1        | 0.0                   | 0.0       | 0.0             | 4.3       | 4.3                | 1.1         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-548  | 101         | 23.8           | 6.9              | 4.0             | 33.7                | 19.8         | 2.0        | 0.0                   | 0.0       | 0.0             | 5.9       | 1.0                | 0.0         | 0.0      | 1.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| SI.87-551  | 104         | 14.4           | 9.6              | 44.2            | 20.2                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 1.9       | 0.0                | 7.7         | 0.0      | 0.0   | 0.0       | 0.0         | 1.9            | 0.0   |
| SI.87-560  | 99          | 8.1            | 8.1              | 16.2            | 27.3                | 0.0          | 0.0        | 0.0                   | 0.0       | 0.0             | 11.1      | 27.3               | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 2.0            | 0.0   |
| CW89-008   | 118         | 8.5            | 3.4              | 28.0            | 24.6                | 18.6         | 16.1       | 0.9                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-030   | 114         | 1.8            | 2.6              | 0.9             | 3.5                 | 86.8         | 4.4        | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-085   | 112         | 0.9            | 3.6              | 0.9             | 0.0                 | 2.7          | 89.3       | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-095   | 106         | 3.8            | 8.5              | 12.3            | 0.9                 | 45.3         | 25.5       | 2.8                   | 0.9       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-117   | 107         | 14.0           | 54.2             | 11.2            | 4.7                 | 13.1         | 2.8        | 0.0                   | 0.0       | 0.0             | 10.7      | 6.8                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-138   | 116         | 11.2           | 11.2             | 7.8             | 3.5                 | 56.9         | 9.5        | 0.0                   | 0.0       | 0.0             | 4.3       | 4.3                | 1.1         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-159   | 112         | 11.6           | 31.3             | 5.4             | 0.0                 | 13.4         | 38.4       | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-172   | 111         | 0.9            | 3.6              | 0.9             | 0.9                 | 77.5         | 16.2       | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-196   | 105         | 4.8            | 33.3             | 13.3            | 0.0                 | 39.1         | 8.6        | 0.0                   | 0.0       | 0.0             | 1.9       | 0.0                | 7.7         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-228   | 128         | 2.3            | 12.5             | 10.2            | 2.3                 | 46.1         | 26.6       | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 0.0            | 0.0   |
| CW89-229   | 124         | 4.0            | 1.6              | 0.0             | 0.0                 | 83.9         | 10.5       | 0.0                   | 0.0       | 0.0             | 0.0       | 0.0                | 0.0         | 0.0      | 0.0   | 0.0       | 0.0         | 2.0            | 0.0   |

## APPENDIX E

### Geochemical Analyses of -0.063 mm (-230 mesh; Silt and Clay) Fraction

#### Notes:

- 1) All sample analyses were carried out by the Geoscience Laboratory, Ontario Geological Survey
- 2) Trace element analyses carried out on the -0.063 mm (-230 mesh) fraction obtained by sieving;
- 3) In 1986 and 1987, the following analytical techniques were used:

| Element | Technique   | Detection Limit (ppm) |
|---------|-------------|-----------------------|
| Ag      | AAS Flame   | 2                     |
| As      | AAS Hydride | 1                     |
| Au      | AAS Furnace | 0.002                 |
| Ba      | AAS Flame   | 10                    |
| Cd      | AAS Flame   | 2                     |
| Co      | AAS Flame   | 5                     |
| Cr      | AAS Flame   | 10                    |
| Cu      | AAS Flame   | 5                     |
| Fe      | AAS Flame   | 5                     |
| Li      | AAS Flame   | 3                     |
| Mo      | AAS Flame   | 3                     |
| Ni      | AAS Flame   | 5                     |
| Pb      | AAS Flame   | 10                    |
| Pd      | AAS Furnace | 0.001                 |
| Pt      | AAS Furnace | 0.001                 |
| Rb      | XRF         | 5                     |
| Sb      | AAS Hydride | 0.1                   |
| Sr      | XRF         | 5                     |
| Zn      | AAS Flame   | 10                    |

In 1989, the following analytical techniques were used:

| Element | Technique   | Detection Limit (ppm) |
|---------|-------------|-----------------------|
| Ag      | AAS Flame   | 2                     |
| As      | AAS Hydride | 1                     |
| Au      | AAS Furnace | 0.002                 |
| Ba      | AAS Flame   | 10                    |
| Be      | ICP/OES     | 1                     |
| Bi      | AAS Hydride | 0.05                  |
| Co      | ICP/OES     | 5                     |
| Cr      | AAS Furnace | 10                    |
| Cu      | ICP/OES     | 5                     |
| Fe      | AAS Flame   | 5                     |
| Li      | AAS Flame   | 3                     |
| Mn      | AAS Flame   | 5                     |
| Mo      | ICP/OES     | 10                    |
| Ni      | ICP/OES     | 5                     |
| Pb      | AAS Flame   | 10                    |
| Pd      | AAS Furnace | 0.001                 |
| Pt      | AAS Furnace | 0.001                 |
| Sb      | AAS Hydride | 0.1                   |
| Sc      | AAS Hydride | 0.1                   |
| Sr      | ICP/OES     | 5                     |
| V       | ICP/OES     | 5                     |
| Y       | ICP/OES     | 5                     |
| Zn      | ICP/OES     | 5                     |

- 4) Blind duplicate samples were submitted in 1987 and 1989. The results showed satisfactory duplication of analytical results.

**APPENDIX E: Geochemical analysis of -0.063 mm (-230 mesh) silt and clay fraction**

Note: for analytical techniques used and elements analysed see appendix cover page

| Sample    | Ag ppm | As ppm | Au ppb | Ba ppm | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | Li ppm | Mn ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Rb ppm | Sb ppm | Sr ppm | Zn ppm |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| BI186-1   | -2     | 5.5    | 4      | 525    | -2     | 14     | 118    | 105    | 2.88 | 15     | 635    | -3     | 67     | 5      | N/A    | N/A    | 0      | 0.3    | 209    | 61     |
| BI186-2   | -2     | 8.0    | 3      | 510    | -2     | 14     | 122    | 78     | 2.76 | 14     | 550    | -3     | 68     | 10     | N/A    | N/A    | 48     | 0.3    | 295    | 62     |
| BI186-5   | -2     | 3.5    | 2      | 510    | -2     | 10     | 94     | 46     | 2.27 | 10     | 438    | -3     | 55     | 10     | N/A    | N/A    | 50     | 0.2    | 315    | 41     |
| ST86-005  | -2     | 10.5   | 3      | 508    | -2     | 11     | 110    | 85     | 3.11 | 13     | 453    | -3     | 61     | 10     | N/A    | N/A    | 47     | 0.3    | 298    | 56     |
| ST86-006A | -2     | 10.0   | 13     | 472    | -2     | 17     | 140    | 108    | 3.64 | 15     | 725    | -3     | 81     | 13     | N/A    | N/A    | 52     | 0.3    | 282    | 63     |
| ST86-006B | -2     | 4.0    | 12     | 534    | -2     | 9      | 85     | 41     | 2.15 | 8      | 510    | -3     | 43     | 11     | N/A    | N/A    | 48     | 0.1    | 321    | 34     |
| ST86-009  | -2     | 20.0   | 1      | 525    | -2     | 22     | 118    | 86     | 3.84 | 28     | 1040   | -3     | 70     | 12     | N/A    | N/A    | 50     | 5.0    | 261    | 122    |
| ST86-015  | -2     | 3.5    | 2      | 544    | -2     | 12     | 96     | 49     | 2.45 | 13     | 465    | -3     | 50     | 13     | N/A    | N/A    | 54     | 0.2    | 295    | 37     |
| ST86-016  | -2     | 105.0  | 37     | 436    | -2     | 65     | 304    | 450    | 6.00 | 17     | 2275   | -3     | 250    | 34     | N/A    | N/A    | 47     | 0.7    | 288    | 119    |
| ST86-021  | -2     | 13.0   | 12     | 529    | -2     | 17     | 106    | 63     | 3.25 | 13     | 800    | -3     | 58     | 17     | N/A    | N/A    | 50     | 0.5    | 300    | 47     |
| ST86-024  | -2     | 32.5   | 17     | 525    | -2     | 20     | 176    | 47     | 3.55 | 15     | 745    | -3     | 95     | 14     | N/A    | N/A    | 55     | 0.6    | 280    | 44     |
| ST86-027  | -2     | 6.0    | 3      | 569    | -2     | 12     | 124    | 54     | 2.59 | 11     | 400    | -3     | 81     | 12     | N/A    | N/A    | 52     | 0.1    | 288    | 39     |
| ST86-030  | -2     | 18.0   | 35     | 505    | -2     | 20     | 135    | 113    | 4.03 | 13     | 900    | -3     | 85     | 19     | N/A    | N/A    | 53     | 0.3    | 310    | 50     |
| ST86-033  | -2     | 8.0    | 7      | 470    | -2     | 14     | 100    | 67     | 2.92 | 14     | 360    | -3     | 58     | 14     | N/A    | N/A    | 48     | 0.2    | 263    | 36     |
| ST86-037  | -2     | 8.0    | 3      | 510    | -2     | 15     | 110    | 41     | 3.22 | 15     | 655    | -3     | 72     | 12     | N/A    | N/A    | 49     | 0.3    | 300    | 46     |
| ST86-039  | -2     | 5.5    | 17     | 535    | -2     | 10     | 84     | 42     | 2.53 | 13     | 500    | -3     | 46     | 13     | N/A    | N/A    | 54     | -0.1   | 307    | 36     |
| ST86-042  | -2     | 73.0   | 130    | 460    | -2     | 41     | 168    | 163    | 5.50 | 17     | 1380   | -3     | 115    | 29     | N/A    | N/A    | 46     | 2.2    | 287    | 139    |
| ST86-043  | -2     | 7.5    | 20     | 485    | -2     | 14     | 150    | 50     | 3.09 | 12     | 490    | -3     | 85     | 10     | N/A    | N/A    | 46     | 0.4    | 302    | 41     |
| ST86-048  | -2     | 12.5   | 12     | 480    | -2     | 20     | 139    | 68     | 3.52 | 18     | 675    | -3     | 89     | 10     | N/A    | N/A    | 49     | 0.7    | 281    | 67     |
| ST86-049  | -2     | 45.0   | 65     | 505    | -2     | 37     | 148    | 138    | 5.05 | 20     | 1680   | -3     | 106    | 17     | N/A    | N/A    | 54     | 1.5    | 268    | 84     |
| ST86-057  | -2     | 3.5    | 2      | 505    | -2     | 16     | 109    | 37     | 3.28 | 17     | 570    | -3     | 56     | 14     | N/A    | N/A    | 44     | 0.1    | 318    | 47     |
| ST86-059  | 2      | 36.5   | 3      | 505    | -2     | 34     | 144    | 265    | 4.65 | 16     | 1640   | -3     | 97     | 27     | N/A    | N/A    | 49     | 0.9    | 325    | 85     |
| ST86-060  | -2     | 7.0    | 3      | 480    | -2     | 16     | 125    | 105    | 3.59 | 20     | 500    | -3     | 71     | 14     | N/A    | N/A    | 52     | 0.4    | 272    | 63     |
| ST86-063  | -2     | 1.5    | 1      | 490    | -2     | 8      | 77     | 30     | 2.37 | 12     | 525    | -3     | 36     | 10     | N/A    | N/A    | 46     | -0.1   | 342    | 39     |
| ST86-067  | -2     | 2.5    | 28     | 490    | -2     | 10     | 82     | 31     | 2.60 | 14     | 480    | -3     | 41     | 11     | N/A    | N/A    | 51     | 0.2    | 317    | 35     |
| ST86-068  | -2     | 2.5    | 14     | 532    | -2     | 13     | 83     | 45     | 3.03 | 14     | 535    | -3     | 42     | 15     | N/A    | N/A    | 50     | 0.1    | 308    | 40     |
| ST86-069  | -2     | 8.0    | 9      | 483    | -2     | 19     | 99     | 72     | 3.44 | 13     | 500    | -3     | 58     | 13     | N/A    | N/A    | 45     | 0.2    | 296    | 40     |
| ST86-070  | -2     | 4.0    | 7      | 557    | -2     | 14     | 85     | 44     | 3.00 | 18     | 525    | -3     | 48     | 14     | N/A    | N/A    | 54     | 0.1    | 300    | 54     |
| ST86-072B | -2     | 6.5    | 14     | 438    | -2     | 9      | 83     | 34     | 3.25 | 13     | 355    | -3     | 40     | 10     | N/A    | N/A    | 43     | 0.3    | 275    | 31     |
| ST86-072C | -2     | 14.0   | 6      | 542    | -2     | 11     | 115    | 62     | 2.55 | 15     | 540    | -3     | 67     | 11     | N/A    | N/A    | 53     | 0.4    | 302    | 45     |
| ST86-074  | -2     | 3.5    | 6      | 522    | -2     | 13     | 105    | 29     | 2.73 | 13     | 455    | -3     | 60     | 10     | N/A    | N/A    | 49     | 0.3    | 308    | 34     |
| ST86-076  | -2     | 9.0    | 13     | 487    | -2     | 20     | 171    | 84     | 4.15 | 20     | 645    | -3     | 96     | 13     | N/A    | N/A    | 43     | 0.4    | 271    | 51     |
| ST86-077A | -2     | 16.0   | 6      | 487    | -2     | 23     | 130    | 84     | 4.01 | 15     | 810    | -3     | 77     | 16     | N/A    | N/A    | 45     | 0.5    | 305    | 46     |
| ST86-077B | -2     | 4.5    | 5      | 518    | -2     | 12     | 110    | 45     | 2.84 | 12     | 550    | -3     | 59     | 5      | N/A    | N/A    | 46     | 0.2    | 305    | 39     |
| ST86-079  | -2     | 6.5    | 14     | 513    | -2     | 15     | 132    | 56     | 2.94 | 14     | 580    | -3     | 71     | 13     | N/A    | N/A    | 52     | 0.4    | 304    | 47     |
| ST86-081  | -2     | 6.0    | 3      | 528    | -2     | 12     | 105    | 35     | 2.68 | 13     | 495    | -3     | 59     | 5      | N/A    | N/A    | 48     | 0.6    | 307    | 36     |
| ST86-082  | -2     | 12.0   | 7      | 482    | -2     | 16     | 112    | 37     | 3.14 | 15     | 480    | -3     | 68     | 11     | N/A    | N/A    | 45     | 0.5    | 278    | 55     |
| ST86-083  | -2     | 6.0    | 2      | 510    | -2     | 11     | 96     | 14     | 2.64 | 9      | 370    | -3     | 31     | 11     | N/A    | N/A    | 51     | 0.2    | 325    | 27     |
| ST86-084  | -2     | 19.0   | 12     | 583    | -2     | 24     | 146    | 70     | 5.35 | 22     | 1440   | -3     | 85     | 12     | N/A    | N/A    | 64     | 2.0    | 279    | 75     |
| ST86-085  | -2     | 4.0    | 18     | 536    | -2     | 12     | 94     | 31     | 2.78 | 14     | 460    | -3     | 43     | 10     | N/A    | N/A    | 56     | 0.3    | 305    | 36     |
| ST86-087  | -2     | 2.5    | 5      | 542    | -2     | 14     | 158    | 62     | 3.18 | 13     | 610    | -3     | 82     | 5      | N/A    | N/A    | 47     | 0.1    | 306    | 42     |
| ST86-088  | -2     | 4.0    | 7      | 510    | -2     | 19     | 199    | 110    | 3.70 | 13     | 740    | -3     | 103    | 11     | N/A    | N/A    | 45     | 0.1    | 305    | 53     |

Note: for analytical techniques used and elements analysed see appendix cover page

| Sample    | Ag  | As    | Au  | Ba  | Cd  | Co  | Cr  | Cu  | Fe   | Li  | Mn   | Mo  | Ni  | Pb  | Pd  | Pt  | Rb  | Sb   | Sr  | Zn   |
|-----------|-----|-------|-----|-----|-----|-----|-----|-----|------|-----|------|-----|-----|-----|-----|-----|-----|------|-----|------|
|           | ppm | ppm   | ppb | ppm | ppm | ppm | ppm | ppm | %    | ppm | ppm  | ppm | ppm | ppm | ppb | ppb | ppm | ppm  | ppm | ppm  |
| ST86-089  | -2  | 3.0   | 4   | 526 | -2  | 17  | 164 | 43  | 3.24 | 13  | 505  | -3  | 86  | 5   | N/A | N/A | 49  | 0.1  | 297 | 40   |
| ST86-090  | -2  | 110.0 | 16  | 408 | -2  | 56  | 980 | 308 | 7.80 | 22  | 1360 | -3  | 555 | 24  | N/A | N/A | 53  | 8.9  | 181 | 1490 |
| ST86-100  | -2  | 5.5   | 18  | 512 | -2  | 17  | 108 | 39  | 2.60 | 10  | 535  | -3  | 59  | 10  | N/A | N/A | 48  | 0.3  | 308 | 37   |
| ST86-101  | -2  | 4.0   | 1   | 502 | -2  | 14  | 104 | 49  | 2.82 | 10  | 610  | -3  | 62  | 11  | N/A | N/A | 46  | 0.3  | 300 | 38   |
| ST86-102  | -2  | 3.0   | 10  | 552 | -2  | 13  | 101 | 30  | 2.58 | 11  | 530  | -3  | 48  | 10  | N/A | N/A | 54  | 0.1  | 322 | 35   |
| ST86-103  | -2  | 2.0   | 3   | 502 | -2  | 12  | 100 | 41  | 2.21 | 10  | 460  | -3  | 50  | 5   | N/A | N/A | 48  | 0.1  | 318 | 34   |
| ST86-104  | -2  | 6.0   | 8   | 507 | -2  | 16  | 114 | 37  | 2.63 | 12  | 570  | -3  | 57  | 5   | N/A | N/A | 49  | 0.4  | 299 | 39   |
| ST86-105  | -2  | 2.0   | 8   | 507 | -2  | 10  | 85  | 17  | 1.84 | 8   | 375  | -3  | 37  | 5   | N/A | N/A | 43  | 0.2  | 270 | 27   |
| ST86-106  | -2  | 3.5   | 23  | 502 | -2  | 13  | 94  | 18  | 2.38 | 11  | 330  | -3  | 44  | 5   | N/A | N/A | 48  | 0.2  | 295 | 29   |
| ST86-107A | -2  | 2.5   | 1   | 512 | -2  | 10  | 63  | 31  | 2.10 | 10  | 420  | -3  | 26  | 10  | N/A | N/A | 47  | 0.1  | 342 | 35   |
| ST86-107B | -2  | 4.5   | 5   | 512 | -2  | 13  | 69  | 35  | 2.65 | 13  | 510  | -3  | 31  | 10  | N/A | N/A | 45  | 0.1  | 324 | 45   |
| ST86-108A | -2  | 0.5   | 1   | 581 | -2  | 8   | 58  | 28  | 1.97 | 10  | 398  | -3  | 23  | 5   | N/A | N/A | 48  | 0.1  | 302 | 35   |
| ST86-108B | -2  | 1.0   | 1   | 576 | -2  | 10  | 63  | 27  | 2.25 | 14  | 445  | -3  | 31  | 10  | N/A | N/A | 54  | -0.1 | 316 | 41   |
| ST86-109  | -2  | 9.5   | 8   | 478 | -2  | 16  | 114 | 52  | 3.02 | 13  | 635  | -3  | 66  | 5   | N/A | N/A | 46  | 0.5  | 295 | 48   |
| ST86-110  | -2  | 5.0   | 2   | 522 | -2  | 14  | 109 | 71  | 2.75 | 12  | 545  | -3  | 62  | 5   | N/A | N/A | 48  | 0.3  | 307 | 49   |
| ST86-111  | -2  | 6.5   | 23  | 533 | -2  | 15  | 102 | 54  | 3.08 | 13  | 530  | -3  | 58  | 5   | N/A | N/A | 47  | 0.3  | 304 | 45   |
| ST86-112  | -2  | 28.0  | 6   | 569 | -2  | 22  | 112 | 54  | 3.77 | 17  | 690  | -3  | 65  | 12  | N/A | N/A | 53  | 0.5  | 269 | 48   |
| ST86-113  | -2  | 25.5  | 24  | 468 | -2  | 38  | 375 | 62  | 4.08 | 23  | 830  | -3  | 265 | 12  | N/A | N/A | 43  | 2.5  | 254 | 106  |
| ST86-114  | -2  | 11.5  | 7   | 512 | -2  | 15  | 118 | 59  | 2.57 | 14  | 545  | -3  | 61  | 10  | N/A | N/A | 47  | 0.5  | 296 | 47   |
| ST86-115  | -2  | 3.0   | 6   | 438 | -2  | 15  | 139 | 36  | 3.48 | 22  | 388  | -3  | 61  | 10  | N/A | N/A | 36  | 0.5  | 246 | 51   |
| ST86-116  | -2  | 11.0  | 2   | 510 | -2  | 20  | 144 | 31  | 2.93 | 18  | 705  | -3  | 76  | 10  | N/A | N/A | 52  | 0.5  | 263 | 56   |
| ST86-117  | -2  | 9.0   | 13  | 555 | -2  | 20  | 162 | 180 | 4.15 | 19  | 710  | -3  | 105 | 17  | N/A | N/A | 55  | 0.3  | 283 | 81   |
| ST86-118  | -2  | 3.5   | 1   | 510 | -2  | 10  | 82  | 33  | 2.08 | 8   | 430  | -3  | 39  | 10  | N/A | N/A | 46  | 0.1  | 315 | 30   |
| ST86-119  | -2  | 3.5   | 1   | 553 | -2  | 11  | 79  | 40  | 2.51 | 11  | 443  | -3  | 46  | 11  | N/A | N/A | 50  | 0.1  | 312 | 40   |
| ST86-120  | -2  | 3.0   | 4   | 553 | -2  | 10  | 78  | 37  | 2.42 | 11  | 425  | -3  | 39  | 12  | N/A | N/A | 55  | 0.1  | 328 | 40   |
| ST86-121  | -2  | 7.5   | 6   | 510 | -2  | 15  | 121 | 67  | 2.93 | 12  | 545  | -3  | 65  | 12  | N/A | N/A | 44  | 0.4  | 303 | 80   |
| ST86-122  | -2  | 12.0  | 7   | 528 | -2  | 15  | 117 | 88  | 3.29 | 12  | 665  | -3  | 70  | 10  | N/A | N/A | 48  | 0.5  | 313 | 71   |
| ST86-123  | -2  | 7.0   | 4   | 472 | -2  | 12  | 91  | 66  | 2.70 | 10  | 475  | -3  | 49  | 10  | N/A | N/A | 46  | 0.3  | 307 | 49   |
| ST86-124  | -2  | 6.5   | 1   | 492 | -2  | 17  | 139 | 71  | 3.42 | 12  | 620  | -3  | 72  | 10  | N/A | N/A | 45  | 0.2  | 298 | 51   |
| ST86-125  | -2  | 12.5  | 12  | 482 | -2  | 28  | 131 | 197 | 4.50 | 18  | 1180 | -3  | 72  | 14  | N/A | N/A | 50  | 0.5  | 302 | 72   |
| BH87-1A   | -2  | 2.5   | 5   | 540 | N/A | 14  | 126 | 34  | 2.62 | 13  | 475  | -3  | 68  | 5   | -1  | -1  | N/A | -0.1 | N/A | 37   |
| BH87-1B   | -2  | 2.0   | 3   | 505 | N/A | 14  | 128 | 31  | 2.86 | 13  | 455  | -3  | 77  | 5   | -1  | 2   | N/A | -0.1 | N/A | 39   |
| BH87-2A   | -2  | 2.5   | 2   | 556 | N/A | 13  | 114 | 23  | 2.71 | 13  | 435  | -3  | 60  | 5   | -1  | -1  | N/A | -0.1 | N/A | 34   |
| BH87-2B   | -2  | 1.5   | 1   | 510 | N/A | 12  | 119 | 25  | 2.59 | 16  | 440  | -3  | 64  | 10  | -1  | -1  | N/A | -0.1 | N/A | 39   |
| BH87-3    | -2  | 2.0   | 9   | 594 | N/A | 15  | 113 | 68  | 2.47 | 19  | 400  | -3  | 53  | 11  | -1  | -1  | N/A | -0.1 | N/A | 38   |
| BH87-4A   | -2  | 2.0   | 3   | 567 | N/A | 11  | 96  | 22  | 2.27 | 12  | 365  | -3  | 50  | 10  | -1  | -1  | N/A | -0.1 | N/A | 28   |
| BH87-4B   | -2  | 2.0   | 13  | 546 | N/A | 11  | 116 | 33  | 2.48 | 14  | 390  | -3  | 67  | 5   | -1  | -1  | N/A | -0.1 | N/A | 35   |
| BH87-5A   | -2  | 2.0   | 4   | 551 | N/A | 11  | 100 | 18  | 2.32 | 13  | 355  | -3  | 45  | 10  | -1  | -1  | N/A | -0.1 | N/A | 29   |
| BH87-5B   | -2  | 4.0   | 5   | 541 | N/A | 17  | 151 | 47  | 3.18 | 17  | 500  | -3  | 87  | 11  | -1  | -1  | N/A | -0.1 | N/A | 45   |
| BH87-6    | -2  | 3.5   | 7   | 523 | N/A | 10  | 84  | 28  | 2.25 | 12  | 355  | -3  | 41  | 12  | -1  | -1  | N/A | -0.1 | N/A | 29   |
| BH87-7A   | -2  | 2.5   | 15  | 508 | N/A | 11  | 94  | 21  | 2.13 | 14  | 420  | -3  | 56  | 5   | -1  | -1  | N/A | -0.1 | N/A | 33   |
| BH87-7B   | -2  | 2.5   | 6   | 543 | N/A | 8   | 71  | 24  | 1.92 | 10  | 305  | -3  | 35  | 10  | -1  | -1  | N/A | -0.1 | N/A | 24   |
| BH87-7C   | -2  | 2.0   | 7   | 518 | N/A | 11  | 89  | 17  | 2.15 | 11  | 365  | -3  | 49  | 12  | -1  | -1  | N/A | -0.1 | N/A | 27   |

Note: for analytical techniques used and elements analysed see appendix cover page

| Sample    | Ag  | As   | Au  | Ba  | Cd  | Co  | Cr  | Cu  | Fe   | Li  | Min | Mo  | Ni  | Pb  | Pd  | Pt  | Rb  | Sb   | Sr  | Zn  |
|-----------|-----|------|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|
|           | ppm | ppm  | ppb | ppm | ppm | ppm | ppm | ppm | %    | ppm | ppm | ppm | ppm | ppm | ppb | ppb | ppm | ppm  | ppm | ppm |
| BH87-9    | -2  | 7.5  | 13  | 518 | N/A | 17  | 101 | 28  | 2.76 | 12  | 430 | -3  | 78  | 5   | -1  | -1  | N/A | 0.1  | N/A | 35  |
| BH87-10B  | -2  | 3.5  | 4   | 508 | N/A | 13  | 97  | 19  | 2.33 | 11  | 380 | -3  | 72  | 5   | -1  | -1  | N/A | -0.1 | N/A | 32  |
| BH87-11B  | -2  | 4.5  | 2   | 539 | N/A | 14  | 91  | 28  | 2.74 | 12  | 485 | -3  | 55  | 13  | -1  | -1  | N/A | -0.1 | N/A | 40  |
| BH87-12A  | -2  | 2.0  | 3   | 570 | N/A | 12  | 107 | 19  | 2.40 | 12  | 400 | -3  | 59  | 10  | -1  | -1  | N/A | -0.1 | N/A | 29  |
| BH87-12B  | -2  | 2.0  | 2   | 539 | N/A | 13  | 125 | 26  | 2.75 | 15  | 440 | -3  | 81  | 11  | -1  | -1  | N/A | -0.1 | N/A | 41  |
| BH87-13   | -2  | 6.0  | 3   | 505 | N/A | 13  | 82  | 33  | 2.46 | 15  | 405 | -3  | 40  | 14  | -1  | -1  | N/A | 0.2  | N/A | 36  |
| BH87-14   | -2  | 3.5  | 4   | 552 | N/A | 12  | 103 | 22  | 2.19 | 13  | 370 | -3  | 53  | 12  | -1  | -1  | N/A | 0.1  | N/A | 40  |
| ST87-007  | -2  | 3.0  | 5   | 498 | N/A | 14  | 99  | 48  | 2.81 | 11  | 445 | -3  | 48  | 10  | -1  | -1  | N/A | 0.1  | N/A | 39  |
| ST87-009  | -2  | 13.0 | 4   | 473 | N/A | 17  | 88  | 28  | 2.78 | 11  | 450 | -3  | 46  | 10  | -1  | -1  | N/A | 0.3  | N/A | 39  |
| SL87-011  | -2  | 7.0  | 3   | 493 | N/A | 21  | 134 | 53  | 2.54 | 10  | 485 | N/A | 127 | 14  | -1  | -1  | N/A | -0.1 | N/A | 96  |
| SL87-012  | -2  | 3.5  | 1   | 478 | N/A | 13  | 105 | 21  | 2.33 | 9   | 485 | N/A | 55  | 14  | -1  | -1  | N/A | -0.1 | N/A | 31  |
| SL87-013  | -2  | 5.0  | 12  | 457 | N/A | 14  | 93  | 42  | 2.58 | 11  | 580 | N/A | 52  | 11  | -1  | -1  | N/A | 0.1  | N/A | 30  |
| SL87-016  | -2  | 4.0  | 2   | 493 | N/A | 13  | 118 | 33  | 2.51 | 10  | 510 | N/A | 73  | 10  | -1  | -1  | N/A | -0.1 | N/A | 44  |
| SL87-018  | -2  | 8.5  | 4   | 475 | N/A | 12  | 76  | 15  | 2.30 | 9   | 450 | N/A | 38  | 11  | -1  | -1  | N/A | 0.2  | N/A | 24  |
| SL87-022  | -2  | 2.0  | 1   | 475 | N/A | 10  | 83  | 20  | 2.13 | 9   | 425 | N/A | 38  | 11  | -1  | -1  | N/A | -0.1 | N/A | 27  |
| SL87-036  | -2  | 2.0  | 2   | 542 | N/A | 12  | 90  | 36  | 2.17 | 13  | 430 | N/A | 41  | 13  | -1  | -1  | N/A | -0.1 | N/A | 27  |
| SL87-038  | -2  | 1.5  | 5   | 527 | N/A | 9   | 78  | 14  | 1.84 | 10  | 360 | N/A | 32  | 11  | -1  | -1  | N/A | -0.1 | N/A | 23  |
| SL87-069  | -2  | 2.5  | 4   | 492 | N/A | 13  | 116 | 23  | 2.56 | 11  | 460 | N/A | 73  | 12  | -1  | -1  | N/A | -0.1 | N/A | 30  |
| SL87-075  | -2  | 2.0  | 6   | 492 | N/A | 10  | 88  | 20  | 2.08 | 9   | 410 | N/A | 46  | 11  | -1  | -1  | N/A | -0.1 | N/A | 24  |
| SL87-080  | -2  | 2.0  | 7   | 513 | N/A | 8   | 76  | 13  | 1.89 | 8   | 370 | N/A | 35  | 11  | -1  | -1  | N/A | -0.1 | N/A | 21  |
| SL87-082  | -2  | 4.0  | 7   | 497 | N/A | 13  | 86  | 15  | 2.30 | 9   | 475 | N/A | 43  | 11  | -1  | -1  | N/A | -0.1 | N/A | 25  |
| SL87-086  | -2  | 5.0  | 1   | 508 | N/A | 11  | 79  | 18  | 2.30 | 7   | 395 | N/A | 42  | 11  | -1  | -1  | N/A | -0.1 | N/A | 23  |
| SL87-090  | -2  | 2.0  | 7   | 438 | N/A | 10  | 78  | 13  | 1.98 | 7   | 375 | N/A | 40  | 11  | -1  | -1  | N/A | -0.1 | N/A | 23  |
| SL87-096  | -2  | 2.5  | 2   | 463 | N/A | 11  | 88  | 16  | 2.05 | 8   | 440 | N/A | 48  | 12  | -1  | -1  | N/A | -0.1 | N/A | 24  |
| SL87-098  | -2  | 12.0 | 3   | 429 | N/A | 14  | 75  | 24  | 2.28 | 6   | 460 | N/A | 38  | 11  | -1  | -1  | N/A | 0.1  | N/A | 22  |
| SL87-100  | -2  | 6.5  | 2   | 498 | N/A | 14  | 93  | 32  | 2.45 | 8   | 435 | N/A | 54  | 12  | -1  | -1  | N/A | -0.1 | N/A | 26  |
| SL87-102  | -2  | 1.5  | 6   | 557 | N/A | 11  | 57  | 33  | 2.26 | 13  | 390 | N/A | 29  | 10  | -1  | -1  | N/A | -0.1 | N/A | 36  |
| SL87-105  | -2  | 2.0  | 2   | 502 | N/A | 11  | 66  | 24  | 2.22 | 10  | 415 | N/A | 32  | 13  | -1  | -1  | N/A | -0.1 | N/A | 57  |
| SL87-107  | -2  | 1.5  | 1   | 483 | N/A | 11  | 56  | 17  | 2.32 | 13  | 420 | N/A | 24  | 11  | -1  | -1  | N/A | -0.1 | N/A | 31  |
| SL87-132  | -2  | 3.5  | 7   | 483 | N/A | 14  | 85  | 33  | 2.44 | 11  | 455 | N/A | 45  | 11  | -1  | -1  | N/A | -0.1 | N/A | 39  |
| SL87-133A | -2  | 2.5  | 11  | 564 | N/A | 14  | 100 | 54  | 3.14 | 16  | 480 | N/A | 61  | 12  | -1  | -1  | N/A | -0.1 | N/A | 54  |
| SL87-133B | -2  | 2.0  | 1   | 539 | N/A | 12  | 88  | 38  | 2.69 | 12  | 435 | N/A | 41  | 13  | -1  | -1  | N/A | -0.1 | N/A | 41  |
| SL87-134  | -2  | 1.5  | 1   | 579 | N/A | 12  | 56  | 22  | 2.03 | 7   | 360 | N/A | 28  | 12  | -1  | -1  | N/A | -0.1 | N/A | 42  |
| SL87-136  | -2  | 1.5  | 3   | 629 | N/A | 12  | 62  | 22  | 2.22 | 9   | 390 | N/A | 29  | 14  | -1  | -1  | N/A | -0.1 | N/A | 31  |
| SL87-141  | -2  | 2.0  | 1   | 516 | N/A | 10  | 84  | 17  | 2.00 | 9   | 340 | N/A | 43  | 11  | -1  | -1  | N/A | -0.1 | N/A | 23  |
| SL87-157  | -2  | 4.0  | 6   | 547 | N/A | 14  | 68  | 20  | 2.48 | 10  | 520 | N/A | 33  | 12  | -1  | -1  | N/A | 0.1  | N/A | 35  |
| SL87-161  | -2  | 2.5  | 2   | 511 | N/A | 14  | 99  | 24  | 2.44 | 9   | 495 | N/A | 48  | 10  | -1  | -1  | N/A | -0.1 | N/A | 32  |
| SL87-164  | -2  | 2.0  | 33  | 715 | N/A | 15  | 86  | 66  | 3.34 | 23  | 505 | N/A | 47  | 11  | -1  | -1  | N/A | -0.1 | N/A | 71  |
| SL87-219A | -2  | 3.5  | 3   | 476 | N/A | 13  | 99  | 35  | 2.28 | 8   | 393 | N/A | 45  | 11  | -1  | -1  | N/A | -0.1 | N/A | 28  |
| SL87-219B | -2  | 3.5  | 2   | 469 | N/A | 10  | 79  | 23  | 2.02 | 7   | 345 | N/A | 38  | 11  | -1  | -1  | N/A | -0.1 | N/A | 23  |
| SL87-221  | -2  | 4.0  | 11  | 510 | N/A | 13  | 96  | 32  | 2.22 | 10  | 430 | N/A | 50  | 10  | -1  | -1  | N/A | -0.1 | N/A | 29  |
| SL87-229  | -2  | 5.0  | 5   | 472 | N/A | 20  | 126 | 27  | 3.11 | 11  | 600 | -3  | 70  | 10  | -1  | -1  | N/A | 0.2  | N/A | 31  |
| SL87-272  | -2  | 2.0  | 10  | 482 | N/A | 11  | 67  | 27  | 2.54 | 10  | 480 | -3  | 36  | 5   | -1  | -1  | N/A | 0.1  | N/A | 29  |

Note: for analytical techniques used and elements analysed see appendix cover page

| Sample   | Ag  | As   | Au  | Ba  | Cd  | Co  | Cr  | Cu  | Fe   | Li  | Mn   | Mo  | Ni  | Pb  | Pd  | Pt  | Rb  | Sb   | Sr  | Zn  |
|----------|-----|------|-----|-----|-----|-----|-----|-----|------|-----|------|-----|-----|-----|-----|-----|-----|------|-----|-----|
|          | ppm | ppm  | ppb | ppm | ppm | ppm | ppm | ppm | %    | ppm | ppm  | ppm | ppm | ppm | ppb | ppb | ppm | ppm  | ppm | ppm |
| SL87-290 | -2  | 2.0  | 2   | 514 | N/A | 13  | 78  | 65  | 3.27 | 9   | 525  | -3  | 35  | 5   | 2   | -1  | N/A | 0.1  | N/A | 37  |
| SL87-322 | -2  | 5.0  | 3   | 498 | N/A | 22  | 213 | 37  | 3.90 | 16  | 710  | -3  | 92  | 17  | -1  | -1  | N/A | 0.1  | N/A | 67  |
| SL87-353 | -2  | 3.5  | 1   | 535 | N/A | 17  | 142 | 41  | 3.55 | 15  | 610  | -3  | 95  | 5   | -1  | -1  | N/A | 0.1  | N/A | 43  |
| SL87-356 | -2  | 2.5  | 5   | 477 | N/A | 13  | 98  | 27  | 2.81 | 12  | 510  | -3  | 61  | 5   | -1  | -1  | N/A | 0.1  | N/A | 30  |
| SL87-357 | -2  | 2.5  | 5   | 477 | N/A | 9   | 70  | 23  | 2.43 | 8   | 435  | -3  | 40  | 5   | -1  | -1  | N/A | 0.1  | N/A | 24  |
| SL87-358 | -2  | 3.0  | 2   | 467 | N/A | 12  | 69  | 18  | 2.38 | 8   | 438  | -3  | 41  | 5   | -1  | -1  | N/A | 0.1  | N/A | 22  |
| SL87-361 | -2  | 2.5  | 16  | 467 | N/A | 11  | 76  | 24  | 2.16 | 8   | 430  | -3  | 48  | 11  | -1  | -1  | N/A | 0.1  | N/A | 22  |
| SL87-363 | -2  | 2.0  | 2   | 420 | N/A | 22  | 101 | 76  | 3.85 | 14  | 1105 | -3  | 58  | 5   | -1  | -1  | N/A | 0.4  | N/A | 36  |
| SL87-364 | -2  | 6.5  | 10  | 462 | N/A | 12  | 90  | 250 | 2.98 | 12  | 700  | -3  | 52  | 10  | -1  | -1  | N/A | 0.3  | N/A | 34  |
| SL87-383 | -2  | 1.0  | 1   | 745 | N/A | 14  | 65  | 37  | 2.85 | 10  | 490  | -3  | 30  | 10  | -1  | -1  | N/A | 0.1  | N/A | 50  |
| SL87-394 | -2  | 1.5  | 8   | 493 | N/A | 14  | 112 | 32  | 2.54 | 11  | 485  | -3  | 72  | 5   | -1  | -1  | N/A | 0.1  | N/A | 29  |
| SL87-395 | -2  | 1.5  | 1   | 522 | N/A | 7   | 52  | 8   | 1.91 | 13  | 295  | -3  | 22  | 10  | -1  | -1  | N/A | 0.1  | N/A | 25  |
| SL87-411 | -2  | 1.5  | 2   | 513 | N/A | 12  | 67  | 23  | 2.57 | 11  | 540  | -3  | 34  | 5   | -1  | -1  | N/A | 0.1  | N/A | 32  |
| SL87-412 | -2  | 1.0  | 1   | 478 | N/A | 11  | 60  | 42  | 2.71 | 11  | 433  | -3  | 29  | 5   | -1  | -1  | N/A | 0.1  | N/A | 37  |
| SL87-415 | -2  | 1.0  | 1   | 485 | N/A | 10  | 51  | 32  | 2.91 | 11  | 428  | -3  | 25  | 5   | -1  | -1  | N/A | 0.1  | N/A | 42  |
| SL87-416 | -2  | 1.5  | 4   | 475 | N/A | 11  | 52  | 17  | 2.53 | 8   | 380  | -3  | 26  | 5   | -1  | -1  | N/A | 0.1  | N/A | 28  |
| SL87-418 | -2  | 1.5  | 3   | 540 | N/A | 10  | 60  | 27  | 2.08 | 14  | 280  | -3  | 27  | 12  | -1  | -1  | N/A | -0.1 | N/A | 29  |
| SL87-423 | -2  | 3.5  | 1   | 516 | N/A | 20  | 86  | 25  | 2.48 | 20  | 510  | -3  | 63  | 11  | -1  | -1  | N/A | 0.1  | N/A | 33  |
| SL87-439 | -2  | 1.5  | 10  | 478 | N/A | 13  | 78  | 22  | 2.09 | 11  | 430  | -3  | 39  | 10  | -1  | -1  | N/A | 0.1  | N/A | 25  |
| SL87-440 | -2  | 2.0  | 26  | 478 | N/A | 10  | 75  | 16  | 2.21 | 13  | 340  | -3  | 37  | 10  | -1  | -1  | N/A | 0.1  | N/A | 30  |
| SL87-450 | -2  | 1.0  | 1   | 556 | N/A | 11  | 65  | 18  | 2.45 | 14  | 415  | -3  | 25  | 12  | -1  | -1  | N/A | -0.1 | N/A | 31  |
| SL87-451 | -2  | 1.0  | 1   | 600 | N/A | 12  | 62  | 20  | 2.30 | 16  | 370  | -3  | 28  | 13  | -1  | -1  | N/A | -0.1 | N/A | 34  |
| SL87-452 | -2  | 6.0  | 1   | 575 | N/A | 11  | 50  | 20  | 3.06 | 9   | 350  | -3  | 21  | 5   | -1  | -1  | N/A | -0.1 | N/A | 37  |
| SL87-458 | -2  | 2.5  | 1   | 585 | N/A | 11  | 81  | 16  | 2.32 | 14  | 410  | -3  | 37  | 5   | -1  | -1  | N/A | 0.1  | N/A | 36  |
| SL87-461 | -2  | 2.0  | 1   | 610 | N/A | 32  | 108 | 99  | 4.80 | 17  | 760  | -3  | 52  | 13  | -1  | -1  | N/A | -0.1 | N/A | 59  |
| SL87-513 | -2  | 2.0  | 1   | 466 | N/A | 11  | 59  | 23  | 2.26 | 16  | 335  | -3  | 32  | 11  | -1  | -1  | N/A | 0.1  | N/A | 27  |
| SL87-514 | -2  | 1.0  | 1   | 532 | N/A | 9   | 51  | 23  | 1.91 | 13  | 390  | -3  | 21  | 5   | -1  | -1  | N/A | 0.1  | N/A | 25  |
| SL87-517 | -2  | 3.0  | 5   | 556 | N/A | 13  | 70  | 47  | 2.59 | 14  | 520  | -3  | 42  | 10  | -1  | -1  | N/A | 0.1  | N/A | 40  |
| SL87-518 | -2  | 2.0  | 70  | 525 | N/A | 14  | 67  | 30  | 2.56 | 15  | 555  | -3  | 42  | 11  | -1  | -1  | N/A | 0.1  | N/A | 36  |
| SL87-521 | -2  | 2.0  | 5   | 488 | N/A | 14  | 114 | 21  | 2.53 | 10  | 555  | -3  | 91  | 5   | -1  | -1  | N/A | 0.1  | N/A | 27  |
| SL87-527 | -2  | 2.0  | 1   | 494 | N/A | 12  | 90  | 12  | 2.11 | 9   | 435  | -3  | 51  | 10  | -1  | -1  | N/A | 0.1  | N/A | 23  |
| SL87-528 | -2  | 1.0  | 2   | 640 | N/A | 13  | 54  | 17  | 2.52 | 12  | 350  | -3  | 26  | 5   | -1  | -1  | N/A | -0.1 | N/A | 41  |
| SL87-546 | -2  | 2.5  | 13  | 610 | N/A | 13  | 88  | 25  | 2.24 | 10  | 375  | -3  | 53  | 10  | -1  | -1  | N/A | -0.1 | N/A | 28  |
| SL87-547 | -2  | 1.0  | 1   | 537 | N/A | 10  | 78  | 11  | 1.96 | 9   | 350  | -3  | 36  | 11  | -1  | -1  | N/A | -0.1 | N/A | 24  |
| SL87-548 | -2  | 2.0  | 1   | 513 | N/A | 12  | 85  | 13  | 2.15 | 9   | 340  | -3  | 44  | 10  | -1  | -1  | N/A | -0.1 | N/A | 24  |
| SL87-551 | -2  | 2.5  | 1   | 598 | N/A | 14  | 105 | 47  | 3.00 | 11  | 455  | -3  | 67  | 11  | -1  | -1  | N/A | -0.1 | N/A | 39  |
| SL87-552 | -2  | 1.5  | 5   | 613 | N/A | 10  | 76  | 11  | 2.02 | 7   | 365  | -3  | 46  | 10  | -1  | -1  | N/A | -0.1 | N/A | 22  |
| SL87-555 | -2  | 3.0  | 38  | 613 | N/A | 14  | 103 | 20  | 2.62 | 10  | 510  | -3  | 54  | 10  | -1  | -1  | N/A | -0.1 | N/A | 31  |
| SL87-559 | -2  | 2.0  | 4   | 607 | N/A | 10  | 78  | 18  | 2.00 | 14  | 300  | -3  | 40  | 13  | -1  | -1  | N/A | -0.1 | N/A | 35  |
| SL87-560 | -2  | 2.0  | 4   | 548 | N/A | 13  | 85  | 25  | 2.52 | 15  | 390  | -3  | 41  | 13  | -1  | -1  | N/A | 0.1  | N/A | 34  |
| SL87-561 | -2  | 28.0 | 6   | 443 | N/A | 19  | 105 | 46  | 3.60 | 17  | 560  | -3  | 59  | 11  | -1  | -1  | N/A | 0.7  | N/A | 45  |

Note: for analytical techniques used and elements analysed see appendix cover page

| Sample                   | Ag ppm | As ppm | Au ppb | Ba ppm | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | Li ppm | Mn ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Rb ppm | Sb ppm | Sr ppm | V ppm | Y ppm | Zn ppm |  |
|--------------------------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|--|
| AVERAGE                  | 7.1    | 7.1    | 8.2    | 518    | 15     | 107    | 47     | 2.80   | 13   | 533    | 60     | 11     | 49     | 297    | 50     | 50     | 49     | 297    | 297    | 297   | 50    | 50     |  |
| MAXIMUM                  | 110    | 130    | 745    | 65     | 980    | 450    | 450    | 7.80   | 28   | 2275   | 555    | 34     | 64     | 342    | 1490   | 1490   | 64     | 342    | 342    | 342   | 1490  | 1490   |  |
| MINIMUM                  | 0.5    | 1      | 408    | 7      | 50     | 8      | 1.84   | 21     | 6    | 280    | 21     | 5      | 36     | 181    | 21     | 21     | 36     | 181    | 181    | 181   | 21    | 21     |  |
| STD.DEV.                 | 13.8   | 14     | 48     | 7.3    | 78     | 51     | 0.818  | 49     | 4    | 259    | 49     | 4      | 4.1    | 23.7   | 113    | 113    | 4.1    | 23.7   | 23.7   | 113   | 113   | 113    |  |
| No.below detection limit | 1      | 34     |        |        |        |        |        |        |      |        |        |        |        |        |        |        |        |        |        |       |       |        |  |

**APPENDIX E: Gowganda area sample results**

Note: for analytical techniques used and elements analysed see appendix cover page

| Sample                   | Ag ppm | As ppm | Au ppb | Ba ppm | Be ppm | Bi ppm | Co ppm | Cr ppm | Cu ppm | Fe % | Li ppm | Mn ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Sb ppm | Sc ppm | Sr ppm | V ppm | Y ppm | Zn ppm |
|--------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|
| GW89-004 -2              | 2.5    | 6      | 427    | 100    | 10     | 84     | 25     | 1.91   | 9      | 635  | -10    | 10     | 39     | 10     | -1     | -1     | 0.2    | 8      | 287    | 51     | 9     | 26    |        |
| GW89-008 -2              | 13.0   | 6      | 463    | 1      | 17     | 115    | 39     | 1.91   | 10     | 840  | -10    | 13     | 78     | 13     | -1     | -1     | 2.4    | 11     | 276    | 57     | 10    | 35    |        |
| GW89-011 -2              | 4.0    | 20     | 448    | 1      | 14     | 86     | 20     | 2.14   | 11     | 705  | -10    | 13     | 52     | 13     | -1     | -1     | 0.2    | 8      | 253    | 51     | 10    | 30    |        |
| GW89-030A -2             | 5.5    | 17     | 419    | 1      | 20     | 90     | 32     | 2.72   | 18     | 935  | -10    | 12     | 41     | 12     | -1     | -1     | 0.3    | 10     | 238    | 72     | 9     | 40    |        |
| GW89-030B -2             | 6.0    | 2      | 392    | 1      | 180    | 157    | 74     | 3.10   | 18     | 1180 | -10    | 18     | 60     | 18     | -1     | -1     | 0.5    | 15     | 255    | 102    | 11    | 61    |        |
| GW89-048 -2              | 4.5    | 2      | 459    | 1      | 130    | 80     | 37     | 2.30   | 11     | 850  | -10    | 16     | 32     | 16     | -1     | -1     | 0.2    | 9      | 314    | 64     | 9     | 37    |        |
| GW89-057 -2              | 3.0    | 20     | 407    | 1      | 100    | 65     | 30     | 1.89   | 8      | 720  | -10    | 10     | 24     | 10     | -1     | -1     | 0.1    | 8      | 327    | 56     | 9     | 29    |        |
| GW89-071 -2              | 4.5    | 4      | 410    | 1      | 250    | 96     | 27     | 2.73   | 28     | 740  | -10    | 3      | 40     | 10     | -1     | -1     | 0.5    | 11     | 171    | 82     | 10    | 45    |        |
| GW89-085 -2              | 2.0    | 2      | 223    | -1     | 70     | 82     | 8      | 0.85   | 5      | 220  | -10    | 10     | 9      | 10     | -1     | -1     | 0.1    | 4      | 142    | 24     | 6     | 8     |        |
| GW89-095 -2              | 3.5    | 4      | 428    | 1      | 120    | 82     | 21     | 1.56   | 10     | 485  | -10    | 10     | 50     | 10     | -1     | -1     | 1.1    | 8      | 265    | 47     | 8     | 20    |        |
| GW89-115 -2              | 4.0    | 5      | 304    | -1     | 80     | 231    | 75     | 4.03   | 20     | 1880 | -10    | 14     | 99     | 14     | -1     | -1     | 0.3    | 24     | 235    | 142    | 12    | 75    |        |
| GW89-117 -2              | 7.5    | 1      | 500    | 1      | 210    | 173    | 70     | 2.63   | 16     | 1070 | -10    | 25     | 50     | 25     | -1     | -1     | 2.2    | 13     | 328    | 85     | 12    | 72    |        |
| GW89-119 -2              | 16.0   | 5      | 427    | -1     | 1500   | 90     | 33     | 2.91   | 9      | 985  | -10    | 22     | 33     | 22     | -1     | -1     | 0.5    | 11     | 359    | 78     | 11    | 39    |        |
| GW89-127 -2              | 6.0    | 7      | 552    | 1      | 170    | 91     | 11     | 1.90   | 10     | 240  | -10    | 20     | 10     | 20     | -1     | -1     | 3.9    | 4      | 89     | 39     | 6     | 12    |        |
| GW89-128 -2              | 2.5    | 1      | 446    | 1      | 130    | 74     | 17     | 2.02   | 13     | 570  | -10    | 31     | 11     | 11     | -1     | -1     | 0.2    | 8      | 282    | 51     | 8     | 25    |        |
| GW89-138 -2              | 2.5    | 8      | 489    | 1      | 110    | 101    | 30     | 2.53   | 16     | 650  | -10    | 13     | 46     | 13     | -1     | -1     | 0.2    | 9      | 266    | 58     | 9     | 36    |        |
| GW89-151 -2              | 20.0   | 29     | 439    | 1      | 170    | 102    | 77     | 2.81   | 15     | 730  | -10    | 15     | 59     | 74     | -1     | -1     | 0.3    | 9      | 256    | 57     | 11    | 134   |        |
| GW89-159 -2              | 2.5    | 2      | 467    | -1     | 260    | 219    | 41     | 1.77   | 10     | 640  | -10    | 15     | 24     | 15     | -1     | -1     | 0.4    | 8      | 292    | 69     | 10    | 35    |        |
| GW89-172 -2              | 5.0    | 10     | 362    | 1      | 150    | 110    | 41     | 1.88   | 12     | 580  | -10    | 23     | 10     | 23     | -1     | -1     | 0.3    | 8      | 219    | 54     | 8     | 24    |        |
| GW89-185 -2              | 5.5    | 1      | 535    | 1      | 130    | 86     | 39     | 3.21   | 19     | 730  | -10    | 10     | 44     | 21     | -1     | -1     | 0.2    | 11     | 202    | 87     | 11    | 35    |        |
| GW89-195 -2              | 2.0    | 2      | 482    | -1     | 90     | 58     | 9      | 1.65   | 11     | 645  | -10    | 23     | 25     | 14     | -1     | -1     | 0.05   | 8      | 291    | 47     | 9     | 26    |        |
| GW89-200 -2              | 3.0    | 11     | 470    | 1      | 170    | 62     | 23     | 1.91   | 9      | 725  | -10    | 22     | 25     | 14     | -1     | -1     | 0.2    | 8      | 297    | 53     | 9     | 27    |        |
| GW89-218 -2              | 2.0    | 2      | 447    | -1     | 100    | 129    | 29     | 1.69   | 9      | 570  | -10    | 22     | 22     | 14     | -1     | -1     | 0.2    | 7      | 233    | 50     | 7     | 23    |        |
| GW89-228 -2              | 2.5    | 2      | 454    | 1      | 220    | 56     | 18     | 1.97   | 9      | 575  | -10    | 21     | 21     | 12     | -1     | -1     | 0.2    | 8      | 273    | 54     | 9     | 23    |        |
| GW89-229 -2              | 2.5    | 2      | 447    | 1      | 100    | 170    | 28     | 1.63   | 9      | 630  | -10    | 13     | 33     | 13     | -1     | -1     | 0.3    | 8      | 277    | 50     | 9     | 25    |        |
| GW89-230 -2              | 3.5    | 1      | 481    | 1      | 220    | 194    | 38     | 2.04   | 17     | 750  | -10    | 10     | 44     | 10     | -1     | -1     | 0.3    | 9      | 266    | 56     | 10    | 32    |        |
| GW89-238 -2              | 3.0    | 1      | 435    | 1      | 140    | 80     | 23     | 1.97   | 12     | 705  | -10    | 12     | 45     | 12     | -1     | -1     | 0.3    | 8      | 265    | 52     | 8     | 26    |        |
| SI 89-246 -2             | 15.0   | 1      | 450    | -1     | 260    | 43     | 10     | 1.44   | 8      | 365  | -10    | 17     | 17     | 10     | -1     | -1     | 0.3    | 5      | 184    | 38     | 7     | 14    |        |
| SI 89-247 -2             | 19.0   | 5      | 452    | -1     | 70     | 86     | 25     | 2.25   | 10     | 890  | -10    | 10     | 49     | 10     | -1     | -1     | 0.3    | 9      | 309    | 53     | 9     | 25    |        |
| AVERAGE                  | 5.8    | 6      | 439    | 198    | 13     | 32     | 2.17   | 12     | 735    | 40   | 0.6    | 9      | 258    | 61     | 9      | 35     | 9      | 35     | 285    | 58     | 58    | 9     | 23     |
| MAXIMUM                  | 20.0   | 29     | 552    | 1500   | 33     | 77     | 4.03   | 28     | 1880   | 99   | 3.9    | 24     | 359    | 142    | 12     | 134    | 12     | 134    | 342    | 342    | 342   | 1490  | 1490   |
| MINIMUM                  | 1.5    | 1      | 223    | 70     | 3      | 8      | 0.85   | 5      | 220    | 9    | 0.05   | 4      | 89     | 24     | 6      | 8      | 6      | 8      | 181    | 181    | 181   | 21    | 21     |
| STD.DEV.                 | 5.1    | 7      | 61     | 248    | 6      | 19     | 0.62   | 5      | 297    | 19   | 0.8    | 4      | 56     | 22     | 2      | 24     | 2      | 24     | 23.7   | 23.7   | 113   | 113   | 113    |
| No.below detection limit | 6      | 1      |        |        |        |        |        |        |        |      |        |        |        |        |        |        |        |        |        |        |       |       |        |

Aultman Samples, Churchill Township

| Sample   | Ag  | As   | Au  | Ba  | Cd  | Co  | Cr  | Cu  | Fe   | Li  | Mn   | Mo  | Ni  | Pb  | Pd  | Pt  | Rb  | Sb  | Sr  | Zn  |
|----------|-----|------|-----|-----|-----|-----|-----|-----|------|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|          | ppm | ppm  | ppb | ppm | ppm | ppm | ppm | ppm | %    | ppm | ppm  | ppm | ppm | ppm | ppm | ppb | ppb | ppm | ppm | ppm |
| JTA-1A   | -2  | 19.0 | 23  | 533 | N/A | 20  | 129 | 55  | 3.16 | 16  | 650  | -10 | 72  | 10  | -1  | 7   | N/A | 0.8 | N/A | 56  |
| JTA-1B   | -2  | 28.0 | 21  | 549 | N/A | 31  | 123 | 75  | 3.71 | 18  | 1015 | -10 | 73  | 10  | -1  | -1  | N/A | 0.9 | N/A | 60  |
| JTA-2    | -2  | 55.0 | 19  | 462 | N/A | 50  | 132 | 104 | 3.93 | 18  | 1230 | -10 | 86  | 10  | -1  | 7   | N/A | 1.2 | N/A | 65  |
| JTA-3A   | -2  | 16.0 | 3   | 462 | N/A | 19  | 134 | 45  | 2.90 | 14  | 620  | -10 | 81  | 12  | -1  | -1  | N/A | 0.5 | N/A | 75  |
| JTA-3B   | -2  | 13.0 | 5   | 431 | N/A | 21  | 132 | 69  | 2.83 | 14  | 670  | -10 | 74  | 10  | -1  | 1   | N/A | 0.4 | N/A | 80  |
| JTA-4    | -2  | 47.0 | 36  | 411 | N/A | 36  | 166 | 82  | 5.05 | 16  | 1165 | -10 | 85  | 22  | -1  | 1   | N/A | 1.1 | N/A | 78  |
| JTA-5    | -2  | 14.0 | 21  | 492 | N/A | 19  | 133 | 52  | 3.01 | 15  | 640  | -10 | 69  | 13  | -1  | 1   | N/A | 0.5 | N/A | 63  |
| JTA-6    | -2  | 16.0 | 19  | 517 | N/A | 15  | 120 | 72  | 2.84 | 15  | 565  | -10 | 62  | 12  | -1  | -1  | N/A | 0.4 | N/A | 54  |
| JTA-7    | -2  | 9.0  | 6   | 492 | N/A | 26  | 170 | 76  | 3.44 | 17  | 830  | -10 | 108 | 16  | -1  | 2   | N/A | 0.7 | N/A | 120 |
| JTA-8A   | -2  | 15.0 | 5   | 451 | N/A | 24  | 137 | 46  | 3.22 | 14  | 790  | -10 | 68  | 13  | 1   | 1   | N/A | 0.7 | N/A | 73  |
| JTA-9    | -2  | 18.0 | 3   | 447 | N/A | 19  | 159 | 38  | 3.16 | 17  | 615  | -10 | 93  | 10  | -1  | -1  | N/A | 0.6 | N/A | 105 |
| JTA-11   | -2  | 22.0 | 8   | 427 | N/A | 25  | 144 | 71  | 3.34 | 13  | 790  | -10 | 84  | 10  | -1  | -1  | N/A | 0.7 | N/A | 106 |
| JTA-12   | -2  | 16.0 | 13  | 481 | N/A | 20  | 127 | 65  | 2.94 | 13  | 695  | -10 | 66  | 10  | -1  | -1  | N/A | 0.6 | N/A | 73  |
| JTA-14   | -2  | 17.0 | 200 | 532 | N/A | 25  | 111 | 57  | 3.36 | 15  | 1075 | -10 | 56  | 5   | -1  | -1  | N/A | 0.7 | N/A | 50  |
| JTA-16   | -2  | 21.0 | 27  | 491 | N/A | 29  | 134 | 57  | 3.75 | 18  | 1090 | -10 | 75  | 5   | -1  | -1  | N/A | 0.7 | N/A | 67  |
| JTA-17   | -2  | 11.0 | 5   | 501 | N/A | 19  | 121 | 57  | 2.60 | 16  | 665  | -10 | 70  | 5   | -1  | -1  | N/A | 0.6 | N/A | 60  |
| AVERAGE  |     | 21.1 | 26  | 480 |     | 25  | 136 | 64  | 3.33 | 16  | 819  |     | 76  | 8   |     |     |     | 0.7 |     | 74  |
| MAXIMUM  |     | 55.0 | 200 | 549 |     | 50  | 170 | 104 | 5.05 | 18  | 1230 |     | 108 | 22  |     |     |     | 1.2 |     | 120 |
| MINIMUM  |     | 9.0  | 3   | 411 |     | 15  | 111 | 38  | 2.60 | 13  | 565  |     | 56  | 5   |     |     |     | 0.4 |     | 50  |
| STD.DEV. |     | 12.2 | 46  | 40  |     | 8   | 16  | 16  | 0.57 | 2   | 214  |     | 12  | 4   |     |     |     | 0.2 |     | 20  |

No. below detection limit

## APPENDIX F

### INA Analyses of Non-Magnetic and Magnetic Fractions of HMC Samples

Instrumental Neutron Activation Analysis (INA Analysis) of the entire unground non-magnetic or magnetic heavy mineral concentrate was carried out by Bondar-Clegg & Co. Ltd., Ottawa, Ontario. Detection limits for the various elements are as follows:

|    |            |              |
|----|------------|--------------|
| Ag | Silver     | 5 ppm        |
| As | Arsenic    | 1 ppm        |
| Au | Gold       | 5 ppb        |
| Ba | Barium     | 100 ppm      |
| Br | Bromine    | 1 ppm        |
| Cd | Cadmium    | 10 ppm       |
| Ce | Cerium     | 10 ppm       |
| Co | Cobalt     | 10 ppm       |
| Cr | Chromium   | 50 ppm       |
| Cs | Cesium     | 1 ppm        |
| Eu | Europium   | 2 ppm        |
| Fe | Iron       | 0.5 percent  |
| Hf | Hafnium    | 2 ppm        |
| Ir | Iridium    | 100 ppm      |
| La | Lanthanum  | 5 ppm        |
| Lu | Lutetium   | 0.5 ppm      |
| Mo | Molybdenum | 2 ppm        |
| Na | Sodium     | 0.05 percent |
| Ni | Nickel     | 20 ppm       |
| Rb | Rubidium   | 10 ppm       |
| Sb | Antimony   | 0.2 ppm      |
| Sc | Scandium   | 0.5 ppm      |
| Se | Selenium   | 10 ppm       |
| Sm | Samarium   | 0.2 ppm      |
| Sn | Tin        | 200 ppm      |
| Ta | Tantalum   | 1 ppm        |
| Tb | Terbium    | 1 ppm        |
| Te | Tellurium  | 20 ppm       |
| Th | Thorium    | 0.5 ppm      |
| U  | Uranium    | 0.5 ppm      |
| W  | Tungsten   | 2 ppm        |
| Yb | Ytterbium  | 5 ppm        |
| Zn | Zinc       | 200 ppm      |
| Zr | Zirconium  | 500 ppm      |

# APPENDIX F: INA Analysis of non-magnetic HMC samples, Shining Tree Area

| Sample Number | Ag ppm | As ppm | Au ppb | Ba ppm | Ce ppm | Co ppm | Cr ppm | Eu ppm | Fe pct | Hf ppm | La ppm | Lu ppm | Mo ppm | Na ppm | Ni ppm | Sb ppm | Sc ppm | Se ppm | Sm ppm | Sn ppm | Ta ppm | Tb ppm | Th ppm | U ppm | W ppm | Yb ppm | Zn ppm | Zr ppm | Wt g  |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|--------|--------|-------|
| BT186-1       | -5     | 4      | 731    | -100   | 720    | 40     | 2500   | 5      | 20     | 203    | 350    | 3.3    | -2     | 0.29   | 39     | 0.5    | 94.4   | -10    | 59.8   | -200   | 12     | 7      | 151    | 19    | 6     | 26     | -200   | 8600   | 16.07 |
| BT186-2       | -5     | 6      | 190    | -100   | 550    | 46     | 2640   | 4      | 20     | 180    | 270    | 3.2    | -2     | 0.27   | 21     | 0.6    | 96     | -10    | 50.4   | -200   | 9      | 6      | 109    | 16    | 6     | 23     | -200   | 7000   | 17.15 |
| BT186-5       | -5     | 4      | 1020   | -100   | 920    | 41     | 1900   | -2     | 20     | 228    | 460    | 3.6    | -2     | 0.25   | -20    | 0.3    | 92.4   | -10    | 73.8   | -200   | 12     | 8      | 210    | 23    | 7     | 26     | -200   | 9200   | 18.44 |
| ST86-005      | -5     | 3      | 120    | -100   | 760    | 41     | 2400   | 5      | 21     | 218    | 350    | 3.3    | -2     | 0.32   | -20    | 0.5    | 98.5   | -10    | 60.9   | -200   | 10     | 6      | 156    | 19    | 6     | 27     | -200   | 9300   | 12.46 |
| ST86-006A     | -5     | 3      | 62     | 130    | 780    | 43     | 1700   | 6      | 19     | 212    | 410    | 3.2    | -2     | 0.3    | -20    | 0.5    | 94     | -10    | 66.7   | -200   | 12     | 6      | 180    | 22    | -6    | 26     | -200   | 8200   | 17.05 |
| ST86-009      | -5     | 1      | 39     | -100   | 1190   | 34     | 2100   | 4      | 19     | 259    | 606    | 2.9    | -2     | 0.16   | -20    | 0.7    | 88.5   | -10    | 86     | -200   | 13     | 7      | 227    | 28    | 12    | 25     | -200   | 12000  | 13.76 |
| ST86-015      | -5     | 6      | 991    | -100   | 690    | 37     | 2400   | 3      | 18     | 210    | 350    | 2.9    | -2     | 0.3    | 23     | 0.4    | 84.3   | -10    | 64.1   | -200   | 11     | 7      | 166    | 21    | -6    | 22     | -200   | 9200   | 14.31 |
| ST86-016      | -5     | 29     | 1160   | -100   | 390    | 81     | 10400  | 3      | 20     | 94     | 180    | 2.7    | -2     | 0.23   | 120    | 1.8    | 86.3   | -10    | 38     | -200   | 8      | 5      | 73.7   | 10    | 10    | 19     | -200   | 4400   | 21.99 |
| ST86-021      | -5     | 7      | 200    | -100   | 540    | 54     | 1300   | 4      | 21     | 130    | 230    | 2.5    | -2     | 0.34   | 27     | 0.8    | 90.6   | -10    | 44     | -200   | 9      | 5      | 93.7   | 13    | 6     | 20     | -200   | 5200   | 7.34  |
| ST86-024      | -5     | 14     | 840    | -100   | 700    | 53     | 4100   | 5      | 19     | 201    | 310    | 3.5    | -2     | 0.25   | 45     | 0.8    | 101    | -10    | 55     | -200   | 10     | 6      | 128    | 18    | 22    | 28     | -200   | 7800   | 11.63 |
| ST86-027      | -5     | 5      | 778    | -100   | 740    | 45     | 5380   | 3      | 20     | 237    | 350    | 3.7    | -2     | 0.35   | -20    | 1.3    | 102    | -10    | 57.8   | -200   | 12     | 6      | 158    | 20    | -6    | 28     | -200   | 9500   | 14.93 |
| ST86-030      | -5     | 7      | 558    | -100   | 530    | 47     | 3900   | 6      | 18     | 200    | 250    | 3.2    | -2     | 0.3    | 21     | 0.7    | 96.2   | -10    | 47     | -200   | 9      | 5      | 97.4   | 16    | 19    | 25     | -200   | 8500   | 18.7  |
| ST86-033      | -5     | 8      | 240    | -100   | 600    | 53     | 6290   | 6      | 20     | 222    | 270    | 3.3    | -2     | 0.24   | 36     | 0.6    | 97.7   | -10    | 45     | -200   | 10     | 5      | 107    | 17    | -6    | 25     | -200   | 8600   | 6.64  |
| ST86-037      | -5     | 4      | 290    | -100   | 640    | 48     | 2500   | 5      | 21     | 200    | 300    | 3.2    | -2     | 0.19   | 23     | 0.6    | 100    | -10    | 52.2   | -200   | 10     | 6      | 126    | 17    | -6    | 25     | -200   | 8300   | 13.11 |
| ST86-039      | -5     | 12     | 190    | -100   | 610    | 56     | 3600   | 3      | 19     | 180    | 270    | 2.6    | -2     | 0.34   | 50     | 0.8    | 91.1   | -10    | 46     | -200   | 8      | 5      | 111    | 16    | -7    | 19     | -200   | 7100   | 5.58  |
| ST86-043      | -5     | 6      | 1140   | -100   | 600    | 46     | 2400   | 4      | 18     | 217    | 290    | 2.7    | -2     | 0.31   | -20    | 1      | 87.8   | -10    | 54.9   | -200   | 10     | 6      | 138    | 20    | -6    | 21     | -200   | 9700   | 15.48 |
| ST86-048      | -5     | 11     | 92     | -100   | 460    | 67     | 2300   | 4      | 22     | 150    | 200    | 2.6    | -2     | 0.29   | 72     | 1.1    | 86.7   | -10    | 37     | -200   | 8      | 4      | 83.1   | 12    | -6    | 20     | -200   | 6400   | 11    |
| ST86-049      | -5     | 27     | 1490   | -100   | 460    | 49     | 2200   | 3      | 20     | 130    | 210    | 2.7    | -2     | 0.24   | 60     | 2.3    | 90     | -10    | 36     | -200   | 7      | 5      | 90.9   | 12    | -6    | 21     | 210    | 4800   | 6.5   |
| ST86-057      | -5     | 1      | 1740   | -100   | 1060   | 37     | 1400   | 5      | 21     | 216    | 539    | 4.2    | -2     | 0.39   | -20    | 0.3    | 107    | -10    | 87.2   | -200   | 15     | 8      | 234    | 26    | 18    | 30     | -200   | 9000   | 32.29 |
| ST86-059      | -5     | 5      | 190    | -100   | 720    | 43     | 2100   | 7      | 20     | 190    | 330    | 3.4    | -2     | 0.2    | -20    | 0.7    | 103    | -10    | 59.5   | -200   | 10     | 6      | 141    | 18    | -6    | 26     | -200   | 7300   | 20.58 |
| ST86-060      | -5     | 5      | 270    | -100   | 650    | 41     | 4200   | 3      | 21     | 204    | 290    | 3.5    | -2     | 0.25   | 35     | 0.6    | 109    | -10    | 48     | -200   | 11     | 6      | 124    | 16    | 12    | 25     | -200   | 8200   | 10.37 |
| ST86-063      | -5     | 0.5    | 1040   | -100   | 800    | 38     | 870    | 12     | 18     | 180    | 340    | 3.4    | -2     | 0.12   | -20    | 0.4    | 97.7   | -10    | 82.8   | -200   | 11     | 9      | 126    | 20    | -6    | 27     | -200   | 7000   | 9.3   |
| ST86-067      | -5     | 0.5    | 44     | -100   | 700    | 33     | 1600   | 5      | 19     | 190    | 330    | 3.5    | -2     | 0.3    | -20    | 0.2    | 100    | -10    | 57.4   | -200   | 10     | 6      | 142    | 21    | -6    | 25     | -200   | 10000  | 11.56 |
| ST86-068      | -5     | 0.5    | 260    | -100   | 730    | 40     | 1400   | 6      | 19     | 246    | 340    | 3.1    | -2     | 0.23   | 23     | 0.4    | 96.1   | -10    | 46     | -200   | 10     | 6      | 109    | 15    | -6    | 23     | -200   | 7400   | 18.65 |
| ST86-069      | -5     | 5      | 51     | -100   | 580    | 43     | 2200   | 5      | 21     | 180    | 250    | 3.3    | -2     | 0.32   | 24     | 0.4    | 98.9   | -10    | 46     | -200   | 10     | 6      | 172    | 25    | -7    | 26     | -200   | 10000  | 20.44 |
| ST86-070      | -5     | 2      | 400    | -100   | 810    | 39     | 1500   | 4      | 19     | 262    | 390    | 3.2    | -2     | 0.2    | 39     | 0.3    | 93.3   | -10    | 66     | -200   | 11     | 6      | 153    | 20    | 18    | 25     | -200   | 9500   | 10.06 |
| ST86-072C     | -5     | 1      | 320    | -100   | 1040   | 42     | 1700   | 4      | 21     | 238    | 340    | 3.2    | -2     | 0.26   | -20    | 0.6    | 96.7   | -10    | 55.6   | -200   | 11     | 6      | 222    | 26    | -7    | 29     | -200   | 10000  | 14.4  |
| ST86-077A     | -5     | 1      | 1220   | -100   | 790    | 38     | 1900   | 5      | 21     | 237    | 380    | 3.5    | -2     | 0.2    | 41     | 0.4    | 104    | -10    | 61.8   | -200   | 12     | 6      | 164    | 22    | -7    | 28     | -200   | 9500   | 18.35 |
| ST86-078      | -5     | 3      | 1320   | -100   | 660    | 44     | 3000   | 5      | 21     | 201    | 310    | 3      | -2     | 0.27   | 27     | 0.5    | 103    | -10    | 51.1   | -200   | 9      | 6      | 128    | 18    | 9     | 25     | -200   | 8300   | 10.47 |
| ST86-077A     | -5     | 5      | 220    | -100   | 610    | 42     | 2200   | 4      | 22     | 130    | 300    | 3.5    | -2     | 0.26   | 31     | 0.5    | 95.9   | -10    | 54     | -200   | 11     | 5      | 126    | 14    | -6    | 23     | -200   | 5600   | 42.49 |
| ST86-078      | -5     | 2      | 120    | -100   | 830    | 41     | 2100   | 5      | 21     | 227    | 400    | 3.6    | -2     | 0.28   | -20    | 0.4    | 100    | -10    | 68.5   | -200   | 12     | 7      | 166    | 22    | 8     | 28     | -200   | 9000   | 18.95 |
| ST86-079      | -5     | 5      | 200    | -100   | 830    | 41     | 2100   | 5      | 21     | 227    | 410    | 3.5    | -2     | 0.24   | -20    | 0.5    | 98.4   | -10    | 68.5   | -200   | 12     | 7      | 178    | 21    | 9     | 27     | -200   | 9500   | 19.26 |
| ST86-081      | -5     | 3      | 29     | -100   | 780    | 40     | 1600   | 3      | 20     | 213    | 370    | 3.2    | -2     | 0.35   | 44     | 0.5    | 98.4   | -10    | 62.3   | -200   | 10     | 6      | 157    | 19    | -7    | 26     | -200   | 8700   | 14.09 |
| ST86-082      | -5     | 4      | 250    | -100   | 740    | 42     | 2900   | 3      | 21     | 200    | 360    | 3.7    | -2     | 0.31   | -20    | 0.5    | 104    | -10    | 60.1   | -200   | 11     | 6      | 149    | 20    | -7    | 26     | -200   | 8400   | 19.17 |
| ST86-083      | -5     | 7      | 620    | -100   | 610    | 46     | 1700   | 4      | 20     | 140    | 280    | 3      | -2     | 0.21   | -20    | 0.4    | 99.2   | -10    | 53.3   | -200   | 10     | 5      | 113    | 16    | -7    | 22     | -200   | 5800   | 31.08 |
| ST86-084      | -5     | 10     | 2710   | -100   | 660    | 65     | 1100   | 6      | 18     | 190    | 300    | 2.9    | -2     | 0.21   | 43     | 0.6    | 87.6   | -10    | 63.5   | -200   | 11     | 7      | 137    | 22    | -7    | 23     | -200   | 8600   | 15.01 |
| ST86-085      | -5     | 5      | 250    | -100   | 890    | 40     | 1700   | 3      | 18     | 248    | 440    | 2.6    | -2     | 0.33   | 29     | 0.7    | 83.6   | -10    | 72.9   | -200   | 10     | 7      | 208    | 27    | -7    | 25     | 200    | 10000  | 13.44 |
| ST86-087      | -5     | 1      | 260    | -100   | 690    | 39     | 2900   | 6      | 19     | 212    | 330    | 3.2    | -2     | 0.12   | -20    | 0.3    | 96.9   | -10    | 60.2   | -200   | 10     | 6      | 136    | 19    | -7    | 26     | -200   | 9000   | 16.14 |
| ST86-088      | -5     | 1      | 697    | -100   | 800    | 37     | 2300   | 6      | 20     | 214    | 400    | 3.5    | -2     | 0.22   | -20    | 0.3    | 95.7   | -10    | 66.4   | -200   | 11     | 7      | 171    | 22    | -7    | 25     | -200   | 9200   | 23.27 |
| ST86-089      | -5     | 3      | 350    | -100   | 730    | 54     | 1900   | 6      | 21     | 200    | 350    | 3.5    | -2     | 0.26   | -20    | 0.3    | 95.8   | -10    | 60.4   | -200   | 10     | 7      | 137    | 20    | -7    | 25     | -200   | 7700   | 27.27 |
| ST86-090      | -5     | 124    | 210    | -100   | 1020   | 340    | 5770   | 15     | 25     | 140    | 480    | 2.4    | -2     | 0.25   | 390    | 18     | 80.1   | -10    | 76     | -200   | 8      | 6      | 83.1   | 11    | -8    | 21     | 450    | 6100   | 7.64  |
| ST86-101      | -5     | 3      | 91     | -100   | 710    | 39     | 1500   | 5      | 18     | 202    | 340    | 3      | -2     | 0.26   | 27     | 0.5    | 95     | -10    | 59.3   | -200   | 10     | 7      | 139    | 19    | -5    | 24     | -200   | 8500   | 14.84 |
| ST86-102      | -5     | 2      | 360    | 540    | 710    | 37     | 2000   | 3      | 17     | 220    | 380    | 3.3    | -2     | 0.23   | 35     | 0.6    | 91.8   | -10    | 66.5   | -200   | 10     | 7      | 164    | 21    | 6     | 25     | -200   | 9000   | 21.9  |
| ST86-103      | -5     | 3      | 470    | -100   | 880    | 35     | 2200   | 5      | 20     | 255    | 450    | 3.7    | -2     | 0.25   | -20    | 0.3    | 91.8   | -10    | 77.4   | -200   | 14     | 7      | 201    | 26    | -5    | 22     | -200   | 8200   | 15.65 |
| ST86-104      | -5     | 3      | 410    | -100   | 710    | 37     | 1800   | 4      | 19     | 190    | 350    | 2.8    | -2     | 0.21   | -20    | 0.6    | 88.5   | -10    | 66.2   | -200   | 11     | 7      | 170    | 21    | 27    | 21     | -200   | 8400   | 20.34 |
| ST86-105      | -5     | 0.5    | 160    | -100   | 940    | 36     | 1900   | 3      | 21     | 253    | 440    | 2.9    | -2     | 0.25   | 27     | 0.3    | 97.2   | -10    | 73.9   | -200   | 13     | 7      | 206    | 26    | 9     | 27     | -200   | 10000  | 15.87 |
| ST86-106      | -5     | 3      | 310    | -100   | 810    | 36     | 1900   | 4      | 20     | 259    | 390    | 3.3    | -2     | 0.14   | -20    | 0.4    | 98.1   | -10    | 59.5   | -200   | 10     | 6      | 166    | 23    | 6     | 26     | -200   | 11000  | 9.75  |
| ST86-107B     | -5     | 4      | 35     | -100   | 420    | 42     | 1300   | 7      | 17     | 190    | 180    | 2.9    | -2     | 0.27   | -20    | 0.3    | 98.3   | -10    | 44     | -200   | 10     | 5      | 66.3   | 15    | 7     | 22     | -200   | 7600   | 16.52 |
| ST86-108A     | -5     | 2      | 93     | -100   | 700    | 38     | 1200   | 6      | 18     | 213    | 340    | 3.4    | -2     | 0.33   | -20    | 0.1    | 95     | -10    | 60.5   | -200   | 11     | 6      | 131    | 20    | -5    | 24     | -200   | 8000   | 16.85 |

| Sample Number | Ag ppm | As ppm | Au Ppb | Ba ppm | Ce ppm | Co ppm | Cr ppm | Eu ppm | Fe pct | Hf ppm | La ppm | Lu ppm | Mo ppm | Na ppm | Ni ppm | Sb ppm | Sc ppm | Se ppm | Sm ppm | Sn ppm | Ta ppm | Tb ppm | Th ppm | U ppm | W ppm | Yb ppm | Zn ppm | Zr ppm | Wt g  |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|--------|--------|-------|
| SI86-108B     | -5     | 0.5    | 628    | -100   | 690    | 34     | 840    | 6      | 17     | 216    | 310    | 3.4    | -2     | 0.3    | 37     | 0.2    | 103    | -10    | 57.9   | -200   | 11     | 7      | 118    | 20    | 7     | -200   | 9000   | 13.14  |       |
| SI86-109      | -5     | 7      | 130    | -100   | 660    | 44     | 2300   | 6      | 20     | 190    | 300    | 3.6    | -2     | 0.25   | -20    | 0.9    | 99.4   | -10    | 53.4   | -200   | 10     | 6      | 125    | 17    | -5    | 25     | -200   | 7300   | 13.45 |
| SI86-110      | -5     | 3      | 450    | -100   | 820    | 42     | 2000   | 5      | 20     | 230    | 400    | 3.5    | -2     | 0.3    | -20    | 0.5    | 92.3   | -10    | 64.3   | -200   | 12     | 7      | 172    | 21    | -5    | 26     | -200   | 8800   | 14.69 |
| SI86-111      | -5     | 3      | 999    | -100   | 780    | 45     | 1600   | 6      | 21     | 213    | 380    | 3.6    | -2     | 0.3    | -20    | 0.3    | 100    | -10    | 61.5   | -200   | 12     | 6      | 165    | 21    | -6    | 27     | -200   | 9400   | 22.6  |
| SI86-112      | -5     | 12     | 52     | -100   | 480    | 59     | 2300   | 4      | 19     | 140    | 240    | 2      | -2     | 0.25   | 62     | 0.9    | 77.3   | -10    | 47     | -200   | 12     | 5      | 121    | 14    | 12    | 17     | -200   | 6000   | 13    |
| SI86-114      | -5     | 8      | 310    | -100   | 610    | 43     | 2500   | 4      | 19     | 190    | 300    | 2.9    | -2     | 0.22   | 33     | 0.8    | 91.7   | -10    | 44     | -200   | 11     | 5      | 104    | 14    | 8     | 21     | -200   | 6200   | 8.07  |
| SI86-115      | -5     | 2      | 525    | -100   | 680    | 42     | 6370   | 3      | 17     | 283    | 320    | 3.4    | -2     | 0.16   | 32     | 0.9    | 90.5   | -10    | 49     | -200   | 10     | 6      | 136    | 21    | -5    | 26     | 240    | 11000  | 3.66  |
| SI86-116      | -5     | 23     | 62     | -100   | 800    | 64     | 3600   | 5      | 22     | 267    | 360    | 3.1    | -2     | 0.26   | 36     | 2.2    | 94.2   | -10    | 57     | -200   | 9      | 7      | 155    | 22    | -5    | 26     | -200   | 382    | 3.82  |
| SI86-117      | -5     | 13     | 793    | -100   | 380    | 44     | 2800   | 2      | 19     | 84     | 170    | 2.4    | -2     | 0.32   | -20    | 0.7    | 82.8   | -10    | 32     | -200   | 8      | 4      | 74.6   | 8.5   | 7     | 17     | -200   | 3400   | 6.49  |
| SI86-118      | -5     | 4      | 230    | -100   | 700    | 46     | 1600   | 5      | 20     | 214    | 330    | 3.4    | -2     | 0.27   | -20    | 0.9    | 93.2   | -10    | 59.7   | -200   | 10     | 6      | 143    | 20    | -4    | 24     | -200   | 8400   | 19.58 |
| SI86-119      | -5     | 3      | 59     | -100   | 760    | 43     | 1400   | 7      | 19     | 217    | 360    | 3.2    | -2     | 0.24   | -20    | 0.4    | 99.4   | -10    | 62.5   | -200   | 10     | 7      | 154    | 21    | 9     | 26     | -200   | 9200   | 8.42  |
| SI86-120      | -5     | 3      | 140    | -100   | 660    | 42     | 1500   | 7      | 19     | 150    | 310    | 3.2    | -2     | 0.27   | 24     | 0.3    | 98.5   | -10    | 58.5   | -200   | 10     | 6      | 136    | 18    | 7     | 24     | -200   | 6500   | 14.32 |
| SI86-121      | -5     | 5      | 320    | -100   | 670    | 47     | 1900   | 4      | 18     | 180    | 320    | 2.5    | -2     | 0.37   | 52     | 0.5    | 81.4   | -10    | 59.7   | -200   | 10     | 6      | 155    | 19    | 6     | 22     | -200   | 7600   | 18.21 |
| SI86-122      | -5     | 4      | 370    | -100   | 710    | 42     | 1900   | 5      | 19     | 208    | 350    | 2.8    | -2     | 0.35   | 30     | 0.5    | 81.1   | -10    | 69.2   | -200   | 14     | 7      | 181    | 22    | -5    | 23     | -200   | 9200   | 21.18 |
| SI86-123      | -5     | 5      | 210    | -100   | 610    | 55     | 2100   | 5      | 19     | 190    | 300    | 2.7    | -2     | 0.38   | 38     | 0.9    | 90.7   | -10    | 56.6   | -200   | 11     | 7      | 124    | 17    | 7     | 22     | -200   | 7600   | 19.49 |
| SI86-124      | -5     | 8      | 813    | -100   | 510    | 48     | 2100   | 5      | 22     | 140    | 240    | 2.7    | -2     | 0.27   | 30     | 1      | 97.9   | -10    | 46     | -200   | 11     | 7      | 150    | 21    | 7     | 25     | -200   | 9100   | 21.16 |
| SI86-125      | -5     | 4      | 76     | -100   | 710    | 47     | 1700   | 5      | 21     | 170    | 380    | 3.1    | -2     | 0.19   | -20    | 0.3    | 102    | -10    | 62.8   | -200   | 11     | 7      | 172    | 21    | 10    | 29     | -200   | 5900   | 16.63 |
| SI87-1B       | -5     | 4      | 2.5    | -100   | 760    | 39     | 1400   | 3      | 22     | 150    | 390    | 3.2    | -2     | 0.27   | -20    | 0.1    | 103    | -10    | 63.1   | -200   | 10     | 7      | 178    | 18    | -6    | 29     | -200   | 6300   | 13.88 |
| SI87-2B       | -5     | 0.5    | 200    | -100   | 760    | 39     | 1500   | 5      | 20     | 180    | 400    | 3.1    | -2     | 0.28   | -20    | 0.2    | 98.5   | -10    | 62.6   | -200   | 9      | 6      | 167    | 20    | -6    | 28     | -200   | 8200   | 20.64 |
| SI87-5B       | -5     | 2      | 20     | -100   | 720    | 38     | 1900   | 3      | 21     | 150    | 370    | 3      | -2     | 0.18   | -20    | 0.3    | 98.7   | -10    | 58.6   | -200   | 10     | 6      | 159    | 17    | -6    | 27     | -200   | 6300   | 19.15 |
| SI87-6        | -5     | 3      | 669    | -100   | 770    | 36     | 1600   | -2     | 21     | 170    | 370    | 2.8    | -2     | 0.17   | -20    | 0.3    | 100    | -10    | 59.1   | -200   | 10     | 6      | 166    | 19    | -6    | 25     | -200   | 7700   | 17.77 |
| SI87-7A       | -5     | 0.5    | 77     | -100   | 710    | 31     | 1500   | 4      | 19     | 170    | 370    | 2.8    | -2     | 0.14   | -20    | 0.2    | 97     | -10    | 63.8   | -200   | 11     | 6      | 182    | 20    | 6     | 28     | -200   | 7200   | 18.05 |
| SI87-9        | -5     | 4      | 8130   | -100   | 550    | 44     | 1800   | 3      | 20     | 130    | 340    | 3.3    | -5     | 0.21   | -20    | 0.2    | 91.4   | -10    | 60.8   | -200   | 13     | 5      | 147    | 18    | 24    | 21     | 200    | 6600   | 48.55 |
| SI87-10B      | -5     | 4      | 350    | -100   | 700    | 44     | 2300   | -2     | 19     | 213    | 390    | 3      | -2     | 0.22   | -20    | 0.3    | 96.2   | -10    | 60.7   | -200   | 11     | 6      | 170    | 22    | -6    | 26     | -200   | 9100   | 17.39 |
| SI87-11B      | -5     | 0.5    | 1860   | -100   | 740    | 36     | 1500   | -2     | 21     | 150    | 410    | 3.6    | -2     | 0.24   | -20    | 0.1    | 108    | -10    | 66.3   | -200   | 11     | 7      | 174    | 20    | 9     | 29     | 220    | 7100   | 27.51 |
| SI87-12A      | -5     | 3      | 320    | -100   | 450    | 37     | 1800   | -2     | 20     | 81     | 230    | 2.3    | -2     | 0.47   | -20    | 0.2    | 89.4   | -10    | 34     | -200   | 7      | 5      | 115    | 10    | 7     | 22     | -200   | 3600   | 8.13  |
| SI87-12B      | -5     | 3      | 130    | -100   | 840    | 34     | 1300   | 4      | 20     | 206    | 470    | 3.2    | -2     | 0.26   | -20    | 0.3    | 97.8   | -10    | 70.1   | -200   | 13     | 7      | 201    | 23    | 11    | 29     | -200   | 9300   | 18.07 |
| SI87-13       | -5     | 10     | 330    | -100   | 660    | 48     | 2000   | 4      | 18     | 242    | 460    | 2.8    | -2     | 0.22   | -20    | 0.3    | 96.2   | -10    | 67.3   | -200   | 15     | 6      | 205    | 24    | -8    | 30     | 210    | 9300   | 17.59 |
| SI87-011      | -5     | 3      | 55     | -100   | 880    | 41     | 1600   | 3      | 20     | 298    | 480    | 3.7    | -2     | 0.21   | -20    | 0.3    | 96.2   | -10    | 67.3   | -200   | 11     | 8      | 217    | 28    | -4    | 32     | -200   | 13000  | 15.49 |
| SI87-013      | -5     | 3      | 5760   | -100   | 740    | 48     | 1700   | 3      | 21     | 223    | 410    | 3.5    | -2     | 0.28   | -20    | 0.3    | 104    | -10    | 59.8   | -200   | 13     | 7      | 190    | 22    | 8     | 27     | -200   | 9200   | 17.18 |
| SI87-016      | -5     | 3      | 250    | -100   | 680    | 37     | 1500   | 4      | 20     | 227    | 410    | 3.5    | -2     | 0.26   | -20    | 0.2    | 94.8   | -10    | 64.5   | -200   | 14     | 7      | 184    | 22    | -4    | 29     | -200   | 10000  | 21.25 |
| SI87-018      | -5     | 2      | 2230   | -100   | 720    | 33     | 1600   | -2     | 18     | 200    | 390    | 2.8    | -2     | 0.2    | -20    | 0.1    | 94.8   | -10    | 64.5   | -200   | 10     | 7      | 184    | 22    | -4    | 27     | -200   | 10000  | 20.13 |
| SI87-022      | -5     | 0.5    | 250    | -100   | 970    | 41     | 1500   | -2     | 20     | 306    | 606    | 3.9    | -4     | 0.19   | -20    | 0.2    | 102    | -10    | 61.2   | -200   | 15     | 8      | 295    | 36    | 6     | 31     | -200   | 15000  | 21.87 |
| SI87-036      | -5     | 4      | 240    | -100   | 680    | 37     | 1500   | 3      | 19     | 228    | 360    | 3.3    | -2     | 0.24   | -20    | 0.4    | 102    | -10    | 60     | -200   | 11     | 6      | 164    | 23    | -4    | 28     | -200   | 10000  | 14.09 |
| SI87-038      | -5     | 0.5    | 95     | -100   | 650    | 33     | 1200   | -2     | 18     | 180    | 380    | 3.3    | -2     | 0.24   | -20    | 0.2    | 98.7   | -10    | 61.9   | -200   | 11     | 6      | 163    | 21    | 5     | 28     | -200   | 8200   | 24.05 |
| SI87-069      | -5     | 3      | 90     | -100   | 690    | 38     | 1500   | 3      | 20     | 190    | 400    | 3.4    | -2     | 0.26   | -20    | 0.2    | 103    | -10    | 61.9   | -200   | 12     | 7      | 202    | 27    | 5     | 29     | -200   | 13000  | 17.18 |
| SI87-080      | -5     | 0.5    | 110    | -100   | 740    | 37     | 1700   | -2     | 22     | 220    | 440    | 3.4    | -2     | 0.17   | -20    | 0.3    | 100    | -10    | 68.3   | -200   | 12     | 6      | 184    | 22    | -4    | 28     | -200   | 9700   | 14.09 |
| SI87-082      | -5     | 0.5    | 1280   | -100   | 930    | 40     | 1600   | -2     | 25     | 244    | 655    | 4.3    | -5     | 0.18   | -20    | 0.3    | 99.1   | -10    | 64.1   | -200   | 14     | 7      | 194    | 22    | -4    | 28     | -200   | 7800   | 24.05 |
| SI87-086      | -5     | 0.5    | 1320   | -100   | 700    | 32     | 1600   | -2     | 20     | 222    | 410    | 3.2    | -2     | 0.15   | -20    | 0.3    | 101    | -10    | 61.5   | -200   | 11     | 6      | 184    | 22    | -4    | 28     | -200   | 10000  | 29.66 |
| SI87-090      | -5     | 2      | 300    | -100   | 810    | 42     | 1600   | 3      | 21     | 251    | 460    | 3.1    | -2     | 0.19   | -20    | 0.3    | 100    | -10    | 68     | -200   | 12     | 6      | 205    | 25    | -4    | 27     | -200   | 11000  | 15.54 |
| SI87-096      | -5     | 0.5    | 440    | -100   | 810    | 38     | 1700   | -2     | 21     | 229    | 460    | 2.6    | -2     | 0.15   | -20    | 0.3    | 98.1   | -10    | 64.5   | -200   | 11     | 6      | 218    | 23    | -5    | 25     | -200   | 10000  | 12.82 |
| SI87-098      | -5     | 10     | 2410   | -100   | 590    | 43     | 2100   | 2      | 17     | 160    | 320    | 2.4    | -2     | 0.19   | -20    | 0.4    | 84.1   | -10    | 54.7   | -200   | 14     | 6      | 165    | 19    | -4    | 23     | -200   | 7500   | 19.78 |
| SI87-100      | -5     | 7      | 1010   | -100   | 510    | 46     | 2000   | 2      | 18     | 160    | 270    | 1.9    | -2     | 0.2    | 21     | 0.5    | 85.4   | -10    | 52.1   | -200   | 10     | 6      | 141    | 18    | -2    | 22     | -200   | 7200   | 18.29 |
| SI87-102      | -5     | 0.5    | 1440   | -100   | 450    | 34     | 730    | 3      | 16     | 200    | 250    | 2.6    | -2     | 0.26   | -20    | 0.2    | 95.7   | -10    | 53     | -200   | 10     | 5      | 98     | 16    | 7     | 20     | -200   | 9500   | 33.24 |
| SI87-105      | -5     | 2      | 502    | -100   | 560    | 34     | 830    | -2     | 18     | 170    | 330    | 3.5    | -2     | 0.28   | -20    | 0.1    | 108    | -10    | 61.5   | -200   | 10     | 5      | 121    | 18    | 6     | 25     | 220    | 8600   | 54.87 |
| SI87-107      | -5     | 0      |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |       |       |        |        |        |       |

| Sample Number | Ag ppm | As ppm | Au ppb | Ba ppm | Ce ppm | Co ppm | Cr ppm | Eu ppm | Fe pct | Hf ppm | La ppm | Lu ppm | Mo ppm | Na ppm | Ni ppm | Sb ppm | Sc ppm | Se ppm | Sm ppm | Sn ppm | Ta ppm | Tb ppm | Th ppm | U ppm | W ppm | Yb ppm | Zn ppm | Zr ppm | Wt g  |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|--------|--------|-------|
| SI.87-219A    | -5     | 2      | 150    | -100   | 540    | 37     | 1400   | 2      | 18     | 150    | 300    | 2.2    | -2     | 0.19   | -20    | 0.3    | 85.7   | -10    | 58.4   | -200   | 11     | 6      | 141    | 18    | 9     | 21     | 200    | 6800   | 24.24 |
| SI.87-229     | -5     | 2      | 66     | -100   | 540    | 41     | 1600   | 3      | 19     | 140    | 290    | 2.9    | -2     | 0.17   | -20    | 0.3    | 96.5   | -10    | 55.1   | -200   | 10     | 7      | 151    | 22    | -4    | 22     | -200   | 6700   | 36.81 |
| SI.87-290     | -5     | 0.5    | 717    | -100   | 700    | 35     | 1100   | 4      | 16     | 120    | 210    | 2.2    | -2     | 0.32   | -20    | 0.1    | 84.5   | -10    | 49     | -200   | 8      | 4      | 66.5   | 13    | 6     | 18     | -200   | 5500   | 56.43 |
| SI.87-322     | -5     | 2      | 110    | -100   | 420    | 40     | 1100   | 4      | 17     | 130    | 220    | 2.4    | -2     | 0.21   | -20    | 0.2    | 81.6   | -10    | 62.7   | -200   | 7      | 5      | 85.3   | 16    | 11    | 19     | -200   | 6300   | 25.23 |
| SI.87-356     | -5     | 0.5    | 400    | -100   | 870    | 36     | 1800   | 6      | 20     | 217    | 511    | 3.6    | -2     | 0.17   | -20    | 0.3    | 98     | -10    | 77.3   | -200   | 13     | 7      | 221    | 25    | 9     | 32     | -200   | 9600   | 21.99 |
| SI.87-357     | -5     | 0.5    | 500    | -100   | 810    | 35     | 1800   | 2      | 20     | 202    | 490    | 3.7    | -2     | 0.13   | -20    | 0.1    | 96.5   | -10    | 71.4   | -200   | 12     | 6      | 204    | 24    | 5     | 31     | -200   | 9200   | 29.27 |
| SI.87-358     | -5     | 3      | 280    | -100   | 740    | 38     | 2300   | -2     | 20     | 222    | 400    | 3.3    | -2     | 0.18   | -20    | 0.3    | 100    | -10    | 61.5   | -200   | 10     | 6      | 183    | 23    | 7     | 29     | 240    | 9900   | 18.5  |
| SI.87-359     | -5     | 2      | 150    | -100   | 680    | 38     | 1900   | -2     | 21     | 210    | 380    | 3.3    | -2     | 0.17   | -20    | 0.3    | 102    | -10    | 60.7   | -200   | 12     | 6      | 172    | 21    | -5    | 29     | -200   | 9300   | 24.34 |
| SI.87-361     | -5     | 3      | 795    | -100   | 620    | 36     | 1600   | 2      | 19     | 170    | 350    | 2.9    | -2     | 0.21   | -20    | 0.3    | 97     | -10    | 57.8   | -200   | 10     | 6      | 158    | 18    | -5    | 27     | -200   | 7400   | 25.78 |
| SI.87-364     | -5     | 8      | 4500   | -100   | 750    | 37     | 1900   | 4      | 21     | 234    | 410    | 3.6    | -2     | 0.17   | -20    | 0.5    | 104    | -10    | 62.4   | -200   | 12     | 6      | 183    | 23    | 7     | 28     | -200   | 11000  | 15.07 |
| SI.87-394     | -5     | 0.5    | 170    | -100   | 900    | 32     | 2200   | 5      | 21     | 237    | 537    | 4.1    | -2     | 0.21   | -20    | 0.3    | 105    | -10    | 80.5   | -200   | 13     | 7      | 221    | 28    | -6    | 35     | 270    | 10000  | 26.81 |
| SI.87-411     | -5     | 0.5    | 55     | -100   | 380    | 32     | 670    | 4      | 15     | 110    | 200    | 2.5    | -2     | 0.24   | -20    | 0.1    | 90.4   | -10    | 66     | -200   | 10     | 7      | 63.9   | 13    | -4    | 21     | -200   | 4700   | 36    |
| SI.87-412     | -5     | 0.5    | 42     | -100   | 410    | 26     | 660    | 5      | 15     | 120    | 220    | 2.7    | -2     | 0.2    | -20    | 0.1    | 92.7   | -10    | 50.3   | -200   | 8      | 5      | 66.3   | 13    | 7     | 21     | -200   | 6000   | 38.45 |
| SI.87-415     | -5     | 0.5    | 33     | -100   | 210    | 34     | 410    | 4      | 14     | 97     | 110    | 2.2    | -2     | 0.31   | -20    | 0.2    | 100    | -10    | 30     | -200   | 7      | 4      | 27     | 8.2   | -2    | 18     | -200   | 4300   | 37.25 |
| SI.87-439     | -5     | 0.5    | 75     | -100   | 670    | 30     | 1600   | 2      | 18     | 150    | 370    | 3.6    | -2     | 0.13   | -20    | 0.2    | 100    | -10    | 61.6   | -200   | 11     | 6      | 144    | 19    | -5    | 28     | 220    | 7000   | 28    |
| SI.87-440     | -5     | 0.5    | 150    | -100   | 730    | 29     | 2100   | 2      | 21     | 160    | 400    | 3.8    | -2     | 0.19   | -20    | 0.3    | 109    | -10    | 68     | -200   | 12     | 7      | 163    | 20    | 10    | 30     | -200   | 7000   | 30.73 |
| SI.87-521     | -5     | 3      | 42     | -100   | 610    | 37     | 1200   | 4      | 18     | 150    | 330    | 3.2    | -2     | 0.2    | -20    | 0.3    | 98.5   | -10    | 56.8   | -200   | 9      | 5      | 133    | 18    | -5    | 24     | -200   | 6700   | 32.49 |
| SI.87-527     | -5     | 3      | 48     | -100   | 560    | 37     | 1200   | 3      | 18     | 140    | 310    | 3.2    | -2     | 0.21   | -20    | 0.3    | 97.9   | -10    | 55.5   | -200   | 9      | 5      | 126    | 17    | -5    | 25     | -200   | 6500   | 35.13 |
| SI.87-546     | -5     | 0.5    | 150    | -100   | 620    | 33     | 1200   | 4      | 19     | 150    | 340    | 2.9    | -2     | 0.18   | -20    | 0.2    | 90.5   | -10    | 62.5   | -200   | 11     | 7      | 160    | 20    | 5     | 25     | -200   | 7000   | 28.71 |
| SI.87-547     | -5     | 0.5    | 120    | -100   | 590    | 30     | 1000   | -2     | 18     | 170    | 340    | 3      | -2     | 0.19   | -20    | 0.3    | 91     | -10    | 67.3   | -200   | 11     | 7      | 154    | 22    | -5    | 24     | 220    | 8100   | 37.54 |
| SI.87-548     | -5     | 0.5    | 270    | -100   | 750    | 40     | 1800   | 3      | 21     | 211    | 410    | 3.6    | -2     | 0.15   | -20    | 0.1    | 103    | -10    | 63.8   | -200   | 12     | 7      | 204    | 23    | -6    | 29     | -200   | 9300   | 16.24 |
| SI.87-551     | -5     | 2      | 140    | -100   | 660    | 43     | 2000   | -2     | 21     | 212    | 350    | 3.1    | -2     | 0.24   | -20    | 0.3    | 99.2   | -10    | 54.8   | -200   | 10     | 6      | 163    | 20    | -5    | 30     | -200   | 9600   | 17.24 |
| SI.87-560     | -5     | 2      | 160    | -100   | 840    | 34     | 1500   | 5      | 20     | 211    | 450    | 3.6    | -2     | 0.24   | -20    | 0.3    | 103    | -10    | 68.4   | -200   | 12     | 7      | 202    | 23    | -6    | 31     | -200   | 9500   | 17.23 |

|           |    |     |      |      |      |     |       |   |    |     |     |     |    |      |     |      |       |     |      |      |    |   |     |    |    |    |      |       |       |
|-----------|----|-----|------|------|------|-----|-------|---|----|-----|-----|-----|----|------|-----|------|-------|-----|------|------|----|---|-----|----|----|----|------|-------|-------|
| SI.87-560 | -5 | 5   | 644  | -100 | 680  | 44  | 2030  | 4 | 20 | 193 | 349 | 3.1 | -2 | 0.24 | -20 | 0.6  | 95.6  | -10 | 59.5 | -200 | 11 | 6 | 149 | 19 | -6 | 25 | -200 | 8270  | 20.56 |
| SI.87-560 | -5 | 124 | 8130 | -100 | 1190 | 340 | 10400 | 3 | 25 | 306 | 655 | 4.3 | -2 | 0.47 | -20 | 18.0 | 109.0 | -10 | 94.3 | -200 | 16 | 9 | 295 | 36 | -6 | 36 | -200 | 15000 | 67.36 |
| SI.87-560 | -5 | 0.5 | 2.5  | -100 | 210  | 26  | 410   | 2 | 14 | 81  | 110 | 1.6 | -2 | 0.12 | -20 | 0.1  | 66.7  | -10 | 30.0 | -200 | 6  | 4 | 27  | 8  | -6 | 13 | -200 | 3400  | 3.66  |
| SI.87-560 | -5 | 11  | 1184 | -100 | 161  | 27  | 1287  | 2 | 2  | 45  | 93  | 0.5 | -2 | 0.06 | -20 | 1.6  | 7.0   | -10 | 11.2 | -200 | 2  | 1 | 45  | 4  | -6 | 4  | -200 | 1915  | 10.87 |

**Aultman Samples, Churchill Township**

| Sample Number | Ag ppm | As ppm | Au ppb | Ba ppm | Ce ppm | Co ppm | Cr ppm | Eu ppm | Fe pct | Hf ppm | La ppm | Lu ppm | Mo ppm | Na ppm | Ni ppm | Sb ppm | Sc ppm | Se ppm | Sm ppm | Sn ppm | Ta ppm | Tb ppm | Th ppm | U ppm | W ppm | Yb ppm | Zn ppm | Zr ppm | Wt g  |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|--------|--------|-------|
| JTA-3B        | -5     | 12     | 1240   | -100   | 520    | 46     | 2500   | 3      | 20     | 150    | 260    | 2.7    | -2     | 0.3    | 39     | 1.3    | 101    | -10    | 44     | -200   | 9      | 5      | 98.8   | 13    | -6    | 23     | -200   | 6300   | 15.75 |
| JTA-7         | -5     | 9      | 140    | -100   | 500    | 43     | 2500   | 4      | 21     | 140    | 250    | 2.7    | -2     | 0.26   | -20    | 1.2    | 97.2   | -10    | 42     | -200   | 10     | 5      | 106    | 13    | -6    | 23     | -200   | 6100   | 11.39 |
| JTA-8A        | -5     | 12     | 100    | -100   | 480    | 44     | 2400   | 4      | 20     | 140    | 230    | 2.2    | -2     | 0.22   | 33     | 1.3    | 97.1   | -10    | 41     | -200   | 8      | 5      | 92.2   | 12    | -6    | 22     | -200   | 5900   | 11    |
| JTA-9         | -5     | 7      | 2.5    | -100   | 460    | 44     | 3100   | 5      | 20     | 140    | 220    | 2.1    | -2     | 0.22   | 55     | 0.9    | 95.5   | -10    | 39     | -200   | 8      | 5      | 93.9   | 12    | -6    | 22     | -200   | 6100   | 6.02  |
| JTA-11        | -5     | 7      | 575    | -100   | 450    | 41     | 2200   | 3      | 19     | 150    | 230    | 2.3    | -2     | 0.18   | -20    | 1.2    | 88     | -10    | 41     | -200   | 8      | 5      | 106    | 13    | 10    | 19     | -200   | 5900   | 14.27 |
| JTA-12        | -5     | 8      | 110    | -100   | 460    | 38     | 1900   | 2      | 17     | 170    | 240    | 2.1    | -2     | 0.26   | 35     | 1.1    | 87.3   | -10    | 46     | -200   | 9      | 6      | 108    | 15    | 6     | 20     | -200   | 7400   | 11    |
| JTA-14        | 8      | 18     | 1620   | -100   | 420    | 48     | 2000   | 3      | 19     | 130    | 200    | 2.1    | -2     | 0.18   | 27     | 1.9    | 90     | -10    | 39     | -200   | 8      | 5      | 79.9   | 11    | -6    | 20     | -200   | 5400   | 8.71  |
| JTA-17        | -5     | 9      | 160    | -100   | 520    | 46     | 2700   | 4      | 21     | 170    | 260    | 2.4    | -2     | 0.23   | -20    | 1.2    | 98.6   | -10    | 41     | -200   | 11     | 5      | 115    | 14    | -6    | 23     | -200   | 6800   | 9.35  |
| JTA-17        | -5     | 10     | 493    | -100   | 476    | 44     | 2413   | 4      | 20     | 149    | 236    | 2.3    | -2     | 0.23   | -20    | 1.3    | 94     | -10    | 42     | -200   | 9      | 5      | 100    | 13    | -6    | 22     | -200   | 6238   | 10.94 |

Control Samples: INA analysis of non-magnetic fraction of IIMC (Klip control)

| Sample Number | Ag ppm | As ppm | Au ppb | Ba ppm | Ce ppm | Co ppm | Cr ppm | Eu ppm | Fe pct | Hf ppm | La ppm | Lu ppm | Mo ppm | Na ppm | Ni ppm | Sb ppm | Sc ppm | Se ppm | Sm ppm | Sn ppm | Ta ppm | Tb ppm | Th ppm | U ppm | W ppm | Yb ppm | Zn ppm | Zr ppm | Wt g  |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|--------|--------|-------|
| ST86-100B     | -5     | -1     | -5     | 160    | 590    | 40     | 250    | 6      | 21     | 304    | 290    | 4.9    | -2     | 0.38   | -20    | -0.2   | 76.5   | -10    | 66.2   | -200   | 9      | 8      | 54.8   | 25    | -5    | 33     | -200   | 13000  | 25.62 |
| ST86-017      | -5     | 2      | -5     | -100   | 630    | 35     | 240    | 7      | 21     | 322    | 280    | 4.3    | -2     | 0.32   | -20    | -0.2   | 74.1   | -10    | 59.6   | -200   | 8      | 8      | 58.8   | 24    | -5    | 35     | -200   | 13000  | 8.17  |
| ST86-091      | -5     | 2      | -5     | -100   | 560    | 38     | 230    | 4      | 18     | 310    | 260    | 3.2    | -2     | 0.34   | -20    | -0.2   | 66.2   | -10    | 64.1   | -200   | 8      | 8      | 59.3   | 26    | -6    | 28     | -200   | 13000  | 14.65 |
| SL87-083      | -5     | -1     | -5     | 140    | 510    | 37     | 200    | 5      | 21     | 297    | 270    | 4      | -2     | 0.36   | -20    | -0.2   | 77.6   | -10    | 58.1   | -200   | 9      | 9      | 58.4   | 26    | -7    | 36     | -200   | 13000  | 24.99 |
| SL87-165      | -5     | -1     | -5     | -100   | 470    | 35     | 210    | 4      | 18     | 276    | 230    | 2.3    | -2     | 0.34   | -20    | -0.2   | 66.7   | -10    | 50.7   | -200   | 7      | 8      | 52.1   | 22    | -5    | 27     | -200   | 11000  | 16.91 |
| SL87-417      | -5     | -1     | -5     | -100   | 480    | 35     | 190    | 4      | 20     | 262    | 250    | 4.2    | -2     | 0.3    | -20    | -0.2   | 74.7   | -10    | 55.3   | -200   | 8      | 7      | 47     | 22    | -4    | 31     | -200   | 11000  | 26.91 |
| BL87-3B       | -5     | -1     | -5     | -100   | 520    | 32     | 200    | 4      | 21     | 277    | 260    | 4.3    | -2     | 0.28   | -20    | -0.2   | 77.3   | -10    | 52.4   | -200   | 8      | 7      | 50     | 21    | -5    | 34     | -200   | 12000  | 13.91 |
| JTA-4         | -5     | -1     | -5     | -100   | 530    | 37     | 200    | 3      | 21     | 304    | 280    | 4.1    | -2     | 0.33   | -20    | -0.2   | 76.1   | -10    | 57.5   | -200   | 8      | 8      | 54.3   | 24    | -5    | 34     | -200   | 14000  | 22.68 |

APPENDIX F. INA Analysis of magnetic fraction of HMC samples, Shining Tree Area

| Sample Number             | Ag | As | Au | Ba   | Ce  | Co    | Cr  | Eu | Fe   | Hf | La  | Lu   | Mo | Na    | Ni   | Sb   | Sc  | Se  | Sm  | Sn   | Ta | Tb | Th  | U    | W  | Yb | Zn   | Zr   |
|---------------------------|----|----|----|------|-----|-------|-----|----|------|----|-----|------|----|-------|------|------|-----|-----|-----|------|----|----|-----|------|----|----|------|------|
| BH86-1                    | -5 | 5  | -5 | -100 | -10 | 8360  | 75  | -2 | 63.7 | 4  | 8   | -0.5 | -2 | 0.11  | 230  | 0.4  | 19  | -10 | 2.1 | -200 | 2  | -1 | 1.7 | 0.6  | -2 | -5 | 410  | -500 |
| ST86-05                   | -5 | 5  | -5 | -100 | -10 | 8710  | 71  | -2 | 64.8 | 3  | 12  | -0.5 | -2 | 0.13  | 190  | 0.3  | 19  | -10 | 2.9 | -200 | 2  | -1 | 2.4 | 0.7  | -2 | -5 | 290  | -500 |
| ST86-015                  | -5 | 4  | -5 | -100 | -10 | 7600  | 71  | -2 | 69.3 | 3  | 6   | -0.5 | -2 | 0.15  | 190  | -0.2 | 17  | -10 | 1.4 | -200 | 2  | -1 | 1.8 | -0.5 | -2 | -5 | 310  | -500 |
| ST86-016                  | -5 | 12 | -5 | -100 | -10 | 13500 | 79  | -2 | 55.3 | 3  | 10  | -0.5 | -2 | 0.22  | 240  | 0.9  | 26  | -10 | 2.8 | -200 | 2  | -1 | 2.2 | 0.7  | -2 | -5 | 220  | -500 |
| ST86-021                  | -5 | 8  | -5 | -100 | 33  | 5360  | 73  | -2 | 55.7 | 7  | 26  | -0.5 | -2 | 0.22  | 140  | 1.2  | 32  | -10 | 7.1 | -200 | 3  | 1  | 4.8 | 1.5  | 2  | -5 | 260  | -500 |
| ST86-027                  | -5 | 4  | -5 | -100 | -10 | 21900 | 110 | -2 | 65.6 | 5  | 11  | -0.5 | -2 | 0.1   | 440  | -0.2 | 16  | -10 | 2.4 | -200 | 1  | -1 | 3.2 | 0.6  | -2 | -5 | 280  | -500 |
| ST86-030                  | -5 | 6  | -5 | -100 | -10 | 10600 | 70  | -2 | 56.3 | 5  | 14  | -0.5 | -2 | 0.2   | 180  | 0.3  | 29  | -10 | 3.5 | -200 | 2  | -1 | 2   | 0.8  | -2 | -5 | 280  | -500 |
| ST86-033                  | -5 | 5  | -5 | -100 | -10 | 11800 | 63  | -2 | 58.3 | 5  | 14  | -0.5 | -2 | 0.31  | 180  | 0.6  | 29  | -10 | 3.2 | -200 | 2  | -1 | 3.3 | 1.1  | 3  | -5 | 290  | -500 |
| ST86-037                  | -5 | 5  | -5 | -100 | -10 | 10300 | 73  | -2 | 63   | 3  | 10  | -0.5 | -2 | 0.14  | 230  | 0.5  | 27  | -10 | 3.2 | -200 | 2  | -1 | 2.2 | 0.6  | -2 | -5 | 370  | -500 |
| ST86-042                  | -5 | 10 | -5 | -100 | -10 | 5410  | 67  | -2 | 48   | 6  | 13  | -0.5 | -2 | 0.21  | 190  | 1.4  | 27  | -10 | 4.6 | -200 | 2  | -1 | 1.9 | 1    | -2 | -5 | 300  | -500 |
| ST86-043                  | -5 | 5  | -5 | -100 | -10 | 11000 | 77  | -2 | 64.5 | 4  | 9   | -0.5 | -2 | 0.1   | 240  | 0.5  | 20  | -10 | 2.4 | -200 | 2  | -1 | 2.3 | 0.6  | -2 | -5 | 310  | -500 |
| ST86-048                  | -5 | 6  | -5 | -100 | -10 | 7320  | 92  | -2 | 59.3 | 5  | 13  | -0.5 | -2 | 0.18  | 160  | 0.7  | 30  | -10 | 3.6 | -200 | 2  | -1 | 2.4 | 0.8  | -2 | -5 | 330  | -500 |
| ST86-049                  | -5 | 8  | -5 | -100 | -10 | 7770  | 75  | -2 | 56.4 | 5  | 12  | -0.5 | -2 | 0.21  | 180  | 1.1  | 27  | -10 | 3.5 | -200 | 2  | -1 | 3.2 | 0.6  | -2 | -5 | 350  | -500 |
| ST86-057                  | -5 | 3  | -5 | -100 | -10 | 8690  | 57  | -2 | 66   | 3  | 9   | -0.5 | -2 | 0.09  | 200  | -0.2 | 14  | -10 | 1.9 | -200 | 1  | -1 | 2.6 | 0.7  | -2 | -5 | 310  | -500 |
| ST86-059                  | -5 | 7  | -5 | -100 | -10 | 8410  | 74  | -2 | 64.4 | 4  | 11  | -0.5 | -2 | 0.12  | 170  | 0.5  | 23  | -10 | 2.9 | -200 | 2  | -1 | 2.8 | 0.7  | -2 | -5 | 330  | -500 |
| ST86-063                  | -5 | 4  | -5 | -100 | -10 | 4000  | 58  | -2 | 59.7 | 4  | 12  | -0.5 | -2 | 0.13  | 110  | -0.2 | 25  | -10 | 3.4 | -200 | 2  | -1 | 3.2 | 1.2  | -2 | -5 | 350  | -500 |
| ST86-074                  | -5 | 4  | -5 | -100 | -10 | 9080  | 70  | -2 | 71.1 | 3  | 6   | -0.5 | -2 | 0.08  | 210  | -0.2 | 15  | -10 | 1.4 | -200 | 1  | -1 | 2.3 | -0.5 | -2 | -5 | 350  | -500 |
| ST86-077A                 | -5 | 4  | -5 | -100 | -10 | 6890  | 60  | -2 | 54.9 | 5  | 11  | -0.5 | -2 | 0.23  | 140  | 0.7  | 31  | -10 | 3.7 | -200 | 2  | -1 | 2.1 | 1    | -2 | -5 | 370  | -500 |
| ST86-077B                 | -5 | 4  | 52 | -100 | -10 | 8930  | 71  | -2 | 70.2 | 4  | 7   | -0.5 | -2 | 0.06  | 170  | 0.3  | 16  | -10 | 1.8 | -200 | 1  | -1 | 2.2 | 0.7  | -2 | -5 | 340  | -500 |
| ST86-079                  | -5 | 4  | -5 | -100 | -10 | 9650  | 71  | -2 | 68.3 | 3  | 8   | -0.5 | -2 | 0.06  | 210  | -0.2 | 14  | -10 | 1.7 | -200 | 1  | -1 | 2.4 | -0.5 | -2 | -5 | 330  | -500 |
| ST86-081                  | -5 | 4  | -5 | -100 | -10 | 9000  | 69  | -2 | 66.1 | 4  | 8   | -0.5 | -2 | 0.1   | 200  | 0.3  | 16  | -10 | 1.9 | -200 | 1  | -1 | 2.3 | 0.6  | -2 | -5 | 340  | -500 |
| ST86-082                  | -5 | 4  | -5 | -100 | -10 | 8710  | 68  | -2 | 58.3 | 3  | 7   | -0.5 | -2 | 0.15  | 160  | 0.3  | 21  | -10 | 2   | -200 | 2  | -1 | 2.2 | 0.6  | -2 | -5 | 400  | -500 |
| ST86-083                  | -5 | 4  | 21 | -100 | -10 | 7580  | 64  | -2 | 63   | 4  | 7   | -0.5 | -2 | 0.1   | 180  | 0.3  | 20  | -10 | 1.9 | -200 | 2  | -1 | 1.5 | 0.5  | -2 | -5 | 320  | -500 |
| ST86-084                  | -5 | 4  | 10 | -100 | -10 | 5180  | 58  | -2 | 64.2 | 4  | 7   | -0.5 | -2 | 0.15  | 120  | 0.3  | 20  | -10 | 2.2 | -200 | 2  | -1 | 2.1 | 0.8  | -2 | -5 | 380  | -500 |
| ST86-087                  | -5 | 2  | -5 | -100 | -10 | 10400 | 69  | -2 | 61   | 4  | 9   | -0.5 | -2 | 0.13  | 200  | -0.2 | 20  | -10 | 2.4 | -200 | 2  | -1 | 1.9 | -0.5 | -2 | -5 | 400  | -500 |
| ST86-088                  | -5 | 3  | 8  | -100 | -10 | 9980  | 65  | -2 | 61   | 5  | 7   | -0.5 | -2 | 0.09  | 210  | -0.2 | 16  | -10 | 2.2 | -200 | 2  | -1 | 2.1 | -0.5 | -2 | -5 | 320  | -500 |
| ST86-103                  | -5 | 3  | -5 | -100 | -10 | 9310  | 66  | -2 | 71.4 | 2  | 5   | -0.5 | -2 | 0.11  | 190  | -0.2 | 16  | -10 | 1.9 | -200 | 2  | -1 | 1.5 | -0.5 | -2 | -5 | 340  | -500 |
| ST86-108A                 | -5 | 3  | -5 | -100 | -10 | 3200  | 52  | -2 | 62.6 | 4  | 11  | -0.5 | -2 | 0.16  | 85   | -0.2 | 25  | -10 | 2.5 | -200 | 2  | -1 | 1.8 | -0.5 | -2 | -5 | 380  | -500 |
| ST86-109                  | -5 | 7  | 7  | -100 | -10 | 8950  | 72  | -2 | 61.9 | 5  | 12  | -0.5 | -2 | 0.17  | 210  | 0.9  | 26  | -10 | 3.5 | -200 | 2  | -1 | 2.3 | 0.8  | -2 | -5 | 240  | -500 |
| ST86-111                  | -5 | 4  | -5 | -100 | -10 | 6290  | 61  | -2 | 67.1 | 5  | 8   | -0.5 | -2 | 0.12  | 130  | -0.2 | 18  | -10 | 1.8 | -200 | 2  | -1 | 2.6 | 0.9  | -2 | -5 | 330  | -500 |
| ST86-112                  | -5 | 9  | -5 | -100 | -10 | 6150  | 68  | -2 | 52   | 4  | 8   | -0.5 | -2 | 0.18  | 180  | 1.9  | 22  | -10 | 2.6 | -200 | 2  | -1 | 2.5 | 0.7  | 7  | -5 | 250  | -500 |
| ST86-114                  | -5 | 6  | -5 | -100 | -10 | 8490  | 75  | -2 | 63.9 | 3  | 10  | -0.5 | -2 | 0.14  | 230  | 0.6  | 24  | -10 | 2.8 | -200 | 2  | -1 | 2   | 0.6  | -2 | -5 | 320  | -500 |
| ST86-118                  | -5 | 4  | -5 | -100 | -10 | 8840  | 73  | -2 | 69.4 | 4  | 8   | -0.5 | -2 | 0.09  | 200  | 0.2  | 16  | -10 | 1.8 | -200 | 2  | -1 | 2.2 | 0.6  | -2 | -5 | 280  | -500 |
| ST86-125                  | -5 | 7  | -5 | -100 | -10 | 6460  | 75  | -2 | 62.7 | 4  | 12  | -0.5 | -2 | 0.13  | 140  | 0.6  | 29  | -10 | 3.2 | -200 | 3  | -1 | 1.8 | 0.8  | -2 | -5 | 380  | -500 |
| BH87-4BM                  | -5 | 4  | -5 | -100 | -10 | 9580  | 79  | -2 | 68.5 | 6  | 19  | -0.5 | -2 | 0.1   | 180  | -0.2 | 16  | -10 | 2.2 | -200 | 2  | -1 | 8.7 | 0.7  | -2 | -5 | 360  | -500 |
| BH87-9M                   | -5 | 6  | -5 | -100 | -10 | 10700 | 140 | -2 | 63.1 | 4  | 10  | -0.5 | -2 | 0.06  | 380  | 0.3  | 16  | -10 | 2.2 | -200 | 2  | -1 | 2.3 | 0.9  | -2 | -5 | 270  | -500 |
| BH87-10BM                 | -5 | 7  | -5 | -100 | -10 | 11800 | 130 | -2 | 65.2 | 5  | 13  | -0.5 | -2 | 0.07  | 440  | 0.3  | 17  | -10 | 2.6 | -200 | 2  | -1 | 3.6 | 0.7  | -2 | -5 | 310  | -500 |
| SI87-353M                 | -5 | 4  | -5 | -100 | -10 | 8580  | 77  | -2 | 70   | 3  | 11  | -0.5 | -2 | 0.025 | 160  | -0.2 | 13  | -10 | 1.9 | -200 | 2  | -1 | 4.5 | 0.7  | -2 | -5 | 360  | -500 |
| SI87-571M                 | -5 | 4  | -5 | -100 | -10 | 10700 | 75  | -2 | 67.1 | 4  | 14  | -0.5 | -2 | 0.09  | 200  | -0.2 | 15  | -10 | 2.7 | -200 | 2  | -1 | 5.9 | 0.8  | -2 | -5 | 270  | -500 |
| SI87-572M                 | -5 | 4  | -5 | -100 | -10 | 8800  | 74  | -2 | 68.4 | 5  | 11  | -0.5 | -2 | 0.08  | 200  | -0.2 | 17  | -10 | 2.4 | -200 | 2  | -1 | 6.4 | 0.7  | -2 | -5 | 320  | -500 |
| AVERAGE                   | 5  |    |    |      |     | 8793  | 74  |    | 62.8 | 4  | 10  |      |    | 0.13  | 200  |      | 21  |     | 2.6 |      | 2  |    | 2.7 |      |    |    | 324  |      |
| MAXIMUM                   | 12 |    |    |      |     | 21900 | 140 |    | 71.4 | 7  | 26  |      |    | 0.31  | 440  |      | 32  |     | 7.1 |      | 3  |    | 8.7 |      |    |    | 410  |      |
| MINIMUM                   | 2  |    |    |      |     | 3200  | 52  |    | 48   | 2  | 5   |      |    | 0.03  | 85.0 |      | 13  |     | 1.2 |      | 1  |    | 1.5 |      |    |    | 220  |      |
| STD.DEV.                  | 2  |    |    |      |     | 2918  | 17  |    | 5.40 | 1  | 3.7 |      |    | 0.06  | 70.5 |      | 5.5 |     | 1.0 |      | 0  |    | 1.4 |      |    |    | 43.9 |      |
| No. below detection limit | 2  |    |    |      |     |       |     |    |      |    |     |      |    |       |      |      |     |     |     |      |    |    |     |      |    |    |      |      |

## APPENDIX G

### Fire Assay Analysis of Non-Magnetic and Magnetic Fractions of HMC Samples

Fire Assay (FA), Directly Coupled Plasma (DCP), Atomic Absorption (AA) or a combination of methods was used on 15 g or less portions of the non-magnetic or magnetic heavy mineral concentrate. The analyses were carried out by Bondar-Clegg & Company, Ottawa, Ontario.

The elements analyzed, the extraction techniques utilized, the methods of analysis and the lower detection limits are listed in the following table:

|    |            |                              |        |         |
|----|------------|------------------------------|--------|---------|
| Ag | Silver     | HCL-HNO <sub>3</sub> , (3:1) | AA     | 0.1 ppm |
| Au | Gold       | Aqua Regia                   | FA/DCP | 1 ppb   |
| Ba | Barium     | Borate Fusion                | DCP    | 1 ppm   |
| Co | Cobalt     | HCL-HNO <sub>3</sub> , (3:1) | AA     | 1 ppm   |
| Cr | Chromium   | Borate Fusion                | DCP    | 1 ppm   |
| Cu | Copper     | HCL-HNO <sub>3</sub> , (3:1) | AA     | 0.5 ppm |
| Mo | Molybdenum | HCL-HNO <sub>3</sub> , (3:1) | AA     | 1 ppm   |
| Ni | Nickel     | HCL-HNO <sub>3</sub> , (3:1) | AA     | 1 ppm   |
| Pb | Lead       | HCL-HNO <sub>3</sub> , (3:1) | AA     | 2 ppm   |
| Pd | Palladium  | Aqua Regia                   | FA/DCP | 1 ppb   |
| Pt | Platinum   | Aqua Regia                   | FA/DCP | 5 ppb   |
| Zn | Zinc       | HCL-HNO <sub>3</sub> , (3:1) | AA     | 0.5 ppm |

APPENDIX G. Fire assay analysis of magnetic fraction of HMC, Shining Tree Area.

| Sample Number | Ag ppm | Au ppb | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| BI186-1       | -0.1   | -4     | 44     | 29     | 6930   | 15.2   | 2      | 120    | 10     | -4     | -19    | 75.4   | 4        |
| ST86-005      | -0.1   | -4     | 21     | 27     | 6720   | 17.6   | 2      | 117    | 8      | -4     | -19    | 73.2   | 4        |
| ST86-015      | -0.1   | -5     | 21     | 26     | 5480   | 21.6   | 2      | 123    | 9      | -5     | -25    | 76.5   | 3        |
| ST86-016      | -0.1   | 4      | 66     | 34     | 11470  | 46.5   | 3      | 173    | 13     | -2     | -9     | 83.1   | 8        |
| ST86-021      | -0.1   | -5     | 54     | 35     | 4630   | 35.7   | 2      | 103    | 45     | -5     | -26    | 95.9   | 2.9      |
| ST86-027      | -0.1   | -3     | 25     | 46     | 17280  | 22.8   | 1      | 321    | 11     | -3     | -13    | 69.7   | 6        |
| ST86-030      | -0.1   | 3      | 58     | 27     | 9730   | 48.5   | 1      | 102    | 14     | -2     | -8     | 70.7   | 9        |
| ST86-033      | -0.1   | -8     | 78     | 25     | 9920   | 32.1   | 2      | 127    | 16     | -8     | -38    | 82.7   | 2        |
| ST86-037      | -0.1   | -8     | 40     | 27     | 7660   | 21.2   | 1      | 113    | 11     | -8     | -38    | 85.9   | 2        |
| ST86-042      | -0.1   | 4      | 80     | 32     | 5710   | 35.8   | 2      | 106    | 11     | -4     | -19    | 116.5  | 4        |
| ST86-043      | -0.1   | -3     | 27     | 28     | 9170   | 20.7   | 1      | 145    | 9      | -3     | -15    | 81.2   | 5        |
| ST86-048      | -0.1   | 5      | 58     | 42     | 5910   | 34.5   | 2      | 118    | 9      | -5     | -25    | 182.7  | 3        |
| ST86-049      | -0.1   | -6     | 53     | 33     | 6720   | 40.2   | 2      | 115    | 10     | -6     | -30    | 118.4  | 2.49     |
| ST86-057      | -0.1   | 1      | 5      | 21     | 7630   | 14.3   | 2      | 95     | 13     | -1     | -5     | 62.6   | 15       |
| ST86-059      | -0.1   | -3     | 75     | 30     | 6940   | 42.6   | 2      | 130    | 11     | -3     | -13    | 100.7  | 6        |
| ST86-063      | -0.1   | -8     | 101    | 25     | 3330   | 36     | 3      | 74     | 14     | -8     | -38    | 86.5   | 2        |
| ST86-074      | -0.1   | -3     | 42     | 29     | 7100   | 17.8   | 2      | 132    | 9      | -3     | -15    | 87.8   | 5        |
| ST86-076      | -0.1   | -6     | 55     | 28     | 6280   | 32.9   | 2      | 115    | 13     | -6     | -30    | 100.5  | 2.49     |
| ST86-077A     | -0.1   | -1     | 25     | 32     | 6630   | 18.5   | 2      | 127    | 9      | -1     | -5     | 99     | 15       |
| ST86-077B     | -0.1   | 68     | 81     | 30     | 7310   | 17.7   | 2      | 139    | 9      | -3     | -13    | 86.7   | 6        |
| ST86-079      | -0.1   | -3     | 21     | 30     | 8290   | 15.7   | 2      | 150    | 8      | -3     | -13    | 80.7   | 6        |
| ST86-081      | -0.1   | -5     | 30     | 31     | 7660   | 17.5   | 2      | 137    | 8      | -5     | -25    | 86.1   | 3        |
| ST86-082      | -0.1   | -8     | 42     | 31     | 7940   | 14.9   | 2      | 122    | 14     | -8     | -38    | 103.8  | 2        |
| ST86-083      | -0.1   | 42     | 34     | 27     | 6360   | 15     | 2      | 109    | 11     | 12     | -8     | 77.6   | 10       |
| ST86-084      | -0.1   | -5     | 64     | 23     | 4300   | 17.4   | 2      | 91     | 10     | -5     | -25    | 75.7   | 3        |
| ST86-087      | -0.1   | 12     | 47     | 30     | 8450   | 26     | 2      | 135    | 11     | -6     | -30    | 86.2   | 2.5      |
| ST86-088      | -0.1   | 4      | 47     | 28     | 8790   | 28     | 2      | 120    | 10     | 11     | -6     | 71.6   | 12       |
| ST86-089      | -0.1   | 3      | 72     | 29     | 8340   | 17.5   | 2      | 123    | 9      | -2     | -8     | 86.6   | 10       |
| ST86-103      | -0.1   | -2     | 32     | 24     | 8360   | 17.4   | 1      | 118    | 8      | 69     | -11    | 67.4   | 7        |
| ST86-108A     | -0.1   | -3     | 60     | 22     | 2910   | 24.3   | 2      | 62     | 10     | -3     | -15    | 73.3   | 5        |
| ST86-109      | -0.1   | -4     | 72     | 26     | 8070   | 15.8   | 2      | 126    | 28     | -4     | -19    | 71.8   | 4        |
| ST86-111      | -0.1   | -2     | 33     | 23     | 5340   | 19.6   | 1      | 82     | 10     | -2     | -8     | 72.5   | 9        |
| ST86-112      | -0.1   | 10     | 84     | 30     | 6950   | 21.5   | 2      | 127    | 102    | -5     | -25    | 88.1   | 3        |
| ST86-114      | -0.1   | -8     | 44     | 27     | 7000   | 21.4   | 2      | 131    | 11     | -8     | -38    | 76.4   | 2        |
| ST86-118      | -0.1   | 3      | 64     | 26     | 7400   | 13.7   | 2      | 119    | 10     | -3     | -15    | 74.3   | 5        |
| ST86-125      | -0.1   | -4     | 52     | 34     | 5860   | 34.5   | 3      | 91     | 11     | -4     | -19    | 118.8  | 4        |
| BI187-4B      | -0.1   | 4      | 64     | 31     | 7880   | 16.6   | 2      | 148    | 11     | -2     | -11    | 83.3   | 7        |
| BI187-9       | -0.1   | 2      | 46     | 75     | 9860   | 23.6   | 2      | 346    | 12     | 11     | -5     | 90.4   | 15       |
| BI187-10B     | -0.1   | 3      | 23     | 65     | 8940   | 21.7   | 2      | 387    | 10     | -3     | -13    | 91.6   | 6        |
| SL87-353      | -0.1   | 5      | 38     | 32     | 7170   | 13.9   | 2      | 111    | 9      | 15     | -13    | 77.3   | 6        |
| SL87-521      | -0.1   | -2     | 34     | 30     | 8440   | 15     | 2      | 145    | 8      | 2      | -8     | 69.7   | 9        |
| SL87-527      | -0.1   | 2      | 68     | 28     | 7370   | 12.2   | 1      | 121    | 10     | 10     | -8     | 76.3   | 9        |

|          |     |    |       |      |   |     |     |       |    |
|----------|-----|----|-------|------|---|-----|-----|-------|----|
| AVERAGE  | 50  | 31 | 7482  | 23.7 | 2 | 136 | 14  | 86.6  | 6  |
| MAXIMUM  | 101 | 75 | 17280 | 48.5 | 3 | 387 | 102 | 182.7 | 15 |
| MINIMUM  | 21  | 21 | 2910  | 12   | 1 | 62  | 8   | 63    | 2  |
| STD.DEV. | 20  | 10 | 2285  | 9.6  | 0 | 64  | 15  | 20.1  | 4  |

**Aultman Samples, Churchill Township**

| Sample Number | Ag ppm | Au ppb | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| JTA-3B        | -0.1   | 3      | 87     | 33     | 7400   | 25.9   | 2      | 125    | 11     | 10     | -13    | 89.2   | 6        |
| JTA-7         | -0.1   | -5     | 60     | 31     | 7150   | 22.7   | 3      | 128    | 11     | 10     | -25    | 99.1   | 3        |
| JTA-8A        | -0.1   | -6     | 60     | 33     | 7900   | 19.4   | 2      | 126    | 10     | -6     | -30    | 94.3   | 2.5      |
| JTA-9         | -0.1   | -15    | 78     | 31     | 7300   | 25.4   | 2      | 126    | 16     | 31     | -76    | 116.5  | 0.98     |
| JTA-11        | -0.1   | -3     | 60     | 35     | 7040   | 30.9   | 2      | 122    | 10     | -3     | -13    | 94.6   | 6        |
| JTA-12        | -0.1   | -8     | 69     | 33     | 6910   | 30.4   | 2      | 129    | 12     | -8     | -38    | 90.3   | 2        |
| JTA-14        | -0.1   | 12     | 74     | 31     | 7430   | 22.7   | 3      | 129    | 10     | -6     | -29    | 90.2   | 2.59     |
| JTA-17        | -0.1   | -6     | 78     | 34     | 7760   | 29.4   | 2      | 123    | 10     | 6      | -30    | 100.9  | 2.5      |

|         |    |    |      |      |   |     |    |       |   |
|---------|----|----|------|------|---|-----|----|-------|---|
| AVERAGE | 71 | 33 | 7361 | 25.9 | 2 | 126 | 11 | 96.9  | 3 |
| MAXIMUM | 87 | 35 | 7900 | 30.9 | 3 | 129 | 16 | 116.5 | 6 |
| MINIMUM | 60 | 31 | 6910 | 19.4 | 2 | 122 | 10 | 89.2  | 1 |

**Control samples: fire assay analysis of magnetic fraction of HMC (Fort Frances Control)**

| Sample Number | Ag ppm | Au ppb | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| BH86-2        | -0.1   | -3     | 60     | 44     | 1760   | 20.5   | 4      | 124    | 18     | -3     | -25    | 75.8   | 3        |
| ST86-038      | -0.1   | -3     | 40     | 44     | 1670   | 28.6   | 4      | 125    | 17     | -3     | -13    | 80.3   | 6        |
| ST86-086      | -0.1   | 11     | 60     | 52     | 1680   | 20.1   | 4      | 88     | 15     | 17     | -11    | 81.1   | 7        |
| JTA-4BM       | -0.1   | -2     | 55     | 38     | 1650   | 34.3   | 6      | 96     | 26     | -2     | -11    | 81.5   | 7        |

APPENDIX G: Fire assay analysis of non-magnetic fraction of HMC, Shining Tree Area

| Sample Number | Ag ppm | Au ppm | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| BI 186-1      | 0.1    | 833    | 46     | 6      | 2800   | 29.6   | 2      | 18     | 30     | 5      | 6      | 33.9   | 12       |
| BI 186-2      | 0.1    | 232    | 18     | 7      | 2870   | 25.4   | 2      | 17     | 24     | 16     | -6     | 32.8   | 13       |
| BI 186-5      | -0.1   | 4581   | 33     | 4      | 2220   | 15.3   | 1      | 12     | 33     | 5      | -6     | 26.1   | 13       |
| ST86-005      | -0.1   | 62     | 61     | 6      | 2400   | 29.8   | 2      | 14     | 25     | -2     | -8     | 38.6   | 10       |
| ST86-006A     | 0.1    | 5674   | 58     | 7      | 1880   | 18.8   | 1      | 15     | 30     | 2      | 7      | 29.4   | 13       |
| ST86-006B     | -0.1   | 91     | 50     | 6      | 1610   | 19.6   | 2      | 13     | 24     | -2     | -8     | 28.5   | 10       |
| ST86-009      | -0.1   | 71     | 65     | 6      | 2560   | 16.7   | 1      | 14     | 31     | -1     | -7     | 33.8   | 11       |
| ST86-015      | -0.1   | 2073   | 42     | 8      | 2690   | 25.1   | 1      | 17     | 28     | -1     | -6     | 32.4   | 12       |
| ST86-016      | 0.2    | 2762   | 73     | 32     | 11290  | 47.8   | 2      | 78     | 25     | 1      | -5     | 63.4   | 14       |
| ST86-021      | 0.1    | 294    | 59     | 17     | 1150   | 44.4   | 2      | 27     | 24     | -3     | -15    | 55.1   | 5        |
| ST86-024      | 0.2    | 1595   | 51     | 14     | 3780   | 17     | 2      | 26     | 24     | -2     | -8     | 29.3   | 9        |
| ST86-027      | 0.2    | 1558   | 65     | 6      | 5050   | 17.3   | 1      | 20     | 28     | -1     | -6     | 24.4   | 13       |
| ST86-030      | 0.5    | 536    | 42     | 11     | 3860   | 29.8   | 2      | 22     | 24     | -1     | -5     | 26     | 14       |
| ST86-033      | 0.2    | 474    | 73     | 10     | 5880   | 136.4  | 2      | 24     | 27     | -3     | -15    | 33.5   | 5        |
| ST86-037      | 0.1    | 428    | 54     | 12     | 2470   | 25     | 2      | 17     | 25     | -1     | 11     | 27.5   | 11       |
| ST86-039      | -0.1   | 206    | 64     | 14     | 3570   | 29.1   | 2      | 34     | 26     | -4     | -19    | 32.4   | 4        |
| ST86-042      | 0.6    | 13063  | 64     | 28     | 2030   | 46.5   | 3      | 44     | 25     | 6      | 21     | 69.2   | 8        |
| ST86-043      | 0.3    | 2421   | 52     | 11     | 2590   | 14.2   | 2      | 22     | 26     | 3      | -6     | 27     | 12       |
| ST86-048      | 0.1    | 1110   | 79     | 29     | 2190   | 24.6   | 2      | 38     | 18     | -2     | -8     | 80.1   | 9        |
| ST86-049      | 1.8    | 2381   | 55     | 18     | 2210   | 29.5   | 3      | 27     | 25     | -4     | -19    | 45.3   | 4        |
| ST86-057      | -0.1   | 2947   | 58     | 6      | 1390   | 8      | 2      | 9      | 42     | 2      | -6     | 25.9   | 13       |
| ST86-059      | 0.1    | 288    | 47     | 11     | 1930   | 23.9   | 2      | 17     | 37     | -1     | -5     | 25.4   | 14       |
| ST86-060      | -0.1   | 300    | 44     | 3      | 3800   | 12.4   | 2      | 13     | 25     | -2     | -11    | 21.9   | 7        |
| ST86-063      | -0.1   | 2436   | 34     | 4      | 831    | 17     | 2      | 16     | 28     | -2     | 11     | 24.9   | 7        |
| ST86-067      | 0.1    | 3      | 44     | 2      | 1880   | 5.6    | 1      | 11     | 26     | -1     | -5     | 19.9   | 14       |
| ST86-068      | 0.1    | 384    | 59     | 8      | 1330   | 13     | 2      | 15     | 33     | -2     | -8     | 26     | 10       |
| ST86-069      | 0.1    | 86     | 47     | 7      | 2120   | 20.8   | 2      | 20     | 22     | -1     | -5     | 27.2   | 15       |
| ST86-070      | 0.1    | 166    | 40     | 6      | 1340   | 9.8    | 1      | 15     | 14     | -1     | -6     | 17.7   | 13       |
| ST86-072B     | -0.1   | 2033   | 62     | 10     | 2120   | 6.7    | 2      | 16     | 30     | -2     | -9     | 22.6   | 8        |
| ST86-072C     | 0.2    | 351    | 62     | 6      | 1710   | 8.4    | 1      | 16     | 30     | -1     | -6     | 20.8   | 12       |
| ST86-074      | 0.1    | 249    | 54     | 5      | 1780   | 7.7    | 1      | 13     | 24     | -1     | -5     | 16.3   | 15       |
| ST86-076      | 0.6    | 2808   | 51     | 8      | 3030   | 19.7   | 1      | 18     | 27     | 2      | -8     | 26.4   | 9        |
| ST86-077A     | 0.1    | 91     | 54     | 9      | 2550   | 11.8   | 1      | 19     | 26     | -1     | -5     | 27.7   | 15       |
| ST86-077B     | 0.2    | 49     | 51     | 6      | 2240   | 11.1   | 1      | 15     | 25     | -1     | -5     | 20.5   | 15       |
| ST86-079      | -0.1   | 447    | 57     | 6      | 2310   | 9.6    | 1      | 17     | 25     | -1     | -6     | 22.7   | 13       |
| ST86-081      | -0.1   | 36     | 54     | 7      | 1750   | 7.9    | 1      | 15     | 24     | -1     | -6     | 22.1   | 12       |
| ST86-082      | -0.1   | 241    | 51     | 4      | 3220   | 13.2   | 1      | 17     | 29     | -1     | 7      | 27.5   | 15       |
| ST86-083      | 1      | 1919   | 57     | 10     | 1920   | 8.6    | 1      | 16     | 24     | -1     | -5     | 21.9   | 15       |
| ST86-084      | -0.1   | 4749   | 37     | 30     | 1230   | 16.5   | 3      | 23     | 21     | 3      | 11     | 22.8   | 12       |
| ST86-085      | -0.1   | 475    | 40     | 8      | 2100   | 11.8   | 2      | 14     | 27     | -1     | -7     | 22.4   | 11       |
| ST86-087      | 0.1    | 623    | 59     | 5      | 3220   | 12.8   | 3      | 13     | 24     | -1     | -6     | 21.8   | 12       |
| ST86-088      | -0.1   | 878    | 43     | 3      | 2660   | 15.5   | 2      | 14     | 22     | -1     | 9      | 17.7   | 15       |

| Sample Number | Ag ppm | Au ppm | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| ST86-089      | -0.1   | 691    | 56     | 16     | 2080   | 12.1   | 2      | 25     | 22     | 1      | 7      | 29.5   | 15       |
| ST86-090      | 0.6    | 200    | 47     | 199    | 6000   | 174.6  | 3      | 670    | 30     | 5      | 15     | 646.5  | 6        |
| ST86-100      | -0.1   | 43     | 65     | 6      | 1650   | 24.3   | 1      | 14     | 24     | 13     | 11     | 32.6   | 12       |
| ST86-101      | -0.1   | 348    | 44     | 7      | 1910   | 23.6   | 2      | 16     | 18     | 1      | 11     | 30.2   | 11       |
| ST86-102      | -0.1   | 1039   | 572    | 4      | 2090   | 27.2   | 1      | 14     | 26     | 3      | 9      | 33.6   | 12       |
| ST86-103      | -0.1   | 1381   | 52     | 3      | 2400   | 15.5   | 1      | 10     | 29     | 2      | 10     | 22.6   | 15       |
| ST86-104      | -0.1   | 1214   | 49     | 6      | 2030   | 17.9   | 2      | 13     | 32     | -1     | -5     | 29.7   | 13       |
| ST86-105      | 0.4    | 359    | 44     | 4      | 2210   | 9.8    | 1      | 10     | 31     | -1     | -5     | 27.7   | 13       |
| ST86-106      | 0.1    | 639    | 62     | 7      | 2100   | 20.4   | 2      | 14     | 32     | -2     | 19     | 33.7   | 7        |
| ST86-107B     | -0.1   | 51     | 44     | 8      | 1240   | 18.4   | 1      | 13     | 16     | -1     | -6     | 27.2   | 12       |
| ST86-108A     | 0.6    | 90     | 67     | 5      | 1150   | 16.5   | 1      | 11     | 23     | -1     | -6     | 29.4   | 12       |
| ST86-108B     | 0.3    | 1394   | 39     | 3      | 872    | 26.7   | 1      | 9      | 22     | -1     | -7     | 36.8   | 11       |
| ST86-109      | -0.1   | 134    | 47     | 9      | 2180   | 19.9   | 2      | 17     | 22     | -1     | -7     | 36.5   | 11       |
| ST86-110      | -0.1   | 950    | 105    | 7      | 2040   | 30     | 1      | 16     | 28     | -1     | -6     | 36.4   | 12       |
| ST86-111      | -0.1   | 1343   | 47     | 11     | 1780   | 27.3   | 1      | 14     | 28     | 2      | -5     | 32     | 15       |
| ST86-112      | 1.2    | 32     | 33     | 23     | 2730   | 37.9   | 1      | 24     | 32     | 2      | -8     | 40.5   | N/A      |
| ST86-113      | 1.5    | 1158   | 28     | 12     | 8700   | 20.1   | 1      | 40     | 26     | -3     | -13    | 47.2   | 6        |
| ST86-114      | 0.1    | 368    | 26     | 8      | 2830   | 22.8   | 1      | 17     | 26     | -2     | -9     | 35.7   | 8        |
| ST86-115      | 0.3    | 80     | 36     | 7      | 7500   | 50     | 2      | 13     | 59     | -10    | -50    | 80.8   | 1.5      |
| ST86-116      | 0.2    | 3      | 33     | 24     | 3460   | 38.5   | 2      | 38     | 33     | -6     | -30    | 51     | 2.5      |
| ST86-117      | -0.1   | 1658   | 49     | 12     | 3350   | 50.3   | 2      | 22     | 27     | 4      | -19    | 55.2   | 4        |
| ST86-118      | 0.4    | 550    | 33     | 9      | 1850   | 16.5   | 1      | 16     | 25     | -1     | -6     | 30.9   | 13       |
| ST86-119      | -0.1   | 85     | 52     | 4      | 1320   | 21.6   | 1      | 12     | 28     | -3     | -13    | 30.3   | 6        |
| ST86-120      | 0.1    | 248    | 27     | 5      | 1590   | 21     | 1      | 11     | 24     | 1      | -6     | 29.9   | 12       |
| ST86-121      | -0.1   | 575    | 39     | 13     | 2230   | 46     | 1      | 40     | 28     | 1      | -5     | 45     | 14       |
| ST86-122      | 0.2    | 498    | 52     | 9      | 2690   | 38.6   | 1      | 26     | 31     | 1      | -6     | 38.9   | 13       |
| ST86-123      | 0.1    | 600    | 42     | 14     | 2180   | 56     | 1      | 57     | 22     | 2      | 6      | 41     | 14       |
| ST86-124      | -0.1   | 682    | 20     | 9      | 2220   | 22.2   | 1      | 16     | 28     | 2      | 6      | 30.2   | 14       |
| ST86-125      | 3      | 156    | 15     | 14     | 2200   | 48.6   | 2      | 16     | 23     | 2      | 8      | 45.9   | 13       |
| BI87-1B       | -0.1   | 88     | 38     | 13     | 1830   | 19.4   | 3      | 22     | 26     | 2      | 8      | 28.3   | 13       |
| BI87-2B       | 0.2    | 0.5    | 65     | 8      | 1550   | 13.1   | 2      | 18     | 22     | 3      | 11     | 28     | 12       |
| BI87-4B       | 0.1    | 508    | 62     | 5      | 1720   | 14.2   | 2      | 18     | 26     | -1     | -6     | 22.5   | 12       |
| BI87-5B       | -0.1   | 20     | 42     | 7      | 2200   | 21.4   | 2      | 23     | 30     | -1     | -7     | 33     | 11       |
| BI87-6        | -0.1   | 593    | 69     | 7      | 1850   | 22.4   | 2      | 19     | 28     | -1     | -7     | 31.2   | 11       |
| BI87-7A       | 0.1    | 145    | 39     | 5      | 1690   | 10.8   | 2      | 25     | 26     | -1     | -7     | 20.5   | 11       |
| BI87-9        | -0.1   | +20000 | 39     | 9      | 2480   | 12     | 2      | 21     | 20     | 4      | 24     | 24.4   | 18       |
| BI87-10B      | 1.7    | 327    | 47     | 10     | 2690   | 14.2   | 2      | 33     | 28     | -1     | -7     | 28.9   | 11       |
| BI87-11B      | 0.1    | 2520   | 51     | 6      | 1760   | 19.3   | 2      | 22     | 23     | -1     | 8      | 32.6   | 11       |
| BI87-12A      | 0.1    | 273    | 79     | 5      | 1770   | 21.4   | 2      | 19     | 24     | -3     | -15    | 42.7   | 5        |
| BI87-12B      | 0.1    | 168    | 43     | 3      | 1440   | 9.8    | 2      | 13     | 29     | -1     | -6     | 22.1   | 12       |
| BI87-13       | -0.1   | 735    | 1730   | 20     | 2230   | 215.1  | 3      | 30     | 39     | -8     | -38    | 37.8   | 2        |
| SL87-011      | 20.2   | 2999   | 28     | 11     | 2140   | 13     | 3      | 28     | 34     | 2      | 9      | 40.1   | 13       |
| SL87-012      | 0.1    | 57     | 31     | 7      | 1900   | 8.2    | 2      | 18     | 33     | -1     | 8      | 19.1   | 11       |
| SL87-013      | -0.1   | 173    | 50     | 12     | 1780   | 12.3   | 2      | 13     | 27     | -1     | -6     | 23.8   | 12       |

| Sample Number | Ag ppm | Au ppm | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| SL87-016      | 0.1    | 199    | 41     | 8      | 2130   | 8.9    | 2      | 15     | 29     | -1     | -5     | 19.5   | 14       |
| SL87-018      | -0.1   | 10914  | 72     | 7      | 2030   | 10     | 3      | 14     | 29     | -1     | 7      | 23.7   | 13       |
| SL87-022      | 0.1    | 376    | 58     | 4      | 2130   | 7.4    | 3      | 11     | 43     | -1     | -5     | 21.8   | 15       |
| SL87-036      | -0.1   | 250    | 41     | 10     | 1740   | 12.9   | 3      | 13     | 32     | -1     | -6     | 23.8   | 12       |
| SL87-038      | -0.1   | 234    | 69     | 3      | 1470   | 6.9    | 3      | 11     | 30     | -1     | -5     | 17.5   | 15       |
| SL87-069      | -0.1   | 145    | 76     | 8      | 1790   | 8.2    | 3      | 17     | 30     | -1     | -6     | 23.9   | 12       |
| SL87-075      | -0.1   | 347    | 52     | 5      | 2100   | 6.9    | 3      | 13     | 33     | -1     | -6     | 20.8   | 13       |
| SL87-080      | 0.1    | 110    | 58     | 6      | 2170   | 6.6    | 2      | 13     | 31     | -1     | -6     | 19.9   | 13       |
| SL87-082      | -0.1   | 601    | 61     | 6      | 2600   | 6.5    | 2      | 11     | 40     | -1     | -7     | 21.1   | 11       |
| SL87-086      | -0.1   | 3220   | 29     | 6      | 1900   | 7.9    | 2      | 13     | 30     | 1      | -5     | 19.1   | 15       |
| SL87-090      | 0.2    | 470    | 50     | 6      | 1860   | 6.2    | 2      | 13     | 31     | -1     | -6     | 18.8   | 12       |
| SL87-096      | -0.1   | 978    | 32     | 5      | 2150   | 11.1   | 2      | 12     | 26     | 421    | -7     | 21.9   | 11       |
| SL87-098      | 0.3    | 6773   | 40     | 14     | 2970   | 18     | 2      | 19     | 33     | 3      | -6     | 24.8   | 13       |
| SL87-100      | 0.2    | 1144   | 83     | 14     | 2770   | 20.2   | 2      | 22     | 26     | 1      | -5     | 31.5   | 14       |
| SL87-102      | -0.1   | 4320   | 58     | 7      | 998    | 15.7   | 2      | 13     | 18     | 3      | -5     | 21.3   | 15       |
| SL87-105      | -0.1   | 173    | 60     | 7      | 1030   | 11.2   | 2      | 12     | 28     | -1     | 8      | 30.6   | 15       |
| SL87-107      | -0.1   | 122    | 32     | 6      | 774    | 11.4   | 2      | 12     | 18     | -1     | -5     | 21.3   | 15       |
| SL87-132      | -0.1   | 61     | 53     | 6      | 1320   | 9.9    | 2      | 13     | 25     | -1     | -5     | 21.6   | 15       |
| SL87-134      | -0.1   | 114    | 39     | 7      | 1000   | 15.6   | 2      | 13     | 20     | -1     | -5     | 24.9   | 15       |
| SL87-141      | -0.1   | 1194   | 53     | 6      | 1640   | 10.9   | 2      | 13     | 27     | -1     | -5     | 24.4   | 15       |
| SL87-157      | -0.1   | 241    | 46     | 48     | 1390   | 16.7   | 2      | 75     | 21     | -1     | -5     | 137.1  | 14       |
| SL87-161      | 0.1    | 478    | 42     | 10     | 2460   | 10.5   | 2      | 14     | 28     | -1     | -5     | 26.1   | 14       |
| SL87-164      | 0.1    | 629    | 35     | 8      | 990    | 17.2   | 2      | 15     | 20     | 1      | -5     | 30.3   | 15       |
| SL87-219A     | 0.2    | 176    | 37     | 5      | 2020   | 12.4   | 2      | 123    | 28     | 3      | -5     | 21.7   | 15       |
| SL87-229      | 0.1    | 122    | 22     | 5      | 2060   | 10.1   | 2      | 16     | 24     | -1     | -5     | 21.7   | 15       |
| SL87-272      | -0.1   | 2420   | 51     | 3      | 1290   | 11.6   | 3      | 14     | 25     | 2      | 5      | 22     | 15       |
| SL87-290      | 0.2    | 769    | 51     | 7      | 1030   | 32     | 2      | 17     | 17     | -1     | -5     | 28.2   | 15       |
| SL87-322      | -0.1   | 185    | 48     | 10     | 1430   | 13.3   | 2      | 18     | 30     | -1     | -6     | 29.9   | 12       |
| SL87-353      | 0.1    | 78     | 44     | 6      | 2280   | 8.5    | 2      | 14     | 30     | -1     | -6     | 25.4   | 13       |
| SL87-356      | -0.1   | 846    | 59     | 3      | 2280   | 13.1   | 2      | 13     | 33     | -1     | -5     | 47.3   | 14       |
| SL87-357      | -0.1   | 107    | 33     | 7      | 2320   | 13.6   | 2      | 14     | 30     | -1     | -6     | 26.3   | 13       |
| SL87-358      | -0.1   | 697    | 77     | 6      | 2760   | 18.9   | 2      | 14     | 31     | -1     | -5     | 31.1   | 13       |
| SL87-359      | 0.1    | 256    | 42     | 8      | 2340   | 15     | 2      | 15     | 32     | -1     | -5     | 27.2   | 15       |
| SL87-361      | 0.4    | 1844   | 42     | 7      | 1930   | 17     | 1      | 17     | 27     | -1     | -5     | 22.6   | 15       |
| SL87-363      | -0.1   | 382    | 35     | 8      | 2470   | 18.7   | 2      | 15     | 30     | -1     | -5     | 24.7   | 14       |
| SL87-364      | 0.5    | 13333  | 38     | 6      | 2130   | 55.1   | 2      | 14     | 32     | 3      | 9      | 26     | 12       |
| SL87-394      | 0.3    | 267    | 65     | 0.5    | 2630   | 9      | 2      | 11     | 34     | -1     | -5     | 20.2   | 15       |
| SL87-411      | -0.1   | 32     | 58     | 2      | 825    | 12.7   | 2      | 12     | 19     | -1     | -5     | 23.9   | 15       |
| SL87-412      | -0.1   | 28     | 58     | 2      | 740    | 17.6   | 2      | 11     | 17     | -1     | -5     | 22.5   | 15       |
| SL87-415      | 0.2    | 0.5    | 38     | 6      | 521    | 21.1   | 2      | 13     | 13     | -1     | -6     | 33.1   | 13       |
| SL87-439      | -0.1   | 76     | 36     | 0.5    | 2060   | 9      | 2      | 14     | 26     | -1     | 6      | 22     | 15       |
| SL87-440      | -0.1   | 3      | 44     | 4      | 2580   | 7.7    | 3      | 12     | 30     | 1      | 6      | 24     | 13       |
| SL87-521      | 0.1    | 75     | 44     | 12     | 1580   | 31.6   | 2      | 20     | 30     | 1      | -5     | 39.6   | 15       |
| SL87-527      | 0.1    | 106    | 60     | 7      | 1560   | 9.1    | 2      | 13     | 25     | 2      | 7      | 27.8   | 13       |

| Sample Number | Ag ppm | Au ppm | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| SL87-546      | 0.1    | 266    | 76     | 5      | 1620   | 17.4   | 2      | 16     | 28     | 3      | 8      | 32.3   | 12       |
| SL87-547      | 0.1    | 49     | 28     | 2      | 1480   | 10.8   | 2      | 12     | 28     | 1      | 5      | 24.7   | 15       |
| SL87-548      | -0.1   | 496    | 36     | 10     | 2140   | 19.5   | 2      | 15     | 35     | 1      | 8      | 34.3   | 11       |
| SL87-551      | -0.1   | 162    | 42     | 10     | 2250   | 16.9   | 2      | 15     | 22     | 2      | 9      | 27.8   | 13       |
| SL87-560      | 0.1    | 336    | 42     | 1      | 1740   | 9.5    | 2      | 10     | 31     | 1      | 8      | 19.7   | 13       |
| AVERAGE       |        | 1055   | 65     | 10     | 2271   | 22     | 2      | 24     | 27     |        | 35     | 12     |          |
| MAXIMUM       |        | +20000 | 1730   | 199    | 11290  | 215.1  | 3      | 670    | 59     |        | 647    | 18     |          |
| MINIMUM       |        | 0.5    | 15     | 1      | 521    | 5.6    | 1      | 9      | 13     |        | 16     | 1.5    |          |
| STD.DEV.      |        | 2075   | 151    | 18     | 1352   | 26     | 1      | 57     | 6      |        | 55     | 3.3    |          |

**Aultman Samples, Churchill Township**

| Sample Number             | Ag ppm | Au ppm | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| JTA-3B                    | -0.1   | 2748   | 47     | 10     | 2640   | 26.3   | 2      | 23     | 19     | -1     | -6     | 37.5   | 12       |
| JTA-7                     | -0.1   | 227    | 84     | 11     | 2740   | 24.9   | 2      | 22     | 21     | -2     | -9     | 37.2   | 8        |
| JTA-8A                    | -0.1   | 152    | 28     | 10     | 2660   | 16.4   | 3      | 21     | 15     | -2     | -9     | 32.1   | 8        |
| JTA-9                     | -0.1   | 2.5    | 48     | 7      | 3320   | 12.8   | 2      | 20     | 20     | -5     | 35     | 36.3   | 3        |
| JTA-11                    | -0.1   | 1043   | 40     | 11     | 2660   | 19.4   | 3      | 27     | 20     | -1     | 11     | 37     | 11       |
| JTA-12                    | -0.1   | 176    | 40     | 10     | 2320   | 21.8   | 2      | 24     | 22     | -2     | 17     | 31.9   | 7        |
| JTA-14                    | 0.6    | 2112   | 56     | 15     | 2230   | 25.4   | 3      | 29     | 20     | -3     | 30     | 29.3   | 5        |
| JTA-17                    | -0.1   | 203    | 56     | 10     | 2840   | 20     | 2      | 20     | 22     | -3     | 15     | 31.3   | 6        |
| AVERAGE                   |        | 833    | 50     | 11     | 2676   | 20.9   | 2      | 23     | 20     |        |        | 34.1   | 8        |
| MAXIMUM                   |        | 2748   | 84     | 15     | 3320   | 26.3   | 3      | 29     | 22     |        |        | 37.5   | 12       |
| MINIMUM                   |        | 2.5    | 28     | 7      | 2230   | 12.8   | 2      | 20     | 15     |        |        | 29.3   | 3        |
| No. Below detection limit |        | 1      |        |        |        |        |        |        |        |        |        |        |          |

**Control results: fire assay analyses of non-magnetic fraction of HMC (Klip Control)**

| Sample Number | Ag ppm | Au ppm | Ba ppm | Co ppm | Cr ppm | Cu ppm | Mo ppm | Ni ppm | Pb ppm | Pd ppb | Pt ppb | Zn ppm | Weight g |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|
| SL87-165H     | 0.7    | 5      | 70     | 5      | 225    | 16.8   | 3      | 9      | 10     | -5     | -25    | 46.2   | 3        |
| SL87-417H     | -0.1   | -2     | 43     | 5      | 231    | 7.4    | 3      | 7      | 10     | -2     | -8     | 33.7   | 10       |
| BI187-3BH     | -0.1   | -2     | 65     | 6      | 208    | 12.6   | 3      | 9      | 10     | -2     | -8     | 42.7   | 10       |
| JTA-4H        | -0.1   | -1     | 55     | 5      | 227    | 11.2   | 2      | 10     | 10     | -1     | -5     | 35.7   | 14       |

**APPENDIX H: Trace element analysis (trace 2) of non-magnetic and magnetic fractions of HMCs, Gowganda Map Area**

| Sample                  | Ba ppm | Be ppm | Co ppm | Cr ppm | Cu ppm | Fe pct | Mo ppm | Ni ppm | Pb ppm | Sc ppm | Sr ppm | V ppm | Y ppm | Zn ppm |
|-------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|
| <b>Non-Magnetic HMC</b> |        |        |        |        |        |        |        |        |        |        |        |       |       |        |
| GW89-008                | 90     | -1     | 25     | 1430   | 22     | 16.9   | -10    | 82     | 32     | 74     | 510    | 295   | 125   | 86     |
| GW89-030                | 640    | -1     | 52     | 810    | 20     | 14.7   | -10    | 116    | 14     | 50     | 260    | 340   | 69    | 82     |
| GW89-117                | 1240   | -1     | 32     | 820    | 28     | 13.8   | -10    | 94     | 38     | 62     | 738    | 362   | 83    | 82     |
| GW89-159                | 2240   | -1     | 34     | 804    | 51     | 27     | -10    | 45     | 52     | 62     | 355    | 384   | 106   | 71     |
| GW89-228                | 620    | -1     | 22     | 900    | 20     | 18.5   | -10    | 46     | 46     | 77     | 449    | 298   | 130   | 82     |
| GW89-229                | 720    | -1     | 24     | 1510   | 21     | 19.6   | -10    | 39     | 46     | 83     | 434    | 297   | 148   | 95     |
| SL89-246                | 1020   | -1     | 37     | 796    | 30     | 20.8   | -10    | 146    | 44     | 77     | 439    | 254   | 145   | 91     |
| <b>Magnetic HMC</b>     |        |        |        |        |        |        |        |        |        |        |        |       |       |        |
| GW89-008                | 520    | -1     | 50     | 7960   | 27     | 52.1   | -10    | 244    | -10    | 7      | 44     | 1594  | 12    | 264    |
| GW89-030                | 460    | -1     | 36     | 1730   | 33     | 46.7   | -10    | 121    | -10    | 15     | 57     | 2766  | 15    | 274    |
| GW89-117                | 590    | -1     | 30     | 1800   | 47     | 45.8   | -10    | 88     | 42     | 16     | 47     | 2237  | 21    | 265    |
| GW89-159                | 590    | -1     | 37     | 1610   | 44     | 51     | -10    | 75     | 30     | 15     | 36     | 2571  | 19    | 270    |
| GW89-228                | 190    | -1     | 71     | 9000   | 26     | 57     | -10    | 270    | -10    | 7      | 31     | 1866  | 12    | 286    |
| GW89-229                | 280    | -1     | 68     | 11000  | 32     | 53.2   | -10    | 223    | -10    | 6      | 23     | 1606  | 10    | 278    |
| SL89-246                | 340    | -1     | 54     | 5900   | 19     | 58.9   | -10    | 124    | -10    | 5      | 25     | 1620  | 11    | 318    |

**Control Results from Gowganda Area Non-Magnetic and Magnetic HMC Analysis: KLIP Control**

| Sample                  | Ba ppm | Be ppm | Co ppm | Cr ppm | Cu ppm | Fe pct | Mo ppm | Ni ppm | Pb ppm | Sc ppm | Sr ppm | V ppm | Y ppm | Zn ppm |
|-------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|--------|
| <b>Non-Magnetic HMC</b> |        |        |        |        |        |        |        |        |        |        |        |       |       |        |
| GW89-003H               | 100    | -1     | 17     | 360    | 8      | 20.6   | -10    | 23     | -10    | 59     | 78     | 342   | 193   | 148    |
| GW89-303H               | 880    | -1     | 16     | 342    | 9      | 21     | -10    | 20     | -10    | 59     | 81     | 351   | 196   | 147    |
| <b>Magnetic HMC</b>     |        |        |        |        |        |        |        |        |        |        |        |       |       |        |
| GW89-003M               | 590    | -1     | 70     | 1980   | 22     | 63.5   | -10    | 161    | -10    | -2     | 16     | 1137  | 9     | 140    |
| GW89-303M               | 340    | -1     | 76     | 2320   | 26     | 63.3   | -10    | 138    | -10    | -2     | 17     | 1142  | 11    | 134    |

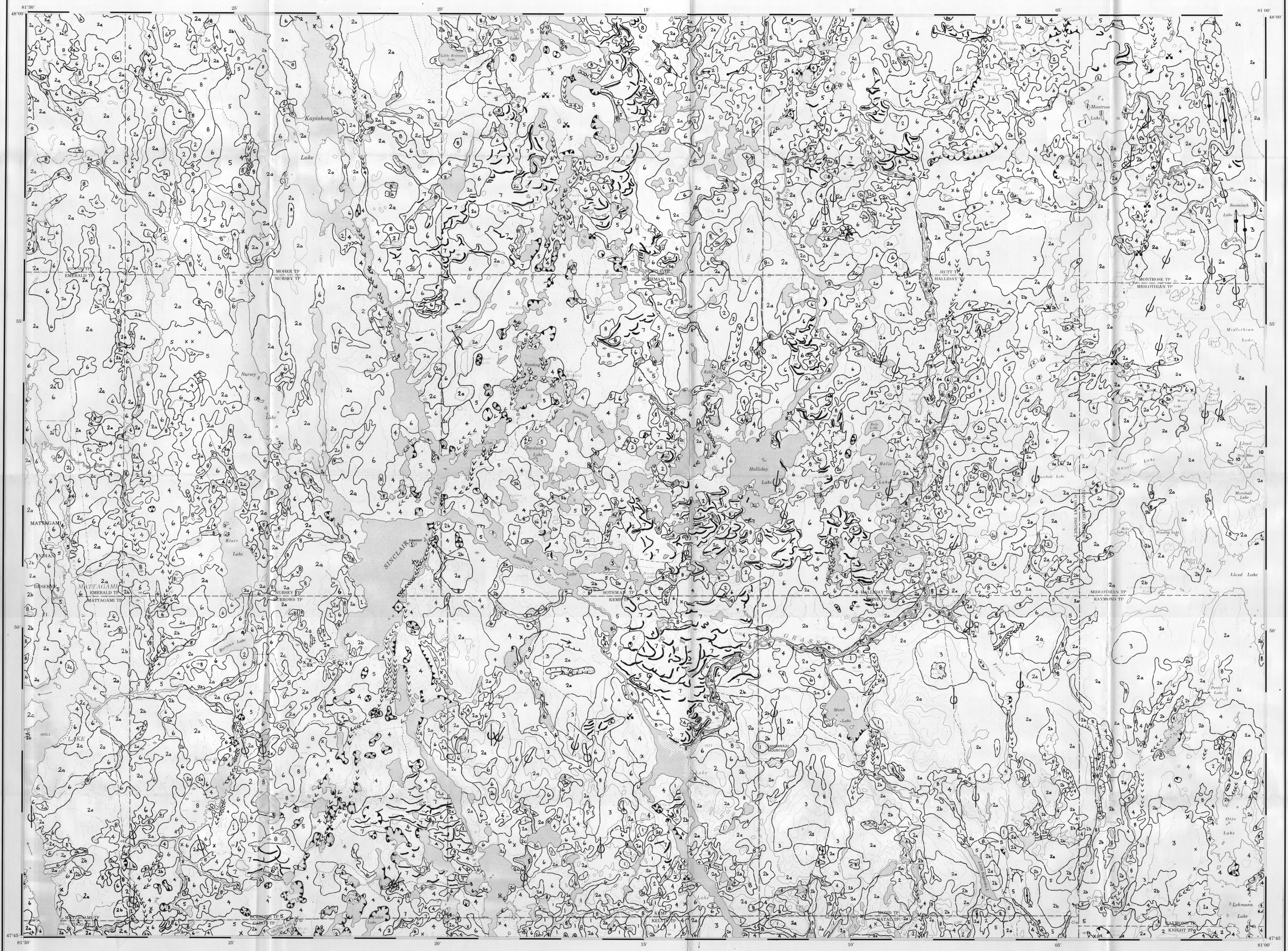
**CONVERSION FACTORS FOR MEASUREMENTS IN ONTARIO GEOLOGICAL SURVEY PUBLICATIONS**

| Conversion from SI to Imperial |                      |                              | Conversion from Imperial to SI |                        |                 |
|--------------------------------|----------------------|------------------------------|--------------------------------|------------------------|-----------------|
| <i>SI Unit</i>                 | <i>Multiplied by</i> | <i>Gives</i>                 | <i>Imperial Unit</i>           | <i>Multiplied by</i>   | <i>Gives</i>    |
| <b>LENGTH</b>                  |                      |                              |                                |                        |                 |
| 1 mm                           | 0.039 37             | inches                       | 1 inch                         | <b>25.4</b>            | mm              |
| 1 cm                           | 0.393 70             | inches                       | 1 inch                         | <b>2.54</b>            | cm              |
| 1 m                            | 3.280 84             | feet                         | 1 foot                         | <b>0.304 8</b>         | m               |
| 1 m                            | 0.049 709 7          | chains                       | 1 chain                        | 20.116 8               | m               |
| 1 km                           | 0.621 371            | miles (statute)              | 1 mile (statute)               | <b>1.609 344</b>       | km              |
| <b>AREA</b>                    |                      |                              |                                |                        |                 |
| 1 cm <sup>2</sup>              | 0.155 0              | square inches                | 1 square inch                  | <b>6.451 6</b>         | cm <sup>2</sup> |
| 1 m <sup>2</sup>               | 10.763 9             | square feet                  | 1 square foot                  | <b>0.092 903 04</b>    | m <sup>2</sup>  |
| 1 km <sup>2</sup>              | 0.386 10             | square miles                 | 1 square mile                  | 2.589 988              | km <sup>2</sup> |
| 1 ha                           | 2.471 054            | acres                        | 1 acre                         | 0.404 685 6            | ha              |
| <b>VOLUME</b>                  |                      |                              |                                |                        |                 |
| 1 cm <sup>3</sup>              | 0.061 02             | cubic inches                 | 1 cubic inch                   | <b>16.387 064</b>      | cm <sup>3</sup> |
| 1 m <sup>3</sup>               | 35.314 7             | cubic feet                   | 1 cubic foot                   | 0.028 316 85           | m <sup>3</sup>  |
| 1 m <sup>3</sup>               | 1.308 0              | cubic yards                  | 1 cubic yard                   | 0.764 555              | m <sup>3</sup>  |
| <b>CAPACITY</b>                |                      |                              |                                |                        |                 |
| 1 L                            | 1.759 755            | pints                        | 1 pint                         | 0.568 261              | L               |
| 1 L                            | 0.879 877            | quarts                       | 1 quart                        | 1.136 522              | L               |
| 1 L                            | 0.219 969            | gallons                      | 1 gallon                       | <b>4.546 090</b>       | L               |
| <b>MASS</b>                    |                      |                              |                                |                        |                 |
| 1 g                            | 0.035 273 96         | ounces (avdp)                | 1 ounce (avdp)                 | 28.349 523             | g               |
| 1 g                            | 0.032 150 75         | ounces (troy)                | 1 ounce (troy)                 | <b>31.103 476 8</b>    | g               |
| 1 kg                           | 2.204 62             | pounds (avdp)                | 1 pound (avdp)                 | <b>0.453 592 37</b>    | kg              |
| 1 kg                           | 0.001 102 3          | tons (short)                 | 1 ton (short)                  | <b>907.184 74</b>      | kg              |
| 1 t                            | 1.102 311            | tons (short)                 | 1 ton (short)                  | <b>0.907 184 74</b>    | t               |
| 1 kg                           | 0.000 984 21         | tons (long)                  | 1 ton (long)                   | <b>1016.046 908 8</b>  | kg              |
| 1 t                            | 0.984 206 5          | tons (long)                  | 1 ton (long)                   | <b>1.016 046 908 8</b> | t               |
| <b>CONCENTRATION</b>           |                      |                              |                                |                        |                 |
| 1 g/t                          | 0.029 166 6          | ounce (troy)/<br>ton (short) | 1 ounce (troy)/<br>ton (short) | 34.285 714 2           | g/t             |
| 1 g/t                          | 0.583 333 33         | pennyweights/<br>ton (short) | 1 pennyweight/<br>ton (short)  | 1.714 285 7            | g/t             |

**OTHER USEFUL CONVERSION FACTORS**

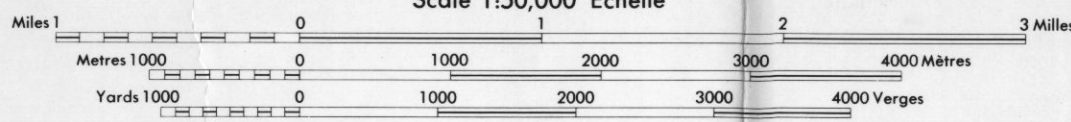
|                                | <i>Multiplied by</i> |                               |
|--------------------------------|----------------------|-------------------------------|
| 1 ounce (troy) per ton (short) | 20.0                 | pennyweights per ton (short)  |
| 1 pennyweight per ton (short)  | 0.05                 | ounces (troy) per ton (short) |

*Note: Conversion factors which are in bold type are exact. The conversion factors have been taken from or have been derived from factors given in the Metric Practice Guide for the Canadian Mining and Metallurgical Industries, published by the Mining Association of Canada in co-operation with the Coal Association of Canada.*



**SINCLAIR LAKE  
ONTARIO**

Scale 1:50,000 Échelle



CONTOUR INTERVAL 50 FEET  
Échelle en pieds au-dessus du niveau moyen de la mer  
Niveau moyen au-dessus de 1927  
Topographie Métrique Projection

ÉLÉVATIONS EN PIEDS AU-DESSUS DU NIVEAU MOYEN DE LA MER  
Élevations en mètres au-dessus du niveau moyen de la mer  
Système de référence géodésique nord-américain, 1927  
Projections Transverse de Mercator

Produced by the SURVEYS AND MAPPING BRANCH,  
DEPARTMENT OF ENERGY, MINES AND TECHNICAL SERVICES,  
Ottawa, Ontario, Canada.  
Copies may be obtained from the Canada Map Office,  
Department of Energy, Mines and Resources, Ottawa,  
at your nearest map dealer.  
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Roads:  
Route or stabilized surface, all weather - gravel aggloméré, toute saison  
Route surface, dry weather and  
unclassified street - dirt/gravel, temps sec et  
carriway - sentiers, pavés ou portage  
Trail, cut line or portage - sentiers, pavés ou portage  
FOR COMPLETE REFERENCE SEE REVERSE SIDE POUR UNE LISTE COMPLÈTE DES SIGNES, VOIR AU VERSO

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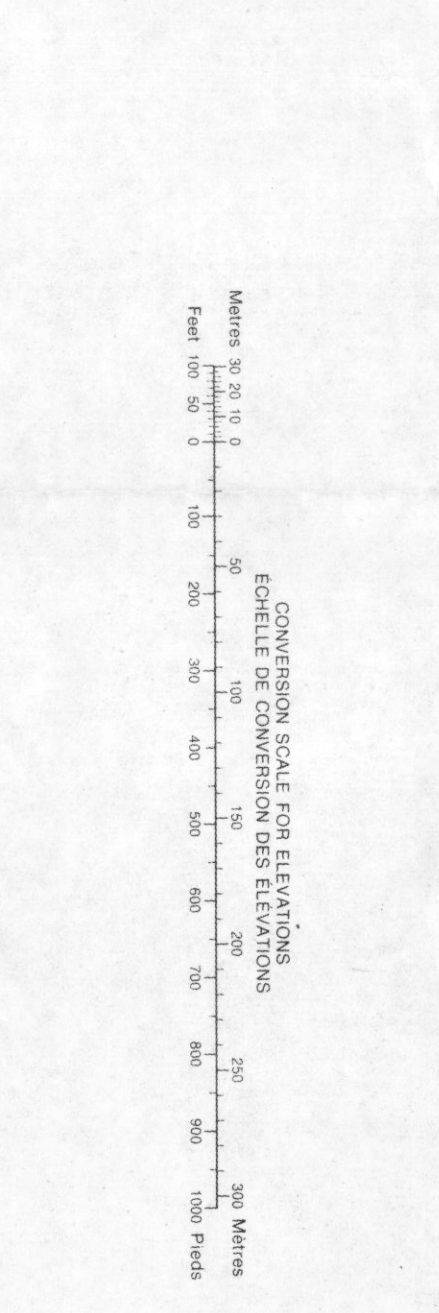
TABLAU D'ASSIPLAGE DU SYSTÈME NATIONAL DE RÉFÉRENCE CARTOGRAPHIQUE

|       |       |       |       |
|-------|-------|-------|-------|
| 47 00 | 47 05 | 47 10 | 47 15 |
| 47 00 | 47 05 | 47 10 | 47 15 |
| 47 00 | 47 05 | 47 10 | 47 15 |
| 47 00 | 47 05 | 47 10 | 47 15 |

INDEX TO ADJOINING MAPS OF THE NATIONAL TOPOGRAPHIC SYSTEM



Military users refer to this map as: Série A 751 Série 41 P/10 CARTE  
 Références de cette carte: ÉDITION 2 MCE ÉDITION  
 pour usage militaire.



Use diagram only to obtain numerical values for contour intervals and elevations. For center of map, contour interval is 10 feet. For center of map, contour interval is 10 feet. For center of map, contour interval is 10 feet.

ONE THOUSAND METRE UNIVERSAL TRANSVERSE MERCATOR GRID  
 ZONE 17  
 QUADRILLAGE DE MILLE MÈTRES TRANSVERSE UNIVERSELLE DE MERCATOR

TO USE AS REFERENCE TO METERS OR FEET  
 EXEMPLE DE LA MÈTRE EMPLOYÉE POUR LES MÈTRES À 100 MÈTRES PRÈS

REFERENCE POINT: CHURCH - ÉGLISE (see diagram)

NOTES: Read number on grid line immediately to left of point. L'INDICATEUR: Lire le chiffre de la ligne de quadrillage immédiatement à gauche du point.

Estimate tenths of a square from contour interval and distance of point from contour interval. Estimer le nombre de dixièmes de carré entre une ligne de contour et le point.

REFERENCE TO QUADRILLAGE: 17984

TABLEAU D'ASSEMBLAGE DU SYSTÈME NATIONAL DE RÉFÉRENCE CARTOGRAPHIQUE

|         |         |        |
|---------|---------|--------|
| 41 P/4  | 41 P/5  | 41 P/6 |
| 41 P/11 | 41 P/10 | 41 P/9 |
| 41 P/8  | 41 P/7  | 41 P/8 |

INDEX TO KNOWING MAPS OF THE NATIONAL TOPOGRAPHIC SYSTEM

GOWANDA  
 41 P/10  
 ÉDITION 2

Prepared by the SURVEYS AND MAPPING BRANCH, DEPARTMENT OF ENERGY, MINES AND RESOURCES, Ottawa, from aerial photographs taken in 1974. Contour interval 10 feet. Information current as of 1975.

Élaboré par le Service des levés et de la cartographie, Ministère de l'Énergie, des Mines et des Ressources, Ottawa, à partir de photos aériennes prises en 1974. Intervalle des courbes de niveau de 10 mètres. Informations actualisées au 1975.

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**GOWANDA**  
 ONTARIO  
 TIMISKAMING DISTRICT  
 Scale 1:50,000 Echelle

Miles 0 1 2 3  
 Mètres 0 1000 2000 3000 4000

CONTOUR INTERVAL: 50 FEET  
 Intervalle des courbes de niveau: 15 mètres

ÉQUIVALENCES DES COURBES DE NIVEAU  
 Échelle des courbes de niveau: 15 mètres

Élaboré par la Direction des levés et de la cartographie, Ministère de l'Énergie, des Mines et des Ressources, Ottawa, à partir de photos aériennes prises en 1974. Intervalle des courbes de niveau de 10 mètres. Informations actualisées au 1975.

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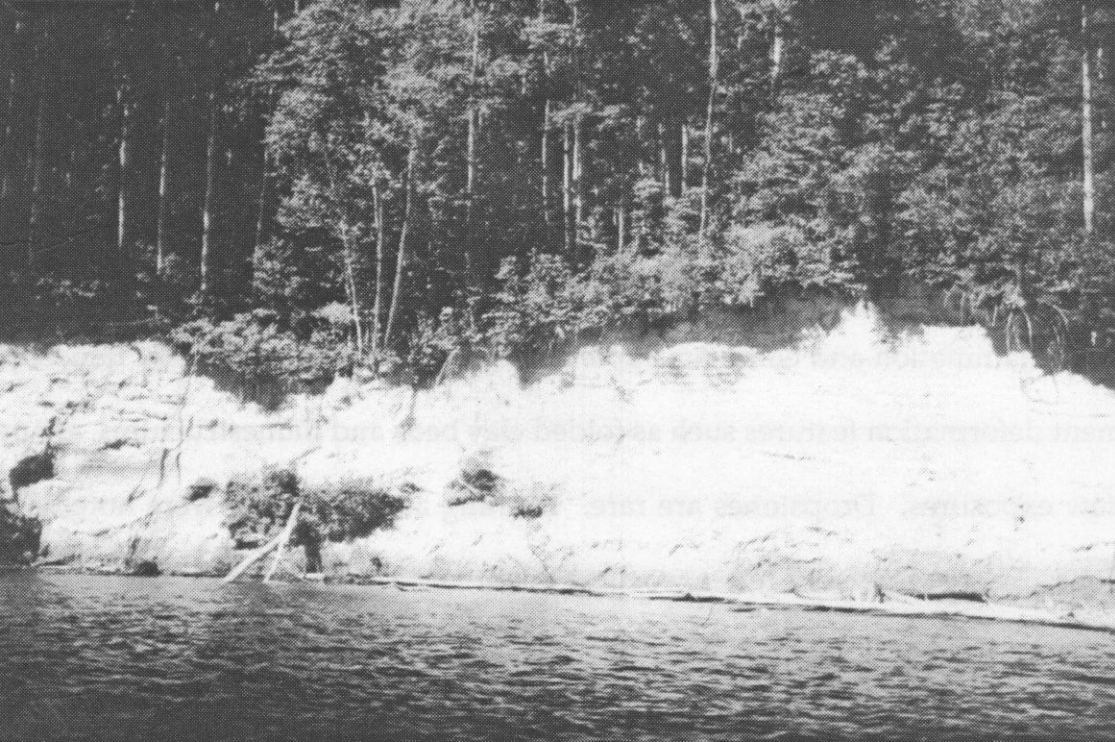






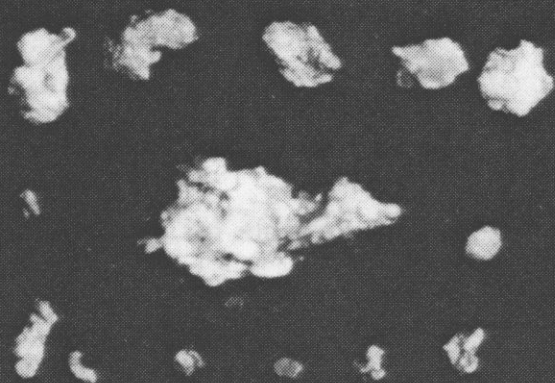












## MARGINAL NOTES

### INTRODUCTION

The Quaternary geology of the Shining Tree area (NTS 41P/11) was mapped during the 1988 field season on this area (continuing with other work in 1987 and 1988 (Alcock 1987, 1988). The Sinclair Lake map area (NTS 41P/14), immediately to the north, has also been mapped (Alcock and Miller 1986).

The surficial sediments were examined at natural and man-made exposures along road and water traverses, and through hand augering, test pitting and backhoe trenching. Access to much of the area is poor. The road system is limited to a few main gravel-surfaced roads and a network of minor bush roads maintained for forestry and recreational purposes. Rivers and lakes allowed access to many remote areas.

Surficial units were delineated through airphoto interpretation using 1:15 840 and 1:50 000 scale airphotos. Deposit morphology, vegetation cover, drainage characteristics and reflections of exposed sediments were used to interpret the surficial deposits in remote areas. The distribution of deposits is strongly topographically controlled. Till predominates in the upland areas. Glaciofluvial ice-contact and outwash deposits are present in north-south oriented valleys and glaciofluvial and organic deposits occupy topographic lows with restricted drainage.

Any map unit represents a composite area, with the indicated deposit type predominating and minor areas of other deposit types. For example, within the bedrock-drift complex, most areas of till veneer (< 1 m thickness) over bedrock also include small areas of thick till (> 1 m thickness) and organic deposits. Many contacts between map units represent an arbitrary division of the gradual transition from one deposit type to another, for example, the transition from glaciofluvial outwash to wave-reworked outwash to lacustrine sands. The bedrock-drift complex areas have covers of drift over bedrock which average 1 m or less in thickness. All other units represent drift or organic material at least 1 m thick. Any site specific use of the surficial deposits map should include an orientation survey to locally verify the sediment types, thickness and distribution.

The present study provides additional detail and local control to the regional mapping of Boissoneau (1965, 1968) and the terrain study of Rod and Hall (1979) and occupies areas irregularly mapped by Closs and Sado (1982). Reference was made to 1:25 000 scale bedrock maps (Carter 1981, Bright 1970, 1984) for verifying areas of bedrock-drift complex.

The authors wish to acknowledge the administrative and logistical assistance of the staff at the Gogama District Office, Ontario Ministry of Natural Resources. Complete assistance during mapping was provided by J. MacKenzie, A. Chippindale, C. Hibberd, J. Aulman and V. Ramani and M. Schroder.

### BEDROCK GEOLOGY

In the Shining Tree map area, Early Precambrian (Archean) rocks consist of a metasedimentary sequence which are intruded by mafic and felsic plutonic rocks and diabase dikes. Middle Precambrian (Proterozoic) rocks include generally flat-lying clastic and chemical sedimentary rocks of the Quirao Lake and Co-Cast groups. These unconformably overlie the Early Precambrian bedrock, and Nipissing-type intrusive diabase sills and dikes. Late Precambrian diabase dikes cut all formations (Carter 1981).

Deposits and occurrences of gold, silver, cobalt, copper, zinc, lead, molybdenum, nickel, iron, and talc occur in the study area (Carter 1981, Bright 1970, 1984). Over the area, approximately 10 to 30 percent of the bedrock is exposed.

### PLEISTOCENE HISTORY

The last late Wisconsinan ice advance, and postglacial glaciofluvial and eolian activity, are represented by the surficial sedimentary sequence. Glacially streamlined and striated bedrock outcrops, till fabrics and dispersion trends of lithologic indicators demonstrate that the last dominant ice movement was towards 180°-30° azimuth. Minor late-glacial shifts in ice direction, due to bedrock topographic influences, are indicated by 160° to 180° striations cutting an earlier set of 140° to 160° striations. Where exposed, the bedrock surface is often glacially smoothed, striated and displays whaleback forms.

Certain rocks, *microvarietas* preserve facets or remnants of grooves oriented southwest-southwest on their (southeast) side. On rare outcrops, such as near the south end of Bobbit Lake in Fawcett Township, southwesterly oriented striations are crossed by easterly oriented ones. This evidence suggests an earlier southwesterly ice advance, perhaps equivalent to that documented by Veilleux (1986) in the Timmins, Matheson and Lake Timiskaming areas to the north and east of the project area.

Ice retreated from the area about 10 000 years BP (Dyke and Prest, 1987), leaving a widespread drift veneer over the bedrock surface. Very few structural features, such as drumlins or minor moraine ridges, are present. Several north-south-trending belts and ice re-entrant infills of glaciofluvial ice-contact and outwash sediments were inundated by short-lived proglacial lakes. Washing and winnowing of the drift-mantled hills and glaciofluvial deposits produced bare bedrock knobs, wave-cut benches in eskers and blankets of nearshore sand stretching out from sediment sources. Accumulations of boulders on till are found over the range of glaciofluvial wave benches.

Meltwater drainage was controlled by the location and elevation of the major bedrock valleys such as those occupied by the West Mountain and Grassy rivers and by Nabakwasi, Mattagami, Biglow and Pigeon lakes. Drainage of the proglacial lakes and subsequent subaerial exposure of waterlain sediments allowed extensive eolian reworking of the coarse-grained deposits, deposition of dunes and a widespread veneer of eolian sediment.

Drift thickness in areas of bedrock-drift complex commonly ranges from less than 1 m to in excess of 10 m. Extreme thicknesses of more than 50 m are present in areas of ice-contact deposits and in the major infilled valleys.

Only rare clasts of carbonate lithologies have been found in till or outwash deposits, indicating that the project area is south and east of the limit of carbonate drift as mapped by Kettle and Geddes (1987).

### SURFICIAL GEOLOGY

#### TILL

Till is frequently found as a veneer over bedrock (Unit 2a) but ranges up to 4 m or more in thickness in areas of thick till (Unit 3). Till veneer areas (average thickness < 1 m) have frequent bedrock outcrops and a surface morphology controlled by the underlying bedrock topography. Veneers of till are found over many bedrock hummocks and uplands. Deposits of thick till are found on the larger upland surfaces and in the lee of bedrock highs.

The till sheet found at surface represents one lithostratigraphic unit with varying composition. The variation is due to the incorporation of various bedrock lithologies and different modes of deposition. All surface till, to a depth of at least 20 cm, has been affected by soil forming processes, including oxidation and translocation of matrix carbonate and iron.

Both surficial and supraglacial tills were identified using sedimentological and structural characteristics. Subglacially deposited tills are common at or near surface in areas of bedrock-drift complex and thick till. Loam-textured till is commonly moderately to highly compact, stony (10 to 50 percent clasts by volume) and has a silty sand matrix. This till type occasionally displays shear structures and may overlie striated bedrock. Subglacial tills are generally loose to moderately compact, stony (10 to 50 percent clasts by volume), with a silty sand matrix and has thin deformed sand bands. The glaciofluvial till facies contain frequent boulders and clasts ranging in size from granules to boulders. The composition of these tills often strongly reflects the local bedrock lithologies.

Supraglacial tills likely represent englacial or subglacial derived debris sheared or eroded onto the surface and then deposited. The supraglacial tills are often found as thin units overlying subglacially deposited facies. Supraglacially derived flow till is often found on or between bedrock knobs, or differentiated within kames or eskers. This till type is moderately to loosely compacted with a stony sand matrix. In the flow units, sorted sand stringers and lenses of gravel or boulders are common. Supraglacial melt-out (tabular) till is commonly thin, loosely compacted with a stony sand matrix and frequent boulders of resistant provenance. The composition of the supraglacial tills often poorly reflects the local bedrock lithologies.

Kames are commonly found in valleys among drift-veneered bedrock knobs. Many are too small to be differentiated and mapped at 1:50 000 scale.

Glaciofluvial outwash deposits (Unit 4), consisting of horizontal beds of cobbly to gravely sand, often flank the esker systems. Occasionally, fans of outwash sediments are found at the downstream ends of eskers. Extensive areas of kettled, and occasionally terraced outwash, occupy large tracts in the southwestern portion of the map area. The frequency of kettles in the outwash deposits indicates that large numbers of ice blocks were left stranded in the proglacial zone. Minor glaciofluvial deposits occur in smaller valleys as terraces.

Glaciofluvial ice-contact and outwash sediment veneers on bedrock (Unit 2b) are associated with esker and outwash systems, generally along the saddles between topographic lows.

Glaciofluvial deposits (Unit 5) consist of rhythmically stratified, low, large, discontinuous and occasionally compound esker complexes occur.

Areas of hummocky and highly kettled ice-contact deposits, up to a few kilometers across, occur in Miramich, Cabot and Fawcett townships. These deposits probably represent sediment deposition over and between ice blocks in ice sheet re-entrants by meltwater streams and sediment gravity flows.

Many lowland areas known as Miercra, Ketchiwabozee, Fawcett and South Sandrum lakes, are partially surrounded by ice-contact deposits and have sections of lakeshore which are often ice-contact slopes. These lakes are relatively flat, kettle lakes, suggesting that very large ice blocks up to several hundred metres in diameter were left stranded upon deglaciation.



concentrate fraction, prepared from the < 2 mm till matrix, can be utilized for geochemical exploration. As the surface till is weathered to a depth of 1 to 3 m, the silt and clay fraction should be utilized for the more labile mineral species, such as base metal sulphides. The heavy mineral fraction can be utilized for unwashed till or for those minerals which do not weather in the surface environment (e.g., native gold). Surface geochemical sampling would not be effective in those areas where non-local glaciofluvial, glacioestuarine or eolian sediment forms the surficial material.

Aulman (1988) completed a study on the nature of gold dispersion in till in the Shining Tree area. Results from surface till samples collected up to several hundred metres down-hill of known gold occurrences indicate gold grains are present in the sand-sized heavy mineral fraction. Further work has also indicated anomalous gold geochemical values in the silt and clay fraction of these samples.

A case study of gold dispersion in till was conducted by Stewart and van Hees (1982) in the Metchewen area, northeast of the Shining Tree area. The results indicated that distinct dispersal trains from adrooping mineralized bedrock were present in the surface till in a number of size fractions.

The Geological Survey of Canada has recently published results from a regional lake sediment geochemical sampling program which included the Shining Tree area (Hornbrock and Fritsko 1988).

Bright, E. G. 1970. Geology of Haldimand and Midlothian townships; Ontario Department of Mines, Report 79, 33p.

—1984. Geology of the Fenier Lake-Canoeshed Lake area, District of Sudbury, Ontario Geological Survey, Open File Report 5346, 67p.

Closs, L. G. and Sado, E.V. 1982. Bedrock and overburden geochemistry investigations in the Midlothian Lake and Natal

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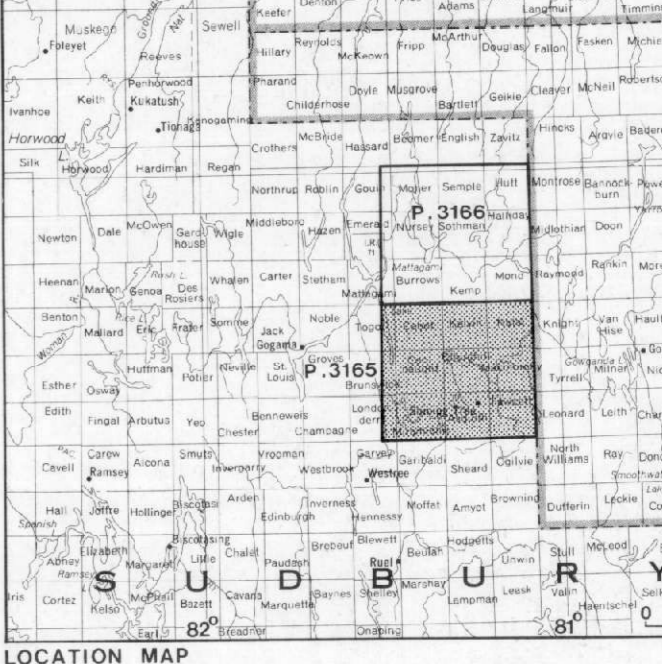
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### LEGEND

| PHANEROZOIC CENOZOIC QUATERNARY RECENT |  |
|--|--|
| 10                                     | Man-Emplaced Deposits: mine tailings, waste rock, wood waste |
| 9                                      | Modern Alluvium: silty sand to cobble gravel                 |
| 8                                      | Organic Deposits: peat, muck, mud                            |

| PLEISTOCENE |   |
|-------------|---|
| 7           | Eolian Deposits: coarse silt, fine- to medium-grained sand  |
| 6           | Glaciofluvial Deposits: silty sand to coarse sand, minor clay and silt  |
| 5           | Glaciofluvial Outwash Deposits: fine-grained sand to boulder gravel   |
| 4           | Ice-Contact Stratified Drift: silt, sand and gravel, boulders, minor fill                                     |
| 3           | Till: silt to sand matrix with granule to boulder-sized clasts  |
| 2           | Bedrock-drift complex: thin (< 1 m) and discontinuous drift (sedimentary character as indicated over bedrock) |
| 2a          | Undifferentiated drift veneer over bedrock  |
| 2a          | Till veneer over bedrock  |
| 2b          | Coarse-grained ice-contact stratified drift or glaciofluvial outwash sands and gravels over bedrock           |
| 2c          | Glaciofluvial or eolian sediments over bedrock  |

### EARLY TO LATE PRECAMBRIAN

|   |   |
|---|---|
| 1 | Bedrock: (> 60% exposure), with minor undifferentiated drift cover. |
|---|---|

### SYMBOLS

| Symbol                  | Name  |
|-------------------------|---|
| [Line with wavy dashes] | Geologic Boundary (Approximate)   |
| [X]                     | Small Bedrock Outcrop   |
| [Dashed line]           | Glacial Striation (Single, Multiple, Sequential, Younger Direction Crosscuts Older) |
| [Wavy line]             | Streamlined Bedrock or Till Form  |
| [Dashed line]           | Minor Moraine Ridge   |
| [Arrow]                 | Esker (Direction Known, Unknown)  |
| [Circle with X]         | Kettle: Ice Contact Slope   |
| [Wavy line]             | Meltwater Channel (Inferred Flow Direction Indicated)                               |
| [Dashed line]           | Fluvial Terrace   |
| [Wavy line]             | Dune Crest (Major Forms Only)   |
| [Arrow]                 | Beach Berm or Bar   |
| [X]                     | Gravel Pit  |

### SOURCES OF INFORMATION

Base map derived from Map 41 P/11 of the National Topographic System, scale 1:50 000.  
Aerial photography by the Ontario Ministry of Natural Resources. Contour interval: 50 feet (15.24 m).  
Magnetic declination approximately 8° 20' W in 1989.  
Geology not tied to surveyed lines.

### CREDITS

Geology by P. Finamore and J. MacKenzie, 1986; P.W. Alcock, M.J. Miller and J. Aulman, 1987, 1988.  
To enable rapid dissemination of data, this map has received only a cursory edit. Discrepancies may occur for which the Ontario Geological Survey does not assume

**MARGINAL NOTES**

**INTRODUCTION**  
The Quaternary geology of the Sinclair Lake map area (NTS 41 P/14) was mapped during the 1987 field season, with some further work in 1988 (Alcock 1987, 1988). The Shining Tree map area (NTS 41 P/11), immediately to the south, has also been mapped (Alcock and Miller 1989).

The surficial sediments were examined at natural and man-made exposures along roads and water courses, and through test cutting, hand auguring and borehole trenching. Access to much of the area is poor. The road system is limited to a few main gravel surfaced roads and a network of minor tracks maintained for forestry and recreational purposes. Rivers and lakes allowed access to many remote areas.

Surface units were delineated through airphoto interpretation using 1:5 840 and 1:50 000 scale airphotos. Deposit morphology, vegetation cover, drainage characteristics and reflectivity of exposed sediments were used to interpret the surficial deposits in remote areas. The distribution of deposits is strongly topographically controlled. Till, proglacial and ice-contact stratified drift, ice-contact and outwash deposits are present in north-south oriented valleys and glaciolacustrine and organic deposits occupy topographic lows with restricted drainage.

Any map unit represents a composite area, with the indicated deposit type predominating plus minor areas of other deposit types. For example, within the bedrock-drift complex, most areas of till veneer (<1 m thickness) over bedrock also include small areas of clastic till (1 m thickness) and organic deposits. Many contacts between map units represent an arbitrary division of the gradual transition from one deposit type to another, for example the transition from glaciolacustrine outwash to wave-washed outwash to glaciolacustrine sands. The bedrock-drift complex areas have a cover of drift over bedrock which varies in thickness, with frequent outcrops. All other units represent drift or organic material at least 1 m thick. Any site specific use of the surficial geology map should include an orientation survey to locally verify the sediment types, thickness and distribution.

The present study provides additional detail and local control to the regional mapping of Boisjourné (1965, 1969) and the basin study of Reed and Hallett (1979) and expands upon the areas initially mapped by Cross and Sado (1982). Reference is made to bedrock maps (Briant 1970, 1984; Carter 1981) for verifying areas of bedrock-drift complex.

The authors wish to acknowledge the administrative and logistical assistance of the staff at the Gogama District Office, Ontario Ministry of Natural Resources. Competent assistance in the field was provided by J. Aulman, J. H. Burchett and J. Schrader.

**BEDROCK GEOLOGY**  
In the Sinclair Lake map area, Early Precambrian rocks consist of a metabasaltic sequence with subordinate units of iron formation and metasediments (Bright 1970, 1984; Carter 1981). Marble and ultramafic sills and sill complexes intrude the metavolcanic sequence. Hanging regional east-west folding, the northwestern portion of the map area was intruded by a granitic pluton. Late porphyritic monzonite, granodiorite and syenite stocks were emplaced in the metavolcanic succession. Generally the Middle Precambrian (Proterozoic) classic and chemical sedimentary rocks of the Quirke Lake and Cobalt Groups unconformably overlie the Archaean rocks in the eastern portion of the map area. Early to Late Precambrian diatasee cluses out the previously emplaced units.

Deposits and occurrences of gold, silver, cobalt, copper, zinc, lead, molybdenum, nickel, iron and asbestos occur in the project area (Bright 1970, 1984; Carter 1981). Over the area, approximately 10 to 30% of the bedrock is exposed.

**PLEISTOCENE HISTORY**

The last late Wisconsinan ice advance, and postglacial glaciolacustrine ocean activity, are represented by the surficial sedimentary sequence. Glacially streamlined and striated bedrock outcrops, till fabrics and dispersion trends of lithologic indicators demonstrate that the last dominant ice movement was towards 180° to 30° azimuth. Minor late-glacial shifts in ice direction, due to bedrock topographic influences, are indicated by 160° to 180° striations constituting an earlier set of 160° to 180° striations. Where exposed, the bedrock surface is often glacially smoothed and striated and displays whaleback forms.

Certain rocher moutonnée-like presieve facets or remnants of grooves oriented southwest-northeast on their (southern) sides. On rare occasions, such as on Ferris Lake in Midland Township and in Gouin Township just west of the map area, north-south oriented grooves are crossed by southerly oriented striations. This evidence suggests an earlier southerly ice advance, similar to the one documented by Valletta (1986) in the Timmins, Matheson and Lake Timiskaming areas to the north and east of the project area.

Ice retreated from the area about 10 000 years BP (Dyke and Prest 1987), leaving a widespread drift veneer over the bedrock surface. Very few ice-conditional features are present in the area. Moraine ridges, are present. Several north-south-trending belts and ice-relevant striations of glaciolacustrine ice-contact and outwash sediments were deposited in the area. Upon deglaciation, meltwater flows were inundated by short-lived proglacial lakes. Widespread and narrowing of the glaciolacustrine and glaciolacustrine deposits produced bare bedrock knobs and blankets of nonstratified sand spilling out from the sediment sources. Accumulations of boulders on till are found over the range of glaciolacustrine veneer influence.

Melt-water drainage was controlled by the major valleys such as those occupied by the Gogama River, Ferris Lake and the Segonku Lake. Drainage of the proglacial lakes and subsequent outwash of the Gogama and West Michelson rivers. Most deposits are of very restricted areal extent and thickness and cannot be mapped at the current scale.

In areas of bedrock-drift complex, drift thickness commonly ranges from less than 1 m to in excess of 10 m. Extreme thicknesses of more than 50 m are present in areas of ice-contact deposits and in the major infilled valleys.

Only rare clasts of carbonate lithologies have been found in till or outwash deposits, indicating that the project area is south and east of the limit of carbonate drift as mapped by Kanow and Geddes (1987).

**SURFICIAL DEPOSITS**

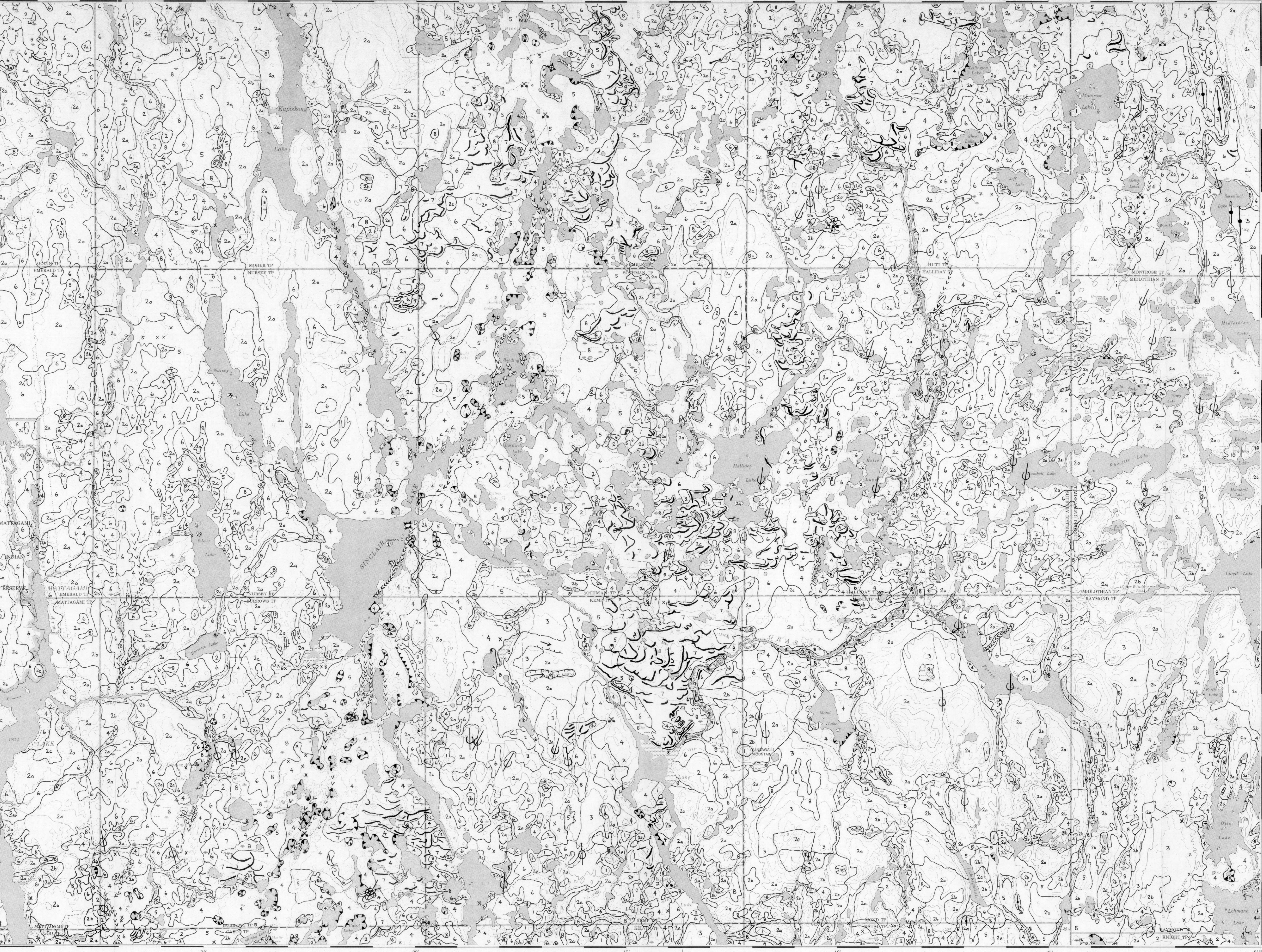
**TILL**  
Till is frequently found as a veneer over bedrock (Unit 2a) but ranges up to 4 m or more in thickness in areas of thick till (Unit 3). Till veneer areas (average thickness <1 m) have frequent bedrock outcrops and a surface morphology controlled by the underlying bedrock topography. Veneers of till are found over many bedrock hummocks and plateaus. Deposits of thick till found on the larger upland surfaces and in the lee of bedrock highs.

Both subglacial and supraglacial tills were identified using sedimentological and structural characteristics. Subglacially deposited tills are common at or near surface in areas of bedrock-drift complex and thick till. Lodgement is commonly incidentally to glacially compact, stony (10 to 50% clasts by volume) and has a silty sand matrix. This till type occasionally displays shear structures, and may overlie stratified bedrock. Subglacial melt-out till is loose to moderately compact, stony (10 to 50% clasts by volume), with a silty sand matrix and a silty sand matrix. Results from surface till samples collected up to several hundred metres down ice of known gold occurrences indicate gold grains are present in the sand-sized heavy mineral fraction. Further work has also indicated the presence of gold geochemical values in the silt and clay fraction of these samples.

A case study of gold dispersion in till was conducted by Stewart and van Hees (1982) in the Malachewan area, east of the Sinclair Lake map area. The results indicated that distinct dispersal trains from subcropping mineralized bedrock were present in the surface till in a number of size fractions.

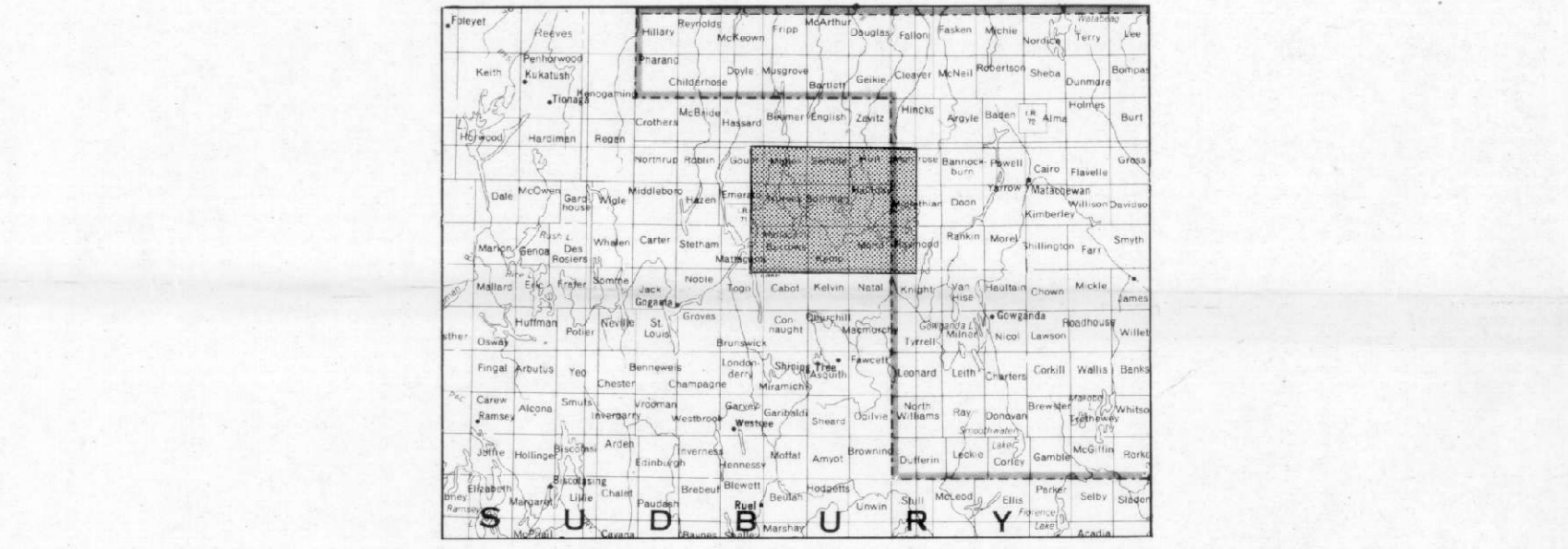
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**AGGREGATE RESOURCES**  
Aggregate resources are locally abundant in the vicinity of the main transportation corridors and are derived from esker, kames and outwash deposits. In higher elevation, remote areas, supplies may be inadequate and till may be used as a substitute for fill or borrow.



Ministry of Northern Development and Mines  
Ontario  
Mines and Minerals Division  
Ontario Geological Survey  
MAP P3166  
QUATERNARY GEOLOGY  
**SINCLAIR LAKE AREA**  
Scale 1:50 000  
100m 0 1 2km  
NTS Reference: 41 P/14  
Queen's Printer for Ontario, 1990.  
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CANADA ONTARIO  
This project is part of the five-year Canada-Ontario 1986 field development agreement (COODA) and is a subsidiary agreement to the Economic and Regional Development Agreement (ERA) signed by the governments of Canada and Ontario.



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**CENOZOIC**

**QUATERNARY**

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**PLEISTOCENE**

- 7 Eolian Deposits: coarse silt, fine to medium grained sand
- 6 Glaciolacustrine Deposits: siltly sand to coarse sand, minor clay and silt
- 5 Glaciolacustrine Outwash Deposits: fine-grained sand to boulder gravel
- 4 Ice-Contact Stratified Drift: silt, sand and gravel, boulders, minor flow till
- 3 Till: silt to sand matrix with granule- to boulder-sized clasts
- 2 Bedrock-drift complex: thin (<1 m) and discontinuous drift (sedimentary character as indicated) over bedrock
  - 2a Undifferentiated drift veneer over bedrock
  - 2a Till veneer over bedrock
  - 2b Coarse-grained ice-contact stratified drift or glaciolacustrine outwash sands and gravels over bedrock
  - 2c Glaciolacustrine or eolian sediments over bedrock

**UNCONFORMITY**

**EARLY TO LATE PRECAMBRIAN**

- 1 Bedrock: (>50% exposure), with minor undifferentiated drift cover

**SYMBOLS**

- Geologic Boundary (Approximate)
- Small Bedrock
- Glacial Stratification (Single, Multiple, Sequential, Youngest Direction Indicated)
- Streamlined Bedrock or Till Form
- Minor Moraine
- Esker (Direction of Flow Indicated)
- Geologic Boundary (Approximate)
- Kame
- Kettle: Ice-Contact Slope
- Meltwater Channel (Inferred Flow Direction Indicated)
- Fluvial Terrace
- Dune Crest (Major Forms Only)
- Beach Berm or Bar
- Gravel Pit

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**CREDITS**  
Geology by P.W. Alcock, M.J. Miller and J. Aulman, 1987 and 1988. To enable the rapid dissemination of information, this map has received only a cursory edit. Discrepancies may occur for which the Ontario Geological Survey does not assume liability. Users should verify critical information. Issued 1990.

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Alcock P.W. and Miller M.J. 1990. Quaternary geology, Sinclair Lake area, Ontario Geological Survey, Preliminary Map P3166, scale 1:50 000.

**SOURCES OF INFORMATION**  
Base map derived from map 41 P/14 of the National Topographic System, scale 1:50 000.  
Aerial photography by the Ontario Ministry of Natural Resources.  
Magnetic declination approximately 8°25' W in 1989.  
Contour interval: 50 feet (15.24 m).  
Geology not tied to surveyed lines.